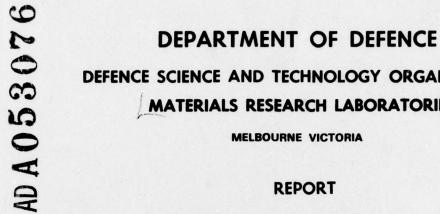
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TEMPERATURES OF ORDNANCE EQUIPMENT EXPOSED AT INNISFAIL, QUEENS--ETC(U)
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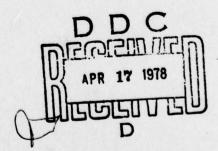
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TEMPERATURES OF ORDNANCE EQUIPMENT EXPOSED AT INNISFAIL, QUEENSLAND

Maureen E. Redman and J. A. McRae

Approved for Public Release





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REPORT

MRL-R-672

TEMPERATURES OF ORDNANCE EQUIPMENT EXPOSED AT INNISFAIL, QUEENSLAND

Maureen E. Redman J. A. McRae

**ABSTRACT** 

D Sep 76

Temperature of ordnance material exposed at Innisfail, Queensland, over a period of 18 months have been analysed to determine realistic temperature specifications for design and testing of equipment. The effect of exposure on the chemical deterioration of propellants has been quantified.

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# TEMPERATURES OF ORDNANCE EQUIPMENT EXPOSED AT INNISFAIL, QUEENSLAND

### INTRODUCTION

As part of a program aimed at defining the environmental factors pertinent to the design of rocket motors, TTCP Panel W4 organised the exposure of a number of inert-filled items of ordnance at the Joint Tropical Research Unit, Innisfail, Queensland (1). Temperatures reached at various locations in and on the items were recorded continuously for some eighteen months between October 1970 and June 1972. The temperatures were extracted from the analogue records and together with relevant meteorological data were assembled in a machine readable form. This report presents the analysis of the data.

### DATA

The data as originally made available had the format shown in Figure 1 which gives the temperatures in <sup>O</sup>F from one of the three chart recorders used to collect the data. The readings on any line are not simultaneous, but were taken at intervals of about 3.6 minutes, the time at the beginning of the line being the time at which channel 12 was recorded. The meteorological data were collected at hourly intervals and the ambient conditions at the end of each line are those recorded on the hour nearest to the time at the beginning of the line.

The data format proved unsuitable for some calculations and secondary files were created by combining the original hourly meteorological data with temperatures calculated to "on the hour" values on the assumption that the temperature variations between readings were linear with time. At the same time the temperatures were converted to OC. All subsequent processing was carried out using these secondary files.

The primary files contained a significant proportion of unlikely temperatures. When the secondary files were created temperatures greater than 80°C and temperatures which were more than 14°C less than the corresponding ambient temperature were put equal to zero. The subsequent analysis of the data showed that isolated, abnormally high readings remain but these do not significantly affect the results or conclusions.

The accuracy of the temperatures as supplied is difficult to estimate. The recorders were calibrated regularly and the reading and digitalising were accurate to within 1°F (1). It has therefore been assumed that the temperatures recorded are sufficiently representative of the temperatures experienced by the various areas of exposed ordnance equipment to allow valid conclusions to be drawn.

### LAYOUT OF TRIAL

The spatial arrangement of the rocket motors at the JTRU site is shown in Figure 2 and details of the items exposed together with all known details of thermocouple positions, surface finish and fillings are given in Table 1. The motors were supported about 300 mm above the ground on wooden blocks resting on light metal frames as shown in Figure 3. A skin thermocouple was located on the top surface of all items.

### METEOROLOGICAL CONDITIONS

JTRU, Innisfail is located at 17°32'S, 149°59'E and is in a relatively small area that because of topography and prevailing winds experiences abnormally high rainfall.

Meteorological data for the JTRU site are available from 1963 to 1974, and monthly averages of daily maximum and minimum temperatures, rainfall and solar radiation are shown in Table 2 together with the corresponding figures for each month of the trial period. Table 3 gives the overall averages for the trial period and compares them with weighted averages from the long term records calculated by taking single values for July, August and September and double values for the remaining months.

# TABLE 3 WEIGHTED METEOROLOGICAL AVERAGES FOR 1963-1974 AND AVERAGES FOR THE TRIAL PERIOD

	1963-1974	Trial Period
Daily Maximum (°C)	28.5	28.8
Daily Minimum (°C)	19.7	19.9
Rainfall (mm/month)	323	355
Solar Radiation (kWhr m <sup>-2</sup> /month)	137	144

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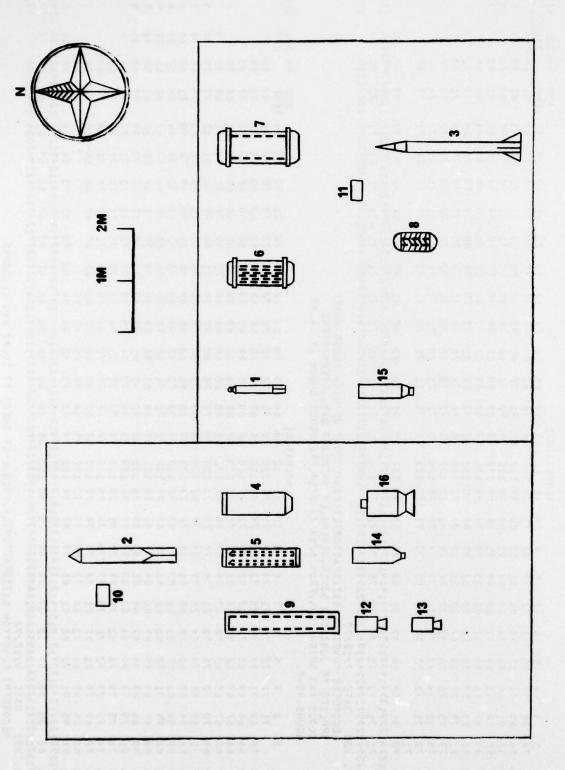


FIG. 2 LAYOUT OF ROCKET MOTORS. THE NUMBERS REFER TO TABLE 1

1

Thermocouple Positions	a. Motor Skin; b. Star Point.	a. Motor Skin; b. Star Point.	<ul><li>a. Motor Skin;</li><li>b. Centre filling;</li><li>c. Fibreglass Skin;</li><li>d. Aluminium</li><li>Skin.</li></ul>	a. Motor Skin; b. Centre filling.	a. Container Surface; b. Motor Skin; c. Star Point.	<ul><li>a. Box Surface;</li><li>b. Box-Motor air</li><li>space;</li><li>c. Motor Skin;</li><li>d. Star</li><li>Point;</li><li>e. Centre filling.</li></ul>	a. Box Surface; b. Box-Motor air space; c. Motor Skin.	a. Motor Skin; b. Cavity.	<ul><li>a. Box Surface;</li><li>b. Box-Motor air</li><li>space;</li><li>c. Motor Skin;</li><li>d. Star</li><li>point.</li></ul>	a. Box Surface; b. Centre of Box.	a. Box Surface; b. Centre of Box.
Filling	Ethyl Cellulose	Ethyl Cellulose	Sand	Sand	Ethyl Cellulose	Ethyl Cellulose	Sand	Sand, Glycol	Ethyl Cellulose	"Inert"	"Inert"
Surface Finish	Standard	Standard	White Aluminium Fibreglass	Standard	Standard	Standard	Standard	White	Standard	Standard	Standard
Dimensions mm	70 diam	140 diam	200 diam	300 diam	70 diam	200 diam	300 diam	300 diam	210 x 165 rectangular	7.62	20
Origin	as	sn	ns	Sn	Sn	ns	ns	Sin	Sn	O.S.	US
Type	FFAR	ZUNI	SPARROW	ASROC	4 X FFAR IN CONTAINER	SPARROW	ASROC	BULLPUP	SIDEWINDER BOXED	7.62 mm CARTRIDGES BOXED	200 mm CARTRIDGES BOXED
Number	1	2	e	4	5	۰	7	80	6	10	11

TABLE 1 (Continued)

Thermocouple Positions	Note (b)	Note (b)	Note (b)	Note (b)	Note (b)
Filling	IP230 <sup>(a)</sup>	IP230 <sup>(a)</sup>	IP230 <sup>(a)</sup>	IP230 <sup>(a)</sup>	IP230 <sup>(a)</sup>
Surface Finish	White to DTD5555 Solar Heat Resistant (c)	White to DTD5555 Non Solar Heat Resistant (c)	White to DTD5555 Solar Heat Resistant	Light Stone DTD5555 Solar Heat Resistant	White to DTD5555 Solar Heat Resistant
Dimensions	125 diam 600 length Light Alloy	125 diam 600 length Light Alloy	180 diam 1050 length Steel	180 diam 1050 length Steel	430 diam 1150 length Steel
Origin	UK	¥	¥	UK	Ħ
Type	LAP	LAP	LINNET	LINNET	CUCKOO
Number	12	13	14	IJ	16

### NOTES FOR TABLE 1

(a) The formulation of the inert propellant used to fill the UK rockets (IP230) is given as

KCl 75.3 pts by weight

BaSO, 9.7 pts by weight

Binder/Wetting Agent 15.0 pts by weight

The Binder/Wetting Agent is stated to be a mixture of high molecular weight poly(-)isobutylene 9 pts, surfactant (unspecified) 1 pt by weight.

- (b) The thermocouples on the UK rocket motors were located as follows:
  - 1. Two exterior thermocouples located diametrically opposite.
  - 2. One internal thermocouple on the same diameter and 12 mm from the inner surface of the case.
  - One internal thermocouple on the same diameter and on a star point.

Each motor contained two sets of thermocouples on the parallel portion of the motor and about 150 mm from the end of the parallel portion.

- (c) The solar heat resistant finishes have one coat of primer filler PR69 epoxy as ground coat and one glossy finishing coat. The non solar heat resisting finishes have no ground coat but two finishing coats.
- (d) No details are available on either the "standard" surface finish or the "inert" filling of US ordnance items.

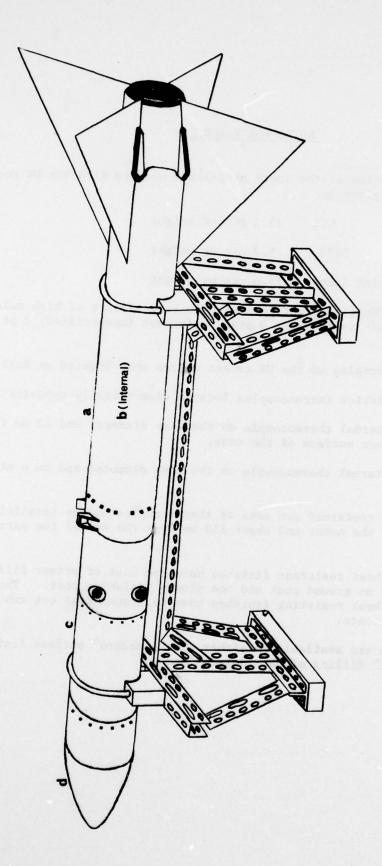


FIG.3 SPARROW ROCKET MOTOR SHOWING
METHOD. OF SUPPORT AND THERMOCOUPLE POSITIONS
TABLE 1

TABLE 2

METEOROLOGICAL CONDITIONS AT JIRU - LONG TERM AND TRIAL PERIOD AVERAGES

Average Daily	1963–74	JAN 31.5	FEB 30.5	максн 29.5	APRIL 28.0	MAY 26.0	JUNE 24.5	JULY 24.0	AUG 26.0	SEPT 27.0	OCT 29.0	31.0	DEC 31.0	
Maximum	70 Trial 71	33.0	31.0	28.0	26.5	27.0	23.5	23.0	27.0	28.5	29.0	30.5	31.0	
Temperatures OC		32.5	29.5	29.0	27.5	24.5	23.5	0 7 0 8 0 8 0 8	_	_		•	1	
Average Daily	1963-74	22.0	22.5	22.0	20.5	18.5	16.5	15.5	16.0	17.0	18.5	20.5	22.0	
Minimum	0, 0	•	.1	1	5 P	1	1	•	1	1	19.5	21.0	22.0	
	Trial 71	22.0	22.5	22.5	20.5	17.0	16.0	15.0	17.5	17.5	19.5	21.5	22.5	
Temperatures OC	1 72	22.0	22.5	21.5	21.0	18.0	16.0	•	-	1	•	•	•	
	Mean 1963-74	474	592	770	361	368	159	109	215	63	96	126	256	
Rain (mm)	( 70	1	1	1	•		•	1	1	1	120	360	320	
	Trial 71	106	760	1226	762	54	61	78	52	11	28	36	39	
	1 72	954	974	938	225	419	207		1	1	1	1	1	
Solar	Mean 1963-74	184	132	130	117	114	93	112	128	144	160	159	168	
Radiation	( 70	1	t	1	ı	1	1	1	1	1	179	168	185	
	Trial 71	248	138	101	29	154	29	112	133	168	118	193	199	
kWhrm-2	( 72	190	139	134	129	107	104	1	1	1	•	1	1	

### TABLE 4

### CUMULATIVE PROBABILITY DISTRIBUTION OF ROCKET TEMPERATURES

NO. OF TIMES THE MEASURED TEMPERATURE WAS EQUAL TO OR GREATER THAN TEMPERATURE IN COL. 1.

	AMBIENT	TEMPER	RATURE					
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	998	984	930	1001	3555	2015	9483	1.00
2	998	984	930	1001	3555	2014	9482	1.00
3	998	984	930	1001	3555	2014	9482	1.00
4	998	984	930	1001	3555	2014	9482	1.00
5	998	984	930	1001	3555	2014	9482	1.00
6	998	984	930	1001	3555	2014	9482	1.00
7	998	984	930	1001	3555	2014	9482	1.00
8	998	984	930	1001	3555	2012	9480	1.00
9	998	984	930	1001	3555	2003	9471	1.00
10	998	984	930	1001	3555	1994	9462	1.00
11	998	984	930	1001	3555	1989	9457	1.00
12	998	984	930	1001	3554	1969	9436	1.00
13	998	984	930	1001	3552	1941	9406	0.99
14	998	984	930	1001	3547	1901	9361	0.99
15	998	984	930	1001	3529	1821	9263	0.98
16	998	984	930	1001	3520	1791	9224	0.97
17	998	984	930	1001	3476	1621	9016	0.95
18	998	983	930	1001	3390	1371	8673	0.91
19	998	981	930	995	3214	1059	8177	0.86
20	988	966	928	970	2839	813	7504	0.79
21	977	955	923	948	2713	755	7271	0.77
22	890	863	836	834	2146	555	6124	0.65
23	724	680	579	592	1632	416	4623	0.49
24	572	515	396	358	1235	285	3361	0.35
25	484	426	303	238	980	179	2610	0.28
26	445	400	277	211	872	155	2360	0.25
27	350	319	196	128	637	88	1718	0.18
28	279	253	145	63	461	28	1229	0.13
29	190	197	78	27	305	8	805	0.08
30	117	128	41	7	174	2	469	0.05
31	105	114	34	3	140	2	398	0.04
32	58	82	13	1	75	0	229	0.02
33	31	38	4	0	35	0	108	0.01
34	16	16	0	0	13	0	45	0.00
35	10	11	0	0	4	0	25	0.00
36	6	6	0	0	3	0	15	0.00
37	2	4	0	0	0	0	6	0.00
38	0	1	0	0	0	0	1	0.00
39	0	0	0	0	0	0	0	0.00

The figures in Table 3 indicate that the trial period was slightly warmer, wetter and sunnier than would have been expected from the long term averages, but the differences are insignificant. The more detailed figures in Table 2 show that this agreement is somewhat fortuitous. Although there is a natural variation from year to year in all meteorological phenomena, the Winter and early Summer of 1971 were warmer and drier than normal and the highest temperature ever recorded at JTRU (40.5°C) occurred in December 1971. March 1971 was the wettest month on record while March, April and June 1971 were exceptionally cloudy.

QSTAG 360, "Climatic Environmental Conditions Affecting Design Criteria" is a quadripartite agreement to which the Australian Army subscribes and which is intended to standardise the environmental specifications for design requirements. Geographical areas are categorised in terms of diurnal cycles of temperature and humidity that can reasonably be expected to be exceeded for about 1% of the most severe month in any year. The climate at JTRU is classed as climatic category B2 where both temperature and relative humidity are factors that must be allowed for when designing equipment for use in such areas.

In the hottest month, a climate close to that of QSTAG 360 (B2) will have on average about 7.5 hours (1%) when the temperature reaches or exceeds 34°C. The cumulative frequency distribution of ambient temperatures at JTRU for the period of the trial is given in Table 4 and from these figures the 1% temperatures, that is the temperature reached or exceeded by 1% of the readings, is 35°C for both December and January with January being marginally hotter. By taking the means of the three-hourly temperature readings on the three days in January 1971 and the one day in January 1972 when temperatures higher than 35°C were recorded, the figures in Table 5 are obtained.

TABLE 5

TEMPERATURES AND HUMIDITIES FOR JTRU COMPARED

WITH THOSE OF QSTAG 360 (B2)

	Temperatu	re (°C)	Relative Hur	midity (%)
Local Time	JTRU	<u>B2</u>	JTRU	<u>B2</u>
0300	22	26	84	100
0600	21	26	83	100
0900	30	31	63	82
1200	36	34	41	75
1500	36	34	49	70
1800	31	32	66	82
2100	27	28	79	95
2400	25	27	85	97

While ambient temperatures are very close to those of category B2, the associated relative humidities are significantly lower. On the other hand, in January 1971, the relative humidity at JTRU was above the appropriate B2 value for 272 hours or about 30% of the time but at no time did both temperature and relative humidity simultaneously exceed the B2 figures.

Solar radiation values at three hourly intervals were higher than those specified for category B2 on 37 occasions during the trial and on three occasions (1500 hours on 3/1/71, 1500 hours and 1800 hours on 20/1/72) both ambient temperature and solar radiation were simultaneously higher than the category B2 figures. On only 3 of the 37 occasions was the 1200 hour radiation value higher than the 1.12 kWm<sup>-2</sup> laid down for category B2 and assuming that these readings represented a total of 9 hours in the two Januaries of the trial, the solar radiation figures are close to those specified for category B2.

Since in the trial, only temperatures were monitored and no account was taken of the effects of high humidities, it is valid to say that the rocket motors exposed at JTRU experienced ambient conditions close to those of QSTAG 360 category B2.

### ANALYSIS OF RESULTS

Three separate analyses of the results have been made. Cumulative probability distributions of temperatures of all thermocouple positions have been calculated. The equivalent constant temperatures, Tc, which give a measure of the chemical deterioration occurring at each thermocouple position (2), have been computed and correlations have been made between incident solar radiation intensity and the increase in motor skin temperature above ambient under clear-sky conditions.

### CUMULATIVE PROBABILITY DISTRIBUTIONS

Cumulative probability distributions giving the number of times each thermocouple recorded a temperature equal to or greater than a given temperature are given in full in Appendix A. Separate distributions were calculated for the following periods:

- (1) December, January, February and March.
- (2) Autumn-Spring and Winter as separate periods.
- (3) The whole trial period.

Table 6 gives as an example the cumulative probability distribution for the skin temperature of the ASROC motor (Table 1, Item 4, Thermocouple position a). This particular thermocouple position recorded the highest temperatures measured during the trial and it can be seen from the figures in Table 6 that the cutoff temperature of 80°C, above which readings were disregarded, is in fact reasonable. There is an isolated reading of

TABLE 6

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPERATURES

### ASROC MOTOR SKIN (UNBOXED)

RECORDER 31A. ROCKET MOTOR CHANNEL 6

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1018	1031	948	1031	3696	2031	9755	1.00
2	1018	1031	948	1031	3696	2031	9755	1.00
1 2 3	1018	1031	948	1031	3696	2031	9755	1.00
4	1018	1031	948	1031	3696	2029	9753	1.00
5	1018	1031	948	1031	3696	2025	9749	1.00
6	1018	1031	948	1031	3696	2022	9746	1.00
7	1018	1031	948	1031	3696	2018	9742	1.00
8	1018	1031	948	1031	3696	2009	9733	1.00
9	1018	1031	948	1031	3696	1992	9716	1.00
10	1018	1031	948	1031	3696	1972	9696	0.99
11	1018	1031	948	1031	3694	1961	9683	0.99
12	1018	1031	948	1031	3688	1931	9647	0.99
13	1018	1031	948	1031	3675	1892	9595	0.98
14	1018	1031	948	1031	3654	1830	9512	0.98
15	1018	1031	948	1031	3612	1742	9382	0.96
16	1017	1031	948	1031	3590	1691	9308	0.95
17	1017	1030	948	1030	3519	1566	9110	0.93
18	1017	1030	948	1018	3394	1394	8801	0.90
19	1009	1027	948	1009	3225	1212	8430	0.86
20	993	1014	948	992	2951	1035	7933	0.81
21	976	1006	945	964	2773	979	7643	0.78
22	915	965	917	901	2343	868	6909	0.71
23	798	883	780	746	1984	791	5982	0.61
24	691	781	605	553	1751	738	5119	0.52
25	616	669	506	461	1603	703	4558	0.47
26	586	617	470	427	1541	683	4324	0.44
27	538	556	416	379	1450	659	3998	0.41
28	505	509	388	339	1368	631	3740	0.38
29	471	470	364	311	1308	598	3522	0.36
30	448	445	335	297	1240	559	3324	0.34
31	435	433	324	288	1215	547	3242	0.33
32	416	410	305	268	1159	508	3066	0.31
33	399	399	294	251	1119	478	2940	0.30
34	386	383	277	237	1068	441	2792	0.29
35	371	373	266	226	1016	412	2664	0.27
36	364	363	258	219	981	403	2588	0.27
37	348	353	244	210	926	375	2456	0.25
38	328	345	234	200	867	337	2311	0.24
39	316	329	223	185	835	312	2200	0.23
40	308	321	209	174	809	279	2100	0.22
41	304	319	203	168	781	270	2045	0.21
42	296	313	194	158	731	236	1928	0.20
43	282	299	182	144	677	210	1794	0.18
44	267	294	169	130	638	179	1677	0.17
45	254	287	163	116	597	151	1574	0.16

### TABLE 6

(Cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPERATURES

### ASROC MOTOR SKIN (UNBOXED)

RECORDER 31A. ROCKET MOTOR CHANNEL 6

DEG.	DEC	JAN	FEB	MAR	AUT-SPR	ING	WINTER	TOTAL	C.PROB
		6876	1100		3030				
46	245	281	160	113	568		142	1509	0.15
47	231	273	147	101	518		127	1397	0.14
48	221	261	136	89	473		110	1290	0.13
49	204	243	132	82	441		96	1198	0.12
50	193	229	126	74	413		83	1118	0.11
51	186	224	124	71	395		74	1074	0.11
52	166	209	113	55	358		59	960	0.10
53	151	200	103	48	322		52	876	0.09
54	137	191	92	42	280		37	779	0.08
55	126	181	80	32	245		31	695	0.07
56	120	175	77	27	229		28	656	0.07
57	105	159	70	24	203		21	582	0.06
58	95	145	60	20	163		14	497	0.05
59	74	132	54	16	129		7	412	0.04
60	62	117	50	14	105		3	351	0.04
61	59	109	46	11	97		2	324	0.03
62	45	92	42	9	64		1	253	0.03
63	35	78	38	6	44		1	202	0.02
64	25	62	29	5	26		1	148	0.02
65	17	54	20	4	12		0	107	0.01
66	14	51	17	3	8		0	93	0.00
67	8	38	14	3	3		0	66	0.00
68	5	28	8	3	0		0	44	0.00
69	2	25	5	2	0		0	34	0.00
70	1	13	4	1	0		0	19	0.00
71	1	11	3	. 1	846.0		0	16	0.00
72	1	4	3	ī	0		0	9	0.00
73	ī	2	2	ī	0		0	6	0.00
74	ō	ō	2	ī	Ö		Ö	3	0.00
75	0	Ö	ō	ī	Ö		Ö	1	0.00
76	0	ő	Ö	ī	0		ő	i i	0.00
77	0	o	0	ō	0		0	ō	0.00
"			U	U	3 7 1 2		•	COC. O A	0.00

76°C in March which is probably erroneous since the next highest reading is 69°C.

The temperature reached or exceeded for any given percentage of the whole trial can be obtained immediately from the right hand column of Table 6. For example the temperature reached or exceeded for 1% of the time was  $65^{\circ}$ C while  $58^{\circ}$ C was reached or exceeded for 5% of the time. Similarly for any of the other periods, the 1% temperature is that temperature reached or exceeded by 1% of the readings; thus the 1% temperature for January will be the temperature recorded on  $1031 \times 0.01 = 10$  readings and this can be read off as  $71^{\circ}$ C.

### COMPARISON WITH STORAGE TEMPERATURES OF QSTAG 360

QSTAG 360 sets out storage temperatures that can be reasonably expected to be reached or exceeded for about 1% of the hottest month by equipment under typical field storage conditions. These are under tarpaulin covers or in railway boxcars and the storage conditions of the motors exposed in closed containers would be expected to be similar to those specified by QSTAG 360.

The temperatures reached or exceeded for 1% of the hottest month (January) at the surfaces of the items stored in enclosed boxes were obtained from the frequency distributions (Appendix A) and are given in Table 7.

TABLE 7

1% STORAGE TEMPERATURES FOR BOXED ITEMS (°C)

<u>Item</u>	1% Temperature	Appendix A Table
ASROC	57.5	N1
7.62 mm Cartridges	56	м3
20 mm Cartridges	55.5	V1
Sparrow	55	C1
FFAR	51	н3
Sidewinder	50	В3

The maximum 1% storage temperature for category B2 of QSTAG 360 is  $63^{\circ}\text{C}$  indicating that storage conditions at JTRU are less severe than those specified for QSTAG 360 (B2).

### TEMPERATURE PROFILES OF ROCKET MOTORS

The temperatures reached or exceeded for 1% and 5% of the whole trial period by the exterior thermocouples have been extracted from the cumulative frequency distributions and these are given in Table 8, where they are grouped in order of descending 1% temperature.

The 1% temperature in Table 8 show that there is a distinct gap between the five positions with the highest 1% temperature and the remainder. Four of these thermocouples were on metal surfaces coated with the U.S. standard grey finish. The high temperatures recorded on the fibreglass nose cone of the Sparrow rocket can be attributed to the poor thermal conductivity of this material. The effect of surface finish is also shown by the difference in 1% temperatures of the Linnet motors finished Light Stone  $(53^{\circ}\text{C})$  and White  $(46^{\circ}\text{C})$ .

The items with the lowest 1% temperatures were all white and there is no significant difference in the solar heat resistant and non-solar heat resistant finishes. The significantly lower temperatures recorded on the surface of the Bullpup motor are thought to be due to the liquid glycol filling providing a measure of convective cooling. This is supported by a difference of only 2°C in the 1% temperatures of skin and centre of the Bullpup compared with a difference of about 25°C between the 1% temperatures of skin and centre thermocouples in the ASROC motor which is of comparable size but had a sand filling.

The 1% temperature of the skin of the exposed ASROC motor is suspiciously high, but there is no other sand-filled grey motor for comparison. The general absence of items differing by only one factor such as filling makes any conclusions tentative, but smaller items appear to remain cooler than comparable larger items while grey motors enclosed in a grey box appear to experience temperatures intermediate between those they would experience if directly exposed and those they would reach if they were painted white and exposed.

The only definite conclusion which can be drawn is that a white surface finish significantly reduces temperatures throughout the exposed store. Even the Light Stone finish on the Linnet caused significantly higher skin temperatures than were reached on the same item with a white finish.

### TABLE 8

### 1% AND 5% TEMPERATURES OF EXTERIOR THERMOCOUPLES (°C)

Rocket Motor	Temperatures		
	1%	<u>5%</u>	
ASROC BOX	69	61	
SPARROW BOX	67	60	
ASROC	65	58	
SPARROW FIBREGLASS	63	57	
SIDEWINDER BOX	60	53	
LINNET (STONE)	53	48	
FFAR CONTAINER	52	47	
FFAR	52	48	
7.62 CARTRIDGE BOX	52	46	
20 mm CARTRIDGE BOX	51	47	
ZUNI	51	46	
SPARROW ALUMINIUM	49	45	
LAP SOLAR HEAT RESISTANT	47	43	
SPARROW MOTOR SKIN (WHITE)	47	43	
LAP NON SOLAR HEAT RESISTANT	46	43	
LINNET (WHITE)	46	42	
CUCKOO NOSE	46	43	
CUCKOO TAIL	44	41	
SPARROW (WHITE)	43	39	
BULLPUP	41	38	

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### CORRELATIONS BETWEEN AMBIENT CONDITIONS AND MOTOR SKIN TEMPERATURES

The temperature rise above that of the ambient air on the surface of an item exposed to solar radiation will be proportional to the intensity of the incident radiation. The constant of proportionality will be a function of a number of factors, the most important of which will be the surface finish which will determine the amount of energy absorbed, the airflow over the surface which will govern convective cooling and heat transfer from the exposed surface to the interior of the item. The surface finish and heat transfer will be relatively constant for a given item so that the skin temperature should be a function of incident solar radiation and wind speed and direction.

The meteorological data collected during the trial were insufficient to allow any estimate of the effect of wind speed on skin temperature so the linear regressions of solar radiation intensity on rise in motor skin temperature above ambient were obtained for days when clear-sky conditions prevailed. The restriction to clear-sky days is necessary because the hourly solar radiation figures that were supplied are time integrals of the intensity over the previous hour while the thermal time constant of the motor skins will be of the order of a few minutes and motor skin temperature will therefore be a function of the solar radiation intensity integrated over a few minutes prior to the temperature being recorded. On days other than those when solar radiation was uninterrupted by cloud, no correlation would be expected between hourly integrals of radiation intensity and instantaneous skin temperatures.

The days that had clear-sky conditions were selected by programming the computer to process data only on those days when each hourly solar radiation figure was above a predetermined value that had been obtained from records made at JTRU on clear-sky days in mid-summer and mid-winter. The criteria used were that each hourly radiation figure should be greater than 80% of the corresponding mid-summer figure for the summer period, greater than 70% of the corresponding mid-summer figure for the Spring and Autumn periods and more than 80% of the mid-winter figure for the Winter period. If any radiation figure on a given day between 0900 hours and 1600 hours was below the specified value, the days data was rejected. Over the period of the trial, 17% of days were selected by this procedure.

The regression equations between solar radiation and rise in motor skin temperature above ambient are summarised in Table 9 together with the rise in motor skin temperature calculated from the regression equations for a solar radiation intensity of  $1.14~\rm kWm^{-2}$  which is the accepted clear-sky maximum for air mass 1.

The entries in Table 9 are placed in the same order as those in Table 8 which gave 1% temperatures and it can be seen that in general, the items with high 1% temperatures had high correlation factors and high regression coefficients. This is as expected, since a high correlation factor implies that solar radiation is the dominant factor controlling skin temperature.

### TABLE 9

Correlations for the Difference between Skin Temperature and Ambient Temperature with Solar Radiation Intensity and 95% Confidence Limits for Increase of Skin Temperature above Ambient at a Solar Radiation Intensity of 1.14  $\rm kWm^{-2}$ .

Rocket Motor	Correlation Factor	Regression Coefficient	Increase above Ambient (°C)
ASROC BOX	0.76	33.9	35 ± 13
SPARROW BOX	0.76	30.6	35 ± 12
ASROC	0.86	27.8	33 ± 7
SPARROW FIBREGLASS	0.76	29.1	31 ± 11
SIDEWINDER BOX	0.72	24.1	26 ± 10
LINNET (STONE)	0.73	16.8	20 ± 7
FFAR CONTAINER	0.62	12.1	19 ± 7
FFAR	0.74	17.2	19 ± 7
7.62 CARTRIDGE BOX	0.47	10.5	19 ± 9
20 mm CARTRIDGE BOX	0.46	9.4	21 ± 8
ZUNI	0.54	7.7	17 ± 5
SPARROW ALUMINIUM	0.59	12.4	17 ± 8
SPARROW MOTOR SKIN (WHITE	E) 0.52	8.4	10 ± 6
LAP SOLAR HEAT RESISTANT	0.30	5.9	13 ± 8
LAP NON SOLAR HEAT RESISTANT	0.37	6.6	13 ± 7
LINNET (WHITE)	0.43	5.9	13 ± 6
CUCKOO NOSE	0.31	5.5	13 ± 7
CUCKOO TAIL	0.21	3.5	10 ± 7
BULLPUP	0.25	3.4	8 ± 6

The low absorbance of solar radiation by white surfaces and the consequent small temperature rises, means that other factors, notably convective cooling, will have magnitudes comparable to that of solar radiation and the correlation of temperature rise with solar radiation will be poor.

The increase in skin temperature above ambient temperature at a solar radiation intensity of 1.14 kWm $^{-2}$  was calculated in order to extend the skin temperatures, measured at JTRU, to areas experiencing higher ambient temperatures. To check whether this is possible, the temperature increases above ambient for those thermocouple positions with correlation factors above 0.7 were added to the ambient 1% temperature (33 $^{\circ}$ C) for the trial period (column 9 Table 4) and these predicted 1% temperatures are compared in Table 10 with measured 1% temperatures from Table 8.

T A B L E 10

MEASURED AND PREDICTED 1% TEMPERATURES (°C)

<u>Item</u>	Measured	Predicted
ASROC Box	69	67
Sparrow Box	67	67
ASROC	65	65
Sparrow Fibreglass	63	64
Sidewinder Box	60	59
Linnet (Stone)	53	53
FFAR	52	52

The 1% temperature for the whole trial period, rather than the 1% temperature for the hottest month was used because the correlations with clear-sky radiation were obtained over the whole trial period.

In extending these results to another area, the major assumption necessary is that the area has substantially the same pattern of wind speeds. The hottest parts of Australia have a 1% temperature of 44°C (3) giving a maximum 1% Skin Temperature of about 80°C. It should be noted that this is the temperature induced on the equipment by exposure to direct solar radiation and is not the storage temperature as defined in QSTAG 360 which refers to equipment stored under cover.

### CALCULATION OF EQUIVALENT CONSTANT TEMPERATURES AND EQUIVALENT LIFETIMES

It has been shown that for any given temperature cycle, it is possible to calculate a single constant temperature that gives the same amount of chemical reaction for any system (2). This constant temperature,  $T_c$ , can be used as a direct measure of the severity of chemical deterioration at any thermocouple position over the period of the whole trial since a higher value of  $T_c$  implies faster deterioration.  $T_c$  can simply be transformed to another measure,  $L_F$ , the equivalent storage lifetime (3) which compares the time taken to reach the same stage of decomposition as would be reached for a standard time at a standard temperature. If the standard conditions are taken to be 10 years at  $25^\circ$ , the equation relating  $L_F$  and  $T_c$  is:

$$L_E = 10 \exp \frac{E_a}{R} \left[ \frac{1}{T_c} - \frac{1}{298} \right]$$
 where  $T_c$  is in  ${}^{O}K$  and  $E_a$  is 80 kJmole<sup>-1</sup>

 $\rm T_{c}$  values were calculated for all thermocouple positions using measured temperatures over the whole trial period and these are given together with  $\rm L_{E}$  values in Table 11.

The figures in Table 11 can be used for comparison with long term storage trials at constant temperatures. For example, an ASROC motor stored at 40°C would be undergoing deterioration at about the same rate as would be occurring adjacent to the motor skin of a motor exposed at JTRU. Alternatively, if the ASROC were known to become unserviceable because of deterioration of the propellant after storage for 10 years at 25°C, it would be expected to be unserviceable after 2 years in the open at JTRU or if stored at 40°C.

Table 11 can also be used to estimate the magnitudes of thermal gradients from the case to the centre of the propellant. The worst example is the ASROC with  $L_{\rm E}$  values of 2 years for the skin and 5.4 years for the centre, while the white painted Linnet has  $L_{\rm E}$  = 5.3 years for the case, propellant and star point indicating that there is a much more even thermal gradient throughout the propellant.

Motor	Position	Refer Table 1	T <sub>C</sub> (°C)	L <sub>E</sub> Years
ASROC (BOXED)	Box Surface	7a	42.8	1.5
SPARROW (BOXED)	Box Surface	6a	42.1	1.6
SPARROW	Fibreglass Skin	3c	40.8	1.8
ASROC	Motor Skin	4a	40.2	2.0
SPARROW (BOXED)	Air Space	6b	36.8	2.8
ASROC (BOXED)	Air Space	7b	36.7	2.8
SIDEWINDER (BOXED)	Box Surface	9a	36.3	2.9
20 mm CARTRIDGES	Box Surface	11a	35.0	3.4
7.62 CARTRIDGES	Box Surface	10a	34.2	3.7
ASROC (BOXED)	Motor Skin	7c	34.2	3.7
SPARROW (BOXED)	Motor Skin	6c	33.5	3.9
FFAR	Motor Skin	la	33.2	4.1
20 mm CARTRIDGES	Centre of Box	11b	33.2	4.1
LINNET (STONE)	Motor Skin	15 Note (b)1	33.0	4.2
FFAR	Star Point	1b	32.9	4.2
FFAR IN CONTAINER	Container Skin	5a	32.7	4.3
7.62 mm CARTRIDGES	Centre of Box	10ь	32.6	4.3
ZUNI	Motor Skin	2a	32.4	4.4
ZUNI	Star Point	2b	32.3	4.5
SPARROW (BOXED)	Centre Filling	6e	32.3	4.5
LAP (NSHR*)	Motor Skin Top	13 Note (b)1	32.3	4.5
SPARROW	Aluminium Skin	3d	32.2	4.6
LINNET (STONE)	Internal Propellant	15 Note (b)2	31.8	4.7
SIDEWINDER (BOXED)	Air Space	9b	31.7	4.8
LAP (SHR*)	Propellant Tail	12 Note (b)2	31.7	4.8
CUCKOO	Motor Skin Top Nose	16 Note (b)1	31.6	4.8
LAP (SHR*)	Propellant Nose	12 Note (b)1	31.5	4.9
LAP (SHR*)	Star Point Tail	12 Note (b)3	31.5	4.9
LAP (SHR*)	Star Point Nose	12 Note (b)3	31.4	4.9
LAP (SHR*)	Motor Skin Tail Top	12 Note (b)1	31.4	4.9
LAP (NSHR)	Propellant Tail	13 Note (b)2	31.4	4.9
LAP (NSHR)	Star Point Nose	13 Note (b)2	31.3	5.0

TABLE 11
(Continued)

Motor	Position	Refer Table 1	T <sub>C</sub> (°C)	L_Years
LAP (NSHR)	Propellant Nose	13 Note (b)3	31.2	5.0
LAP (NSHR)	Motor Skin Tail Top	13 Note (b)2	31.2	5.0
LAP (SHR)	Motor Skin Tail Bottom	12 Note (b)1	31.2	5.0
LAP (NSHR)	Star Point Nose	13 Note (b)1	31.0	5.2
СИСКОО	Star Point Nose	16 Note (b)3	31.0	5.2
LINNET (WHITE)	Motor Skin Top	14 Note (b)3	30.8	5.3
SPARROW (BOXED)	Star Point	6d	30.8	5.3
LINNET (WHITE)	Propellant	14 Note (b)2	30.7	5.3
LINNET (WHITE)	Star Point	14 Note (b)3	30.7	5.3
LINNET (STONE)	Star Point	15 Note (b)3	30.5	5.4
CUCKOO	Motor Skin Top Tail	16 Note (b)1	30.5	5.4
ASROC	Centre Filling	4b	30.5	5.4
FFAR IN CONTAINER	Motor Skin	5ъ	30.4	5.5
СИСКОО	Star Point Tail	16 Note (b)3	30.4	5.5
CUCKOO	Propellant Tail	16 Note (b)2	30.3	5.6
ASROC (BOXED)	Centre Filling	7d	30.2	5.6
FFAR (BOXED)	Star Point	5c	30.2	5.6
SIDEWINDER (BOXED)	Motor Skin	9c	30.0	5.8
SIDEWINDER (BOXED)	Star Point	9Ъ	29.9	5.8
LINNET (WHITE)	Motor Skin Bottom	14 Note (b)1	29.8	5.9
CUCKOO	Star Point	16 Note (b)3	29.8	5.9
СИСКОО	Motor Skin Bottom	16 Note (b)1	29.5	6.1
LINNET (STONE)	Motor Skin Bottom	15 Note (b)1	28.6	6.7
SPARROW	Centre Filling	3ъ	28.2	7.0
BULLPUP	Motor Skin	8a	28.0	7.2
BULLPUP	Cavity	8ъ	27.3	7.7
SPARROW	Motor Skin (White)	3a	27.2	7.8

\*SHR Solar Heat Resistant
NSHR Non Solar Heat Resistant

### CONCLUSIONS

- 1. Equipment with a white surface finish will have significantly lower temperatures than similar equipment with a dark surface finish.
- 2. Equipment exposed in a closed container will experience temperatures lower than those of the same equipment uncovered but higher than would be experienced if the exposed surface finish was white.
- 3. The ambient temperatures and solar radiation at Innisfail during the trial were close to those laid down for QSTAG 360 category B2.
- 4. The solar heat resisting finish of the UK rocket motors had no effect on temperatures.
- 5. Equipment with a dark surface finish exposed in the hotter areas of Australia could be expected to reach skin temperatures of about 80°C for 1% of the hottest month.
- 6. Assuming the propellant of a rocket motor to have a service life of 10 years if stored at 25°C, the exterior layers of the same item stored in the open at JTRU would have service lifetimes varying between 2 years if the item has a dark surface finish and 6 years if it has a white surface finish.

### **ACKNOWLEDGEMENTS**

Thanks are due to the staff at JTRU who, apart from the original data collection, have answered a number of incidental queries that arose during the preparation of this report. The concept of 'Life Expectancy' used on pages 10 and 11 of this report was originally used, in a somewhat different form, by Mr. B.E. Furby of WRE, Salisbury.

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### APPENDIX 1

TABLES A1  $\rightarrow$  X1, A2  $\rightarrow$  X2, A3  $\rightarrow$  N3

# CUMULATIVE PROBABILITY DISTRIBUTIONS FOR ROCKET MOTOR TEMPERATURES

These tables give the number of times the temperature was equal to or greater than the temperature in column one.

DISTRIBUTION STATEMENT A

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TABLE A1 CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW CENTRE (BOXED)

RECORDER 30B.

TABLE A1 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW CENTRE (BOXED)

		RECO	RDER	30B.	ROCKET MO	TOR CHANNE	L 1	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	Ø	13	2	Ø	5	0	20,	0,00
47	Ø	7	Ø	Ø	5	Ø	12.	0,00
48	Ø	1	Ø	Ø	5	Ø	6,	0.00
49	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
50	Ø	Ø	Ø	Ø	5	Õ	5.	0.00
51	Ø	Ø	Ø	0	5	Ø	5.	0.00
52	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
53	Ø	Ø	Ø	Ø	5	Ü	5.	0.00
54	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
55	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
56	Ø	Ø	0	Ø	5	Ø	5.	0.00
57	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
58	Ø	Ø	Ø	Ø	5	Ø	5. 5.	0.00
59	Ø	Ø	0	Ø	5	Ø	5.	0.00
60	Ø	Ø	Ø	0	5	Ø	5.	0.00
61	Ø	Ø	Ø	0	5	Ø	5,	0.00
62	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
63	Ø	Ø	Ø	0	5	Ø	5.	0.00
64	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
65	Ø	Ø	Ø	Ø		Ø	3.	0.00
66	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
67	Ø	Ø	0	Ø	3	Ø	3.	0.00
68	Ø	Ø	Ø	Ø	3		3.	0.00
69	Ø	Ø	Ø	Ø	3 3 3 3 3	Ø	3.	0.00
70	Ø	Ø	Ø	0	3	Ø	3.	0.00
71	0	Ø	Ø	0	3	Ø	3,	0.00
72	Ø	Ø	Ø	0	3	Ø	3.	0,00
73	Ø	Ø	Ø	Ø		Ø	3.	0.00
74	Ø	Ø	0	Ø	3	Ø	3,	0.00
75	Ø	Ø	Ø	0	3 3 3 3 2 1	Ø	3,	0.00
76	Ø	0	0	Ø	3	Ü	3.	0.00
77	0	Ø	0	0	3	Ø	3,	0.00
78	Ø	Ø	Ø	Ø	2	. 0	2.	0,00
79	Ø	Ø	0	0	1	0	1.	0.00 .
80	Ø	Ø	. 0	Ø	Ø	Ø	2.	0.00

TABLE B1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW OUTER FILLING (BOXED)

		0500		7~0	DOCKET NO	TOD GUANA	-	
		RECO	RUER	308.	ROCKET MO	TOR CHANNI	FF 5	
	250	LAN	550	440	AUT CORTNO	HINTED	TOTAL	C 0000
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
	1018	4030	948	1032	3505	2031	9564.	1.00
1 2		1030		1032	3505	2031	9564.	1.00
3	1018			1032	3505	2031	9564.	1,00
4	1018			1032	3505	2031	9564.	1.00
5	1018			1032	3505	2031	9564.	1.00
6	1018			1032	3505	2031	9564.	1,00
7	1018			1032	3505	2031	9564.	1,00
8	1017			1032	3505	2031	9563.	1.00
9		1030		1032	3505	2029	9561,	1.00
		1030			3505	2026	9558.	1.00
10	1017		948	1032	3505	2024	9556.	1,00
11		1030	948			2013	9545.	1.00
12				1032	3505		9532.	
13	1017			1032	3504	2001 1990		1.00
14	1017			1032	3503		9520.	1.00
15		1030			3503	1962	9492.	0.99
16		1030			3503	1936	9466.	
17		1030		1032	3499	1885 1777	9411.	0,98
18		1030			3485	1608	9289.	0.97
19		1030		1032	3458		9093.	0,95
20		1030		1031	3397	1429	8851.	0.93
21			946	1025	3345	1332	8695.	0.91
22	1015	1030	944	1004	3169	1129	8291.	0.87
23	1002		939	966	2932	981	7848.	0.82
24	981	1019	894	883	2614	847	7238.	0.76
25	914	961	815	727	2270	728	6415.	0.67
2.6	871	913	756	641	2105	678	5964.	0.62
27	790	831	654	514	1854	579	5222.	0.55
28	693	743	554	416	1621	507	4534.	0.47
29	622	663	485	357	1448	413	3988.	0.42
30	561	604	419	311	1295	347	3537.	0.37
31	538	574	396	296	1221	311	3336.	0.35
32	479	517	346	257	1083	261	2943.	0.31
33	443	480	306	219	958	203	2609.	0.27
34	397	430	274	182	845	164	2292.	0.24
35	359	395 377	244	147	719	122	1986.	0.21
36	336		229	133	669		1854.	0.19
37	307	349	205	108	602	83	1654.	0.17
38	272	324	177	85	525	57	1440.	0,15
39	243	293	152	58	429	38	1213.	0.13
40	200	267	127	40	347	18	999.	0.10
41	184	252	119	31	318	12	916.	0.10
42	153	218	102	17	250	2	745.	0.08
43	120	186	82	10	191	6	591.	0.06
44	97	165	65	. 4	129	0	460.	0.05
40	71	124	48	2	85		330.	0.03

TABLE B1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW OUTER FILLING (BOXED)

		RECOR	DER	30B.	ROCKET MOT	OR CHANNE	L 2 .	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C,PROB
46	63	110	38	2	59	Ø	272.	0.03
47	41	81	31	2	23	Ø	178.	0,02
48	25	60	22	2	8	Ø	117.	0.01
49	10	40	13	2 2 2 2	5	Ø	70.	0.00
50	0	24	7	2	5	Ø	38.	0.00
51	Ø	16	5	2	5	. 6	28.	0.00
52	Ø	10	Ø	2	5	Ø	17,	0.00
53	Ø	4	0	2	5	Ú	11,	0.00
54	Ø	1	0	2 2 2 2	5 5	Ø	8.	0.00
55	Ø	Ø	Ø	2	5	Ø	7.	0.00
56	Ø	Ø	0	1	5	Ø	6.	0.00
57	0	Ø	Ø	1	5	Ø	6.	0.00
58	0	Ø	0	1	5	Ø	6.	0.00
59	0	Ø	Ø	1	5	Ø	6.	0.00
60	0	Ø	Ø	1	5	Ø	6.	0.00
61	0	Ø	Ø	1	5	Ø	6.	0.00
62	0	Ø	Ø	1	5	Ø	6.	0.00
63	0	Ø	Ø	1	5	Ø	6.	0.00
64	0	Ø.	Ø	1	. 5	Ü	6,	0.00
65	Ø	Ø	Ø	1	5 3 3 3 3 3 3	Ø	4.	0.00
66	0	Ø	Ø	Ø	3	Ü	3.	0.00
67	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
68	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
69	Ø	Ø	0	Ø	3	Ø	3.	0.00
70	0	Ø	0	Ø	3	Ø	3.	0.00
71	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
72	0	Ø	Ø	Ø	3	Ø	3.	0.00
73	Ø	0	Ø	Ø	3	Ø	3.	0.00
74	0	Ø	Ø	0	3	Ø	3.	0.00
75	Ø	Ø	0	Ø	3 3 3 2	80	3,	0.00
76	Ø	Ø	Ø	Ø	3		3,	0.00
77	Ø	0	Ø	Ø	2	Ø	2.	0.00
78	Ø	0	0	0	1	Û	1.	0.00
79	0	0	0	0	. Ø	Ø	Ø.	0.00

TABLE C1

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW MOTOR SKIN (BOXED)

RECORDER 30B. ROCKET MOTOR CHANNEL 3

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1018	1030	948	1032	3505	2031	9564.	1.00
2		1030	948	1032	3505	2031	9564.	1.00
3		1030		1032	3505	2031	9564.	1.00
4		1030		1032	3505	2031	9564.	1,00
5		1030	948		3505	2031	9564	1,00
6	1018		948		3505	2031	9564.	1.00
7		1030	948		3505	2031	9564.	
8		1030		1032	3505	2029	05/0	4 00
9		1030	948		3505	2026	9559	1.00
10		1030		1032	3505	2020	9553.	1.00
		1030						
11		1030		1032	35Ø5	2018	9551.	1.00
12	1018	1030			3505	2004	9537,	1.00
13	1018			1032	3505	1988	9521.	1.00
14		1030	948	1032	3504	1969	9501.	0.99
15		1030	948	1032	3502	1930	9460.	0.99
16		1030		1032	3501	1907	9436.	0.99
17		1030		1032	3490	1835	9353,	0.98
18		1030		1032	3463	1700	9191.	0.96
19	1018		947		3425	1526	8977.	
20		1030	946	1023	3333	1,337	8687.	
21	1018	1030	944	1017	3267	1225	8501.	0.89
22		1029	943	992	3056	1054	8083.	Ø,85
23	995	1021	935	937	2769	933	7590.	0.79
24	949	1005	881	836	2440	825	6936.	0.73
25	865	913	764	668	2116	725	6051.	0,63
26	818	861	700	595	1960	677	5611.	0.59
27	721	761	597	472	1737	609	4897.	0.51
28	644	674	511	401	1563	550	4343.	0,45
29	590	605	449	350	1407	486	3887.	0.41
30	533	556	397	310	1273	412	3481.	0.36
31	511	535	378	297	1218	383	3322.	0.35
32	466	493	333	264	1114	324	2994.	
33	426	455	310	233	1019	277	2720.	0.28
34	394	421	275	205	923	229	2447.	0.26
35	366	391	249	184	828	192	2210.	Ø.23.
36	349	377	234	176	789	171	2096.	0.22
37	315	347	216	150	706	143	1877.	0.20
38	298	322	192	124	624	110	1670.	0.17
39	273	310	175	100	560	82	1500.	0,16
40	237	287	151	78	489	66	1308.	0.14
41	228	274	147	68	452	49	1218.	0.13
42	197	255	131	52	381	30	1046.	Ø.11
43	169	234	113	40	318	19	893.	0.09
44	150	208	96	27	265	11	757.	0.08
45	128	188	80	14	207	4	621.	0.06

TABLE C1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW MOTOR SKIN (BOXED)

		RECO	RDER	30B.	ROCKET MOT	OR CHANNE	L 3	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	121	177	74	10	181	3	566.	0,06
47	98	149	65	5	134	Ø	451.	0.05
48	71	126	54	2	92	0	345.	0.04
49	48	99	39	2	49	Ø	237.	0,02
50	36	72	28	1	24	Ø	161.	0,02
51	25	58	27	1	17	Ø	128.	0.01
52	12	42	17	1	6	Ø	78,	0.00
53	4	27	8	1	6	Ü	46,	0.00
54	2	19	3	1	6	Ø	31.	0.00
55	1	9	2	1	5		18,	0,00
56	Ø	8	Ø	1	5	Ø	14.	0.00
57	Ø	4	Ø	1	5		10.	0.00
58	Ø	0	Ø	1	5	Ö	6.	0,00
59	Ø	Ø	Ø	1	5	Ø	6.	0,00
60	Ø	0	Ø	1	5		6.	0.00
61	Ø	0	Ø	1	5	Ò	6.	0.00
62	Ø	Ø	Ø	1	5	0	6.	0,00
63	Ø	0	Ø	1	5	Ø	6.	0.00
64	Ø	Ø	Ø	. 1	4	Ø	5.	0.00
65	Ø	Ø	Ø	1		Ø	4.	0.00
66	Ø	Ø	Ø	ī	3 3 3 3 3 3 3 3	Ø	4.	0.00
67	Ø	Ø	Ø	Ø	3	Ü	3.	0.00
68	Ø	Ø	Ø	Ø	3	Ö	3.	0.00
69	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
70	Ø	0	Ø	Ø	3	Ø	3,	0.00
71	Ø	0	0	Ø	3	Ø	3,	0.00
72	Ø	Ø	Ø	0	3	. 0	3.	0.00
73	Ø	Ø	0	0	3	Ø	3.	0.00
74	Ø	Ø	0	Ø	3	Ü	3,	0.00
75	Ø	Ø	Ø	0	2	Ø	2.	0.00
76	Ø	Ø	Ø	Ø	2 2	Ø	2.	0.00
77	Ø	0	Ø	0	ø	Ø Ø	Ø,	0,00

TABLE D1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW HALFWAY BET. SKIN AND BOX

TABLE D1 (cont.)

#### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW HALFWAY BET. SKIN AND BOX

		RECO	RDER	3ØB.	ROCKET MOT	OR CHANNE	L 4	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	199	247	126	59	433	56	1120.	0.12
47	184	235	114	46	381	37	997.	0.10
48	168	222	105	36	331	24	886.	0.09
49	151	204	92	29	279	14	769.	0.08
50	134	181	76	22	220	14 6 3 1	639.	0.07
51	124	171	70	17	202	3	587.	0.06
52	104	146	63	11	144	1	469.	0,05
53	81	123	56	6	107	Ø	373.	0.04
54	62	92	50	4	81	Ø	289.	0.03
55	44	74	39	2	50	Ø	209.	0.02
56	35	6.6	34	2 2	36	Ø	173.	0,02
57	27	51	25	2	22	Ø.	127.	0.01
58	21	37	20	1	9	Ø	88.	0.00
59	8	26	8	1	7	Ø	50.	0.00
60	2	20	5 5 2	1	6	Ø Ø	34.	0.00
61	2 2	15	5	1	6	Ø	29.	0.00
62	2	8	2	1	6	Ø	19.	0.00
63	0	4	Ø	1	6	Ú Ú	11,	0.00
64	Ø	2	Ø	1	5		8,	0.00
65	Ø	Ø	Ø	1	4	Ø	5.	0.00
66	Ø	Ø	Ø	1	3	Ø	4.	0,00
67	. Ø	Ø	Ø	Ø	3	Ø	3.	0,00
68	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
69	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
7.0	Ø	Ø	Ø	Ø	3 3 3	Ø	3.	0.00
71	Ø	Ø	0	Ø	3	Ø	3.	0.00
72	Ø	0	Ø	0	1	. 0	1.	0.00
73	Ø	Ø	Ø	Ø	Ø	Ď	Ø.	0,00

TABLE E1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW OUTER CASE

		RECO	0050	30B.	POCKET	WOTOP	CHANNEL	5	
		KEOU	NUEN	000.	ROCKET	MOION	CHANNEL		
DEG.	DEC	JAN	FEB	MAR	AUT-SPRI	NG WI	NTER	TOTAL	C.PROB
				4070	700.				
1		1031	948	-	3501			9561.	1.00
	1018			1032	3501			9561.	1.00
3	1018		948		3501			9561.	1.00
4		1031		1032	3501			9560.	1.00
5		1031	948 948	1032	3501			9554. 9552.	1.00
7		1031		1032	3501 3501			9548.	1.00
8	1018			1032	3501			9534.	1,00
9			948		3501			9514.	1.00
10		1031	948		3501			9491.	0.99
11		1031	948	1032	3501			9480.	0.99
12		1031	948	1032	3499			9445.	0.99
13		1031		1032	3492			9390.	0,98
14		1031			3468			9301.	0.97
15		1031	947		3427			9173.	0,96
16	1018		946	1031	3400			9075.	0,95
17			945	1022	3329			8852.	0.93
18		1029	945	1012	3215			8550.	0.89
19		1025	942	997	3063			8173,	0.85
20		1012	941		2834			7748.	0.81
21	978	1000	939	953	2660			7466.	Ø.78
22	910	960	932	890	2367			6897.	0.72
23	803	884	847	763	2026			6100.	0.64
24	693	770	680	621	1728			5222.	0,55
25	604	645	538	494	1552		693	4526,	0.47
26	567	583	479	436	1499			4247.	0.44
27	513	525	419	381	1409			3904.	0.41
28	486	488	375	347	1329			3658.	0.38
29	461	449	358	326	1271			3469,	0.36
30	439	429	339	302	1216			3301.	0,35
31	430	425	329	290	1194			3224,	0.34
32	415	409	311	278	1152			3084.	0.32
33	394	398	296	265	1113			2953.	0.31
34	382	386	286	254	1070			2835.	0.30
35	365	368	273	243	1217			2695.	0.28
36	355	364	268	236	985			2626.	0.27
37	343	351	254	228	952			2519.	0.26
38	335	343	237	218	913			2406.	0.25
39	321	338	228	204	874			2299.	0.24
40	309	326	219	195	835			2193.	0.23
41	303	322	214	191	812			2138.	0.22
43	290	318 312	205	182	773			2042.	Ø.21 Ø.20
44	284	301	193	172	723			1813.	0,19
45		285	185 173	158	682			1700.	0.18
77	263	200	1/3	141	642		720	1100	D 1 TO

TABLE E1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW OUTER CASE

		RECORDER	₹ 308.	ROCKET MOT	OR CHANNE	L 5	
DEG.	DEC	JAN FE	B MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	257	282 169		616	183	1640.	0.17
47	248	272 166		579	169	1543.	Ø,16
48	239	262 154		545	146	1451.	0.15
49	221	253 147		505	132	1345.	0.14
50	204	241 135		474	111	1242.	0.13
51	202	237 129		447	100	1189.	0.12
52	185	224 125		402	84	1088.	0.11
53	170	207 122		372	74	1003.	0.10
54	160	198 116		329	61	908.	0.09
55	149	188 100		302	51	836.	0.09
56	143	184 98		285	47	801.	0.08
57	121	179 89		247	34	710.	0.07
58	114	168 78		206	21	622.	0.07
59	96	150 76		172	13	529.	0.06
60	88	138 66	25	142	10	469.	0.05
61	80	128 64		132	9	433,	0.05
62	64	114 5		99	5	354.	0.04
63	54	96 5		74	1 1	294.	0.03
64	39	77 46		51	1	224.	0.02
65	30	65 37		30	1	170.	0.02
66	26	61 33		24	1	152.	0.02
67	22	51 25		14	1	118.	0.01
68	21	42 23	2 3	8	Ø Ø Ø	96.	0.01
69	17	37 12	2 3	7	Ø	76.	0.00
70	13	29 1	2	2	Ø	56.	0.00
71	7			1	Ö	44.	0.00
72	4	18	5 2 1	Ø	Ø	29.	0.00
73	2	11 !	5 1	Ø	Ø Ø	19.	0.00
74	1	9	2 1	Ø	Ø	13,	0.00
75	1		1 1	Ø	0	9.	0.00
76	1	3 :	1	Ø	Ø	6.	0.00
77	Ø	Ø	L Ø	0	Ø Ø	1.	0.00
78	0	Ø G	9 0	0	Ø	0.	0.00

TABLE F1
CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS
FFAR CENTRE (UNBOXED)

RECORDER 308. ROCKET MOTOR CHANNEL 6

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C,PROB
1	1018	1030	948	1032	3504	2032	9564	1.00
2	1018	1030	948	1032	3504	2032	9564.	1.00
3		1030	948		3504	2032	9564.	1.00
4		1030	948	1032	3504	2032	9564.	1.00
5		1030	948	1032	3504	2032	9564.	1.00
6		1030	948	1032	3504	2031	9563.	1.00
7		1030	948	1032	3504	2025	9557.	1.00
8		1030	948	1032	3504	2021	9553,	1.00
9		1030	948		3504	2010	9542.	
10		1030		1032	3504	1990	9522.	
11		1030		1032	3504	1984	9516.	0.99
12		1030		1032	3504	1961	9493.	0,99
13		1030		1032	3503	1931	9462.	0.99
14		1030		1032	3496	1878	9402.	0.98
15		1030	948		3469	1807	9304.	0,97
16		1030	947		3456	1758	9241.	7 07
17	1018	1030	946	1031	3405	1628	9058.	0,95
18		1030	945	1017	3317	1424	8751.	0.91
19		1029	942	1006	3198	1209	8400.	0,88
20		1023	942	989	2981	1032	7970.	0.83
21	993	1018	942	965	2816	960	7694.	0.80
22	956	984	937	919	2483	846	7125.	
23	868	927	890	806	2112	772	6375,	0.67
24	734	802	707	627	1802	718	5390.	0.56
25	626	636	530	493	1588	663	4536.	0.47
26	591	58Ø	473	441	1506	635	4224.	0.44
27	531	527	407	366	1400	579	3810.	0,40
28	491	489	369	322	1294	533	3498.	0.37
29	458	456	338	297	1203	486	3238,	0.34
30	431	425	318	270	1121	437	3682.	0.31
31	418	417	308	255	1083	418	2899.	0,30
32	395	402	286	232	1015	374	2704.	0.28
33	373	384	267	211	950	316	2501.	0.26
34	347	359	237	195	894	265	2297.	
35	330	338	223	175	817	219	2102.	0.22
36	322	328	215	167	784	204	2020.	0.21
37	305	319	201	147	721	166	1859.	0.19
38	287	304	179	127	662	146	1705.	0.18
39	269	288	166	102	596	102	1523.	Ø.16
40	240	273	150	74	518	81	1336.	0.14
41	231	269	146	65	473	66	1250.	0,13
42	205	252	125	50	413	46	1091.	0.11
43	190	235	110	32	352	27	946.	0.10
44	164	214	90	18	290	13	789.	0.08
45	145	192	79	10	239	5	670.	0.07

TABLE F1 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS FFAR CENTRE (UNBOXED)

		RECORDER	30B.	ROCKET MOT	OR CHANNE	L 6	
DEG.	DEC	JAN FEE	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	131	174 75	8	207	4	599.	0.06
47	103	148 62	4	152	4 2	471.	0.05
48	80	123 51	. 2	105	Ø	361.	0.04
49	54	94 38		61	9	248.	0.03
50	36	68 24	1	30	Ø	159.	0.02
51	32	56 17		20		126.	0.01
52	16	41 13		10	Û	81.	0.00
53	6			5	Ø	44.	0.00
54	3	27 5 12 2	1	5	Ø	23.	0.00
55	1	7 2	1	4	Ø	13,	0.00
56	Ø	7 2	1	4	Ø	12.	0.00
57	Ø	1 0		4	Ø	6.	0.00
58	Ø	0 0		4	Ö	5.	0.00
59	0	0 0		4	Ú	5.	0.00
60	Ø	ØØ		4	Ø	5.	0.00
61	Ø	0 0	1	4	Ø	5.	0.00
62	Ø	0 0		4	Ø	5.	0.00
63	Ø	Ø	1	4	0	5.	0.00
64	Ø	Ø	1	4	Ø	5.	0.00
65	Ø	0 0	1	. 3	Ø	4.	0.00
66	Ø	0 0	Ø	3	Ø	3.	0.00
67	0	0 0	0	3	Ü	3.	0.00
68	0	0 0	0	3	Ø	3.	0.00
69	0	0 0		3	0	3.	0.00
70	0	0 0		3	Ø	3.	0.00
71	0	0 0		3	0	3.	0.00
72	0	0 0		3	Û	3.	0.00
73	Ø	0 0		Ø .	Ú	Ø.	0.00

TABLE G1

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS FFAR MOTOR SKIN (UNBOXED)

RECORDER 30B. ROCKET MOTOR CHANNEL 7

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1017	1032	948	1032	3500	2032	9561.	1.00
2	1017	1032	948	1032	3500	2032	9561.	1.00
3	1017	1032	948	1032	3500	2032	9561.	1.00
4	1017	1032	948	1032	3500	2032	9561.	1.00
5		1032		1032	3500	2032	9561.	1.00
6	1017	1032	948	1032	3500	2029	9558.	1.00
7	1016	1032	948	1032	3500	2025	9553.	1.00
8	1016	1032	948	1032	3500	2021	9549.	1.00
9	1016	1032	948	1032	3500	2011	9539.	1,00
10	1016	1032	948	1032	3500	1986	9514.	1.00
11	1016	1032	948	1032	3500	1981	9509.	0,99
12	1016	1032	948	1032	3500	1957	9485.	0.99
13	1016	1032	948	1032	3498	1921	9447.	0.99
14	1016	1032	948	1032	3487	1875	9388.	0.98
15	1016	1032	948	1032	3464	1794	9286.	9.97
16	1016	1032	947	1032	3449	1747	9223.	0,96
17	1016	1032	946	1031	3398	1606	9029.	0.94
18	1016	1031	945	1016	3297	1408	8713.	0.91
19	1014	1031	942	1005	3170	1201	8363.	0,87
20	1000	1024	942	987	2955	1028	7936.	0.83
21	992	1017	942	962	2802	956	7671.	0,80
22	952	981	937	915	2467	835	7087.	0.74
23	860	922	887	797	2099	774	6339.	0,66
24	727	801	705	624	1779	710	5346.	0.56
25	615	637	526	482	1560	664	4484.	0.47
26	576	584	471	418	1493	633	4175.	0.44
27	525	521	406	358	1367	584	3761.	0.39
28	485	472	368	318	1286	542	3471.	0.36
29	453	445	342	293	1202	498	3233.	0.34
30	426	425	317	264	1126	455	3011.	0.31
31	419	416	307	257	1095	432	2926.	0.31
32	393	399	278	235	1027	390	2722.	0.28
33	365	383	254	550	952	344	2518.	0,26
34	346	368	241	203	882	289	2329,	0.24
35	331	349	227	185	818	238	2148.	0.22
36	325	344	217	175	790	223	2074.	0.22
37	329	323	206	157	725	180	1900.	0.20
38	293	308	192	136	681	147	1757.	0.18
39	271	294	170	111	615	117	1578.	0.17
40	248	286	148	86	554	90	1412.	0.15
41	238	279	144	72	507	82	1322.	0.14
42	218	262 239	135	56	430	52	1153.	0.12
44	192	229	122	41	367	30	991.	0.10
45	169	205	107	27	308	19	859. 741.	0.09
75	148	200	74	21	259	14	/41.	0.08

TABLE G1 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

#### FFAR MOTOR SKIN (UNBOXED)

					no ron onem	( ONDORED)	,	
		RECO	RDER	308.	ROCKET M	OTOR CHANNE	L 7	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRIN	G WINTER	TOTAL	C.PROB
46	137	193	84	15	225	7	661,	0.07
47	108	169	68	9	170	2	526.	0.06
48	86	133	54	7	116	1	397.	0.04
49	64	106	47	4	76	1	298.	0.03
50	42	85	33	3	39	Ø	202.	0.02
51	35	73	27	2	27	Ø	164.	0.02
52	17	51	19	1	11	. 0	99.	0.01
53	10	35	6	1	4	Ø	56.	0.00
54	3	20	5	1	1	Ø	30.	0.00
55	2	12	1	1	Ø	Ö	16.	0.00
56	2	8	1	1	0	Ø	12.	0.00
57	1	5 2	Ø	1	Ø	Ø	7.	0.00
58	Ø	2	Ø	1	Ø	Ŭ Ŭ Ô	3.	0.00
59	Ø	1	e	1	Ø	Ø	2.	0.00
60	Ø	1	0	1	.0	Ú	2.	0.00
61	Ø	1	0	1	0	Ø	2,	0.00
62	Ø	1	0	1	0	0	2.	0.00
63	0	1	Ø	1	Ø	Ø	2.	0,00
64	Ø	1	Ø	1	Ø	Ø	2,	0.00
65	Ø	1	Ø	1	. 0	Ø	2.	0.00
66	Ø	1	Ø	1	Ø	Ø	2.	0.00
67	Ø	1	Ø	1	0	Ø	2.	0.00
68	0	1	Ø	1	0	Ø	2.	0.00
69	Ø	1	Ø	1	0	Ø	2.	0.00
70	Ø	1	Ø	1	Ø	Ø	2.	0,00
71	Ø	1	Ø	1	Ø	Ø	2,	0.00
72	Ø	Ø	Ø	1	0	Ø	1,	0.00
73	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
74	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
75	Ø	0	Ø	1	Ø	0	1.	0.00
76	Ø	Ø	Ø	1	Ø	Ü	1.	0.00
77	Ø	Ø	Ø	0	0	. 10	Ø.	0.00

TABLE H1
CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS
LINNET EXT. TOP (SAND)

TABLE H1 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

#### LINNET EXT. TOP (SAND)

		RECO	RDER	30B.	ROCKET MO	TOR CHANNEL	. 8	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	132	173	73	19	232	13	642.	0,07
47	114	155	65	10	191	8	543.	0.06
48	93	136	59	7	155	3 1	453.	0.05
49	76	115	47	5	121	i	365.	0.04
50	56	90	32	3	84	1	266.	0.03
51	52	76	30	1	70	Ø	229.	0.02
52	33	54	20	1	42	Ø	150.	0.02
53	Sø	45	11	Ø	17	Ø	93.	0.00
54	16	34	9	Ø	9	Ø	68.	0.00
55	8	27	5	0	7	Ø	47.	0,00
56	5	20	4	Ø	6	Ø	35.	0.00
57	. 2	13	1	Ø	6	Ø	22.	0.00
58	1	6	Ø	Ø	6	Ø	13.	0.00
59	1	4	Ø	Ø	5	Ø	10.	0.00
60	1	Ø	Ø	0	5	.0	6,	0.00
61	1	Ø	Ø	0	5	Ø	6.	0.00
62	1	0	Ø	Ø	5	Ø	6.	0.00
63	Ø	0	Ø	0	5	Ø	5.	0.00
64	Ø	0	0	. 0	5	Ø	5.	0.00
65	Ø	Ø	Ø	0	4	Ø	4.	0.00
66	0	Ø	Ø	Ø	3 3	Ø	3,	0.00
67	. 0	Ø	Ø	Ø	3	Ø	3.	0.00
68	0	Ø	0	Ø	3	Ø	3.	0.00
69	Ø	Ø	Ø	Ø	3	0	3.	0.00
7.0	0	Ø	0	Ø	3	Ø	3,	0,00
71	0	Ø	0	Ø	3	. 0	3.	0.00
72	Ø	Ø	0	0	3 3 3 3 3		3.	0.00
73	Ø	Ø	Ø	Ø	2	Ø	2.	0.00
74	Ø	0	0	Ø	1	0	1.	0.00
75	Ø	Ø	Ø	Ø	Ø	Ò	Ø.	0.00

TABLE J1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

LINNET PROP. SURFACE (SAND)

RECORDER 30B. ROCKET MOTOR CHANNEL 9

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C,PROB
1	1017	1030	948	1032	3506	2032	9565.	1.00
2	1017	1030	948	1032	3506	2032	9565.	1.00
3	1017	1030	948	1032	3506	2032	9565.	1.00
4	1017		948		3506	2032	9565.	1.00
5		1030			3506	2032	9565.	1.00
6		1030		1032	3506	2031	9564.	1.00
7		1030		1032	3506	2027	9559.	1.00
8		1030		1032	3506	2021	9553.	1.00
9		1030		1032	3506	2013	9545.	1,00
10	man and and	1030		1032	3506	1998	9530.	1.00
11	1016	1030	948	1032	35Ø6 35Ø5	1993 1975	9525. 9506.	1.00
13		1030	948	1032	3502	1942	9470.	0.99
14		1030		1032	3495	1895	9416.	0,98
15		1030		1032	3475	1833	9334.	0,98
16		1030	948		3463	1785	9274.	
17		1030	947		3417	1653	9095.	0,95
18	1016	1030	945	1025	3339	1467	8822.	0.92
19	1014	The second second	944	1.014	3224	1278	8504.	0.89
20	1002	1025	942	999	3029	1084	8081.	0.84
21	993	1018	942	980	2884	1008	7825.	0.82
22	962	989	937	926	2547	867	7228.	0.76
23	877	930	877	778	2178	772	6412.	81.67
24	746	814	680	604	1829	689	5350.	0.56
25	646	663	543	466	1619	591	4528.	0,47
26	607	619	483	407	1504	554	4174.	0.44
27	551	556	416	349	1371	479	3722.	0.39
28 29	508 459	5Ø8 466	368	307	1239	419 347	3349. 3006.	0.35
30	424	426	341 302	273 240	1120	280	2698.	Ø,31 Ø,28
31	407	416	289	226	1026 975	256	2569.	0,27
32	368	383	260	186	869	196	2262.	0.24
33	343	354	232	160	775	155	2019.	P. 21
34	315	330	213	131	695	114	1798.	0,19
35	294	307	189	105	609	87	1591.	9.17
36	279	300	179	91	576	69	1494.	0.16
37	254	280	156	66	501	45	1302.	0.14
38	230	257	136	43	423	23	1112.	0,12
39	201	235	115	31	344	10	936,	0.10
40	167	205	92	10	283	5	762.	0.08
41	153	194	84	6	252	4	693,	0.07
42	116	173	74	4	194	Ø	561.	0.06
43	96	139	61	2	139	Ø	437.	0.05
44	75	106	45	1	100	Ø	327.	0.03
49	55	80	30	Ø	59	Ö	224.	0.02

TABLE J1 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET PROP. SURFACE (SAND)

RECORDER 30B. ROCKET MOTOR CHANNEL 9

		WEOU	NUCK	000.	NOCKET MOT	OR CHAIN	,	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	40	71	27	Ø	46	Ø	184.	0.02
47	28	49	22	Ø	21	Ø	120.	0.01
48	21	35	17	Ø	7	Ø	80.	0.00
49	10	27	11	Ø	6	Ø	54.	0.00
50	5	21	4	Ø	5	Ø	35.	0.00
51	2	17		Ø	5	Ø	26.	0.00
52	1	12	2	Ø	5	. Ø	18.	0.00
53	1	6	Ø	Ø	5	Ø	12.	0.00
54	Ø	5	Ø	Ø	5 5	Ø	10.	0.00
55	Ø	2 Ø	Ø	Ø	5	Ø	7.	0.00
56	0	Ø	Ø	Ø	5	Ø	5.	0.00
57	Ø	Ø	Ø	Ø	5	Ø	5,	0.00
58	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
59	0	Ø	Ø	Ø	5	Ø	5.	0.00
60	Ø	Ø	Ø	Ø	5 5	Ø	5. 5.	0.00
61	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
62	Ø	Ø	Ø	0	5	Ø	5,	0.00
63	Ø	Ø	Ø	Ø	5	Ø	5,	0.00
64	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
65	0	Ø	Ø	Ø	. 3	Ø	3.	0.00
66	Ø	Ø	0	Ø	3	Ø	3.	0.00
67	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
68	Ø	Ø	Ø	0	3	Ø	3.	0.00
69	Ø	Ø	Ø	Ø	3 3 3	Ø	3,	0.00
70	Ø	Ø	Ø	0	3	Ø	3,	0.00
71	Ø	Ø	Ø	Ø		Ø	3.	0.00
72	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
73	0	Ø	Ø	Ø	3	Ø	3.	0.00
74	Ø	Ø	Ø	Ø	1	Ø	1.	0.00
75	Ø	Ø	Ø	0	Ø	U	Ø.	0.00

TABLE K1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

LINNET INT. PROP. CHARGE (SAND)

RECORDER 30B. ROCKET MOTOR CHANNEL 10

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1018	1030	948	1032	3506	2031	9565.	1.00
2	1018	1030	948	1032	3506	2031	9565.	1.00
3	1018	1030	948	1032	3506	2031	9565.	1,00
4	1018	1030	948	1032	3506	2031	9565.	1.00
5	1018	1030	948	1032	3506	2031	9565.	1.00
6	1018	1030	948	1032	3506	2031	9565.	1,00
7	1018	1030	948		3506	2027	9561.	1.00
8	1018	1030		1032	3506	2023	9557.	1.00
9	1018	1030	948	1032	3506	2012	9546.	1.00
10	1018	1030	948	1032	3506	2000	9534.	1.00
11	1018	1030	948	1032	3506	1,995	9529.	1.00
12	1018	1030	948	1232	3505	1972	9505.	0.99
13	1018	1030	948	1032	3503	1944	9475.	0.99
14	1018			1032	3496	1903	9427.	0.99
15	1018	1030	948	1032	3476	1852	9356.	0.98
16	1018	1030	948		3463	1812	9303.	
17	1018	1030	947 945	1032	3422	1685	9134. 8884.	0.95
18 19	1018		944		3351 .3240	1515 1316	8562.	Ø.93 Ø.90
20	1009		942	1004	3379	1131	8191.	0.86
21	1002	1019	942	987	2949	1045	7944.	Ø.83
22	975	999	939	942	2616	900	7371.	Ø.77
23	899	945	903	836	2258	807	6648.	0.70
24	775	845	737	658	1928	718	5661.	0,59
25	662	702	566	521	1687	621	4759.	0,50
26	624	633	512	456	1587	596	4408.	0.46
27	570	562	443	370	1422	545	3912.	0.41
28	516	516	390	329	1303	464	3518.	0,37
29	474	477	347	292	1178	403	3171.	0.33
30	435	440	317	264	1788	344	2888.	0.30
31	422	426	305	245	1040	319	2757.	0.29
32	392	396	277	221	942	256	2484.	0.26
33	360	363	253	191	860	205	2232.	0.23
34	336	343	224	169	781	155	2008.	0.21
35	309	319	207	148	701	131	1815.	0.19
36	297	312	196	137	670	117	1729.	0.18
37	277	289	174	110	600	84	1534.	
38	252	270	157	83	530	58	1350.	0.14
39	229	248	140	66	456	32	1171.	0.12
40	203	237	121	45	393	15	1014.	0.11
42	192	231	117	38	356	12	946.	0.10
43	142	185	106	25	291	7 2	649.	0.07
44	118	167	69	14	226 181	Ø	543	0,06
45	92	135	.59	5	135	Ø	426.	0.04
	, ,	100	,,	,	100		1201	0,04

TABLE K1 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET INT. PROP. CHARGE (SAND)

RECORDER 3ØB. ROCKET MOTOR CHANNEL 10 DEG. DEC FEB JAN MAR AUT-SPRING WINTER TOTAL C.PROB 46 83 120 53 3 117 0 376. 0.04 Ø 296. 47 98 45 85 66 2 0.03 219. 48 48 75 59 Ø 36 1 0.02 49 60 0 168. 41 25 0 42 0.02 Ø 50 121. 48 30 18 Ø 25 0.01 0 51 24 38 Ø 16 21 99. 0.01 65. 52 15 30 7 0 13 Ø 0.00 53 5 0 46. 8 24 9 Ø 0.00 2 5 5 5 5 Ø 29. 54 18 4 Ø 0.00 55 0 17. 1 10 Ø 0.00 9 Ø 14. 56 Ø Ø 0 0.00 Ø 9. 57 Ø 4 Ø Ø 0.00 3 55555553333333333 W 8. 58 0 Ø Ø 0.00 5. 59 0 Ø Ø 0.00 Ø 0.00 5, 60 Ø 0 Ø Ø 0.00 61 Ø Ø Ø Ø 5, 0.00 62 Ø Ø Ø Ø Ò 5, 0.00 5. 63 Ø Ø Ø Ø Ø 0.00 ø 5. 64 Ø Ø Ø Ø 0.00 Ø 3. 65 Ø Ø Ø Ø 0.00 Ø 3. 66 Ø Ø Ø Ø 0.00 Ø 3. 67 Ø 0 Ø Ø 0.00 Ø 3, 68 0 0 Ø 0 0.00 69 Ø 0 Ø Ø Ø 3, 0.00 0.00 3. 70 Ø Ø 0000 Ø 0.00 3, Ø Ø 71 0.00 Ø Ø 72 3. 0,00 Ø Ø 73 Ø Ø 0 3, 0.00 Ø 10 1. 74 Ø Ø Ø Ø 0.00 Ø 75 Ø Ø 0. Ø Ø 0.00

TABLE L1 CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET EXT. BOTTOM (SAND)

25.

0.00

TABLE L1 (cont.)

#### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET EXT. BOTTOM (SAND)

RECORDER 308. ROCKET MOTOR CHANNEL 11 DEG. DEC JAN FEB MAR AUT-SPRING WINTER TOTAL C.PROB 12 18. Ø Ø 0.00 46 1 1 9 1 14. 47 3 Ø Ø 0.00 1 2 7 Ø 48 Ø 1 0.00 11. 3 Ø 5, 1111111111111111 49 Ø Ø 0.00 1 3 5. 1 Ø 50 Ø Ø 0,00 3 Ø 5. 51 Ø Ø 0.00 52 Ø 2 1 0 Ø 0.00 53 Ø 1 Ø Ø 3. 0.00 1 54 Ø 1 9.2.0 3. Ø 0.00 Ø 3. 55 0 0.00 56 Ø 1 Ø 3, 0.00 1 57 Ø Ø 1 Ó 3. 0,00 Ø 58 Ø 1 Ø 0.00 1 3. 1 0 59 Ø Ø 1 3, 0.00 Ø 1 Ø 60 3, 0.00 Ø 1 61 Ø Ø 1111 3. 0.00 Ø 0,00 62 Ø 1 Ø 3. 1 3. Ø Ď 63 8888 0.00 Ø Ø 3, 64 0.00 0.0 111 2. 1 65 0,00 Ø Ø 0.00 66 Ø 1 67 Ø 1 Ø 0.00 2, 0.00 1 2. Ø 68 Ø Ø 0.00 1 Ø Ø 2, 69 1 0 0.00 70 Ø 1 ø 2, Ø 0.00 1 Ø Ø 1 Ø 2. 71 0 1 0.00 Ø Ø Ø Ø 1. 0.00 72 Ø Ø 73 Ø Ø Ø 1 Ö 1. 0.00 Ø 74 0 0 Ø Ø Ò 1. 0,00 Ø 75 Ø 0 0.00 1 Ø ø Ø Ø

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0.00

0.00

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TABLE M1
CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS
ASROC CENTRE (BOXED)

ROCKET MOTOR CHANNEL 13

RECORDER 30B.

TABLE M1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

ASROC CENTRE (BOXED)

		RECO	RDER	30B.	ROCKET MOT	OR CHANNE	L 13	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	Ø	4	Ø	Ø	5	Ø	9,	0.00
47	0	Ø	Ø	Ø	5	Ø	5.	0.00
48	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
49	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
50	Ø	Ø	Ø	0	5	Ø	5.	0.00
51	Ø	Ø	Ø	Ø	5	Ø	5.	0.00
52	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
53	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
54	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
55	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
56	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
57	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
58	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
59	Ø	Ø	0	0	4	Ø	4.	0.00
60	Ø	Ø	Ø	0	4	Ö	4.	0.00
61	Ø	Ø	Ø	Ø	4		4.	0.00
62	Ø	Ø	Ø	Ø	4	<b>D</b>	4.	0.00
63	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
64	Ø	Ø	0	Ø	4	Ø	4.	0.00
65	Ø	Ø	Ø	. 0	3	Ø	3.	0.00
66	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
67	. 0	Ø	Ø	Ø	3 3 3 3	Ø	3,	0.00
68	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
69	Ø	Ø	Ø	Ø		Ø	3,	0.00
7.0	Ø	Ø	Ø	Ø	3 3 3	Ø	3,	0.00
71	Ø	Ø	Ø	0	3	Ø	3.	0.00
72	Ø	Ø	Ø	Ø	3	. 0	3,	0,00
73	Ø	Ø	Ø	Ø	3	0	3.	0.00
74	Ø	Ø	Ø	0	3	Ø	3.	0.00
75	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
76	Ø	Ø	Ø	Ø	5	Ø	2.	0.00
. 77	Ø	Ø	Ø	Ø	1.	Ø	1.	0.00
78	Ø	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

TABLE N1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

ASROC MOTOR SKIN (BOXED)

		RECO	RDER	30B.	ROCKET MO	TOR CHANNE	L 14	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C,PROB
1	1015	1029	947	1033	3505	2031	9560.	1.00
2	1015	1029	947	1033	3505	2031	9560.	1.00
3	1015	1029	947	1033	3505	2031	9560.	1.00
4	1015	1029	947	1033	35Ø5	2031	9560.	1.00
5	1015	1029	947	1033	3505	2031	9560.	1.00
6	1015	1029	947	1033	3505	2031	9560.	1.00
7	1015		947	-	3505	2031	9560.	1,00
8	1015		947		3505	2030	9559.	1.00
9	1015		947		3505	2024	9553.	1.00
10	1015	1029	947		3505	5050	9549.	1,00
11	1015	1029	947		3505	2017	9546.	1.00
12	1015	1029	947	1033	3505	2005	9534.	1.00
13	1015		947		3505	1990	9519.	1.00
14	1015		947		3505	1964	9493.	0.99
15	1015		947		3504	1921	9449.	0,99
16	1015		947		3502	1886	9412.	0,98
17	1015	1029	947		3489	1818	9331.	0.98
18 19	1015	1029	946		3458 3404	1670 1503	9152. 8927.	Ø.96 Ø.93
20	1015		944		3300	1292	8600.	0.90
21	1014			1015	3236	1183	8419.	0.88
22	1004		942	987	2986	1023	7969.	0,83
23	986	1015	937	928	2716	903	7485.	0.78
24	934	990	877	817	2352	801	6771.	0,71
25	836	898	757	642	2018	724	5875.	Ø.61
26	779	837	694	568	1864	685	5428.	0.57
27	682	729	583	448	1646	610	4696.	0.49
28	604	639	486	377	1477	558	4141.	0.43
29	551	577	428	338	1362	504	3760.	0.39
30	498	520	386	301	1247	452	3404.	0.36
31	482	494	365	293	1193	433	3260.	0.34
32	444	458	333	267	1102	382	2986.	0.31
33	408	434	296	246	1021	321	2726.	0.29.
34	375	400	279	214	930	268	2466.	Ø.26
35	348	374	253	195	865	222	2257.	0.24
36	338	361	242	180	826	201	2148.	0,22
37	317	342	225	161	763	170	1978.	0.21
38	301	324	207	136	696	139	1803.	0.19
39	283	301	185	118	621	113	1621.	0.17
40	253	290	168	96	558	93	1458.	0.15
41	243	281 270	158	88	528	81	1379. 1236.	0.14
43	194	253	147	71 53	470 400	58 42	1074.	Ø.13 Ø.11
44	170	232	116	41	345	24	928.	0,10
45	147	208	103	31	290	15	794.	0.08
	441		+00	21	270	**	,,,,	0100

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TABLE N1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS
ASROC MOTOR SKIN (BOXED)

		RECO	RDER	30B.	ROCKET M	TOTOR CHANNE	L 14	*
DEG,	DEC	JAN	FEB	MAR	AUT-SPRIM	IG WINTER	TOTAL	C.PROB
46	134	195	98	29	262	13	731.	0,08
47	112	174	82	22	198	7	595.	0.06
48	90	150	66	14	148	3 1	471.	0.05
49	77	126	56	8	109	1	377.	0.04
50	58	103	50	3	70	Ø	284.	0.03
51	48	96	45	2	57	Ø	248.	0.03
52	28	76	31	1	26	Ø	162.	0.02
53	20	57	20	0	7	Ø	104.	0.01
54	10	41	16	0	5	Ø	72,	0.00
55	5	28	11	0	4	Ø	48.	0.00
56	1	22	7	Ø	4	Ø	34.	0.00
57	Ø	14	3	Ø	4	Ø	21.	0.00
58	. 0	7	1	Ø	4	Ø	12.	0.00
59	0	3	Ø	Ø	4	Ø Ø Ø	7.	0.00
60	0	3	Ø	Ø	4	Ø	7.	0.00
61	0	1	0	Ø	4	Ø	5.	0.00
62	0	Ø	Ø	Ø	4	Ø	4.	0.00
63	Ø	Ø	Ø	Ø	4	Ø Ø Ø	4.	0.00
64	0	Ø	0	Ø	4	Ø	4.	0.00
65	Ø	Ø	0	. 9	3	Ø	3.	0.00
66	0	0	0	0	3 3 3 3 3 3 3	Ø	3.	0.00
67	. Ø	Ø	0	Ø	3	. 0	3,	0.00
68	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
69	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
7.0	Ø	Ø	0	Ø	3	U	3,	0.00
71	0	Ø	Ø	Ø	3	Ø	3.	0.00
72	Ø	Ø	Ø	Ø		. 0	3,	0.00
73	0	Ø	Ø	Ø	3	Ø	3.	0,00
74	Ø	Ø	Ø	0	3	Ø	3,	0.00
75	Ø	Ø	Ø	Ø	1	Ø	1.	0.00
76	Ø	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

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TABLE 01

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

ASROC HALFWAY BET. SKIN AND BOX

RECORDER 30B. ROCKET MOTOR CHANNEL 15

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1015	1029	947	1033	3505	2031	9560.	1.00
2		1029	947	1233	3505	2031	9560.	1.00
3		1029		1033	3505	2031	A.F	
4		1029		1033	3505	2031	9560.	1.00
5		1029		1033	3505	2031	9560.	1,00
6		1029		1033	3505	2031	9560.	1.00
7		1029		1033	3505	2028		
8		1029		1033	3505	2026		
9				1033		2021	AFER	4 44
		1029			3505		9550,	1.00
10		1029		1033	3505	2010	9539.	1.00
11		1028		1033	3505	2006	9534.	
12		1028		1033	3505	1990	9518.	1.00
13		1028		1033	3505	1964	9492.	0.99
14		1028		1033	3504	1929	9456.	0.99
15		1028		1033	3498	1862	9383.	0.98
16		1028		1033	3488	1828	9339.	0.98
17	1015	1028	947	1033	3458	1729	9339. 9210. 8990.	0.96
18	1015	1028	946	1031	34Ø8	1562	8990.	0,94
19	1015	1028	944	1023	3332	1376	8718.	0.91
20	1012	1026	942	1011	3182	1184	8357.	
21			941		3075	1102	04 5 6	0.85
22	993		940	963	2804	966	7685.	0.80
23	952	992	924		2485	874	7118,	
24	870	938	829		2141	793	6322.	
25	758	821	692	592	1843	735	5441.	
26	695	749	624		1737	712	5039.	
27	621	651	518	419	1563	661		
28	562	576	448	374	1444	614	4433.	0.42
29	513	532	397	339	1357	569	3707.	0,39
30	474	492	353	313	1268	521	3421.	0.36
31		475				496	3293.	
	456	452	343	300	1223	461	3293.	0,34
32	432		321	273	1158		3097.	
33	408	419	303	252	1094	417	2893,	
34	382	394	284	240	1035	381	2716.	0.28
35	361	379	267	219	977	336	2539.	0.27
36	353	371	260	209	950	315	2458.	0.26
37	330	348	245	198	892	273	2286.	0.24
38	316	338	231	180	834	245	2142.	
39	306	327	213	164	775	209	1994.	0.21
40	292	317	204	150	733	175	1871.	0.20
41	283	310	198	142	706	163	1802.	0.19
42	273	297	185	118	638	129	1640.	0.17
43	248	283	171	99	587	104	1492.	0,16
44	228	270	160	85	536	86	1365.	0.14
45	209	254	144	71	473	68	1219.	0.13
			- '					

TABLE 01 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS ASROC HALFWAY BET. SKIN AND BOX

RECORDER 308. ROCKET MOTOR CHANNEL 15

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	202	247	136	64	434	55	1138.	0.12
47	180	234	122	58	399	38	1031.	0.11
48	152	220	111	47	336	28	894.	0,09
49	139	209	99	38	280	19	784.	0,08
50	114	188	87	29	220	15	653.	0.07
51	104	182	86	26	200	12	610.	0.06
52	84	157	76	17	165		506.	0.05
53	70	140	60	11	121	3	405.	0,04
54	49	113	51	8	80	i	302.	0.03
55	40	97	37	5	54	7 3 1	234.	0.02
56	34	91	34	4	45	ē	208.	0.02
57	24	68	28	3	22		145.	0.02
58	14	55	21	1	11	Ø	102.	0.01
59	8	40	15	ø	4	Ñ	67.	0.00
60	4	33	12	ø	4	Ø	53.	0.00
61	3	29	11	Ø	4	Ø	47.	0.00
62	ø	20	7	ø	4	ŭ	31,	0.00
63	ø	11		Ø	4		17.	0.00
64	ø	4	2	Ø		9 9 9	8.	0.00
65	ø	2	õ	Ø	3	ú	5,	0,00
66	ø	ī	ø	Ø	3	ġ	4.	0.00
67	ø	ē	Ø	Ø	7	Ø	3,	0.00
68	Ø	ø	Ø	Ø	3	Ø	3,	0.00
69	ø	Ø	ø	Ø	7	й.	3,	0,00
70	Ø	ø	Ø	Ø	7	ä	3,	0,00
71	Ø	Ø	Ø	Ø	3 3 3 3 3 3 3	9 · · · · · · · · · · · · · · · · · · ·	3.	0.00
72	ø	Ø	Ø	Ø	2	â	2.	0,00
73	Ø	Ø	Ø	Ø	Ø	á	Ø.	0.00
, 0			0	0	U	~	υ,	0,00

TABLE P1

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS ASROC OUTER CASE (BOXED)

RECORDER 308. ROCKET MOTOR CHANNEL 16

					MONTH INC.	<b>4</b> 1. <b>4</b> 1		
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1015	1030	947	1034	3502	2031	9559.	1.00
2		1030	947		3502	2031	9559.	1.00
3		1030	947		3502	2031	9559.	1.00
4	1015	1030	947	A STATE OF THE STA	3502	2031	9559.	1,00
5		1030	947	CITE OF STREET	3502	2026	9554.	1.00
6	100	1030	947		3502	2024	9552.	1.00
7		1030	947		3502	2018	9545.	1.00
8		1030	947	1034	3502	2009	9536.	1,00
9		1030	947		3502	1992	9519.	1,00
10		1030	947		3502	1976	9503.	0.99
11		1030	947		3502	1967	9494.	0.99
12		1030		1034	3501	1928	9454.	0.99
13		1030	947		3497	1878	9400.	0.98
14		1030	947		3475	1830	9330.	0,98
15		1030	947	1034	3443	1734	9202.	0,96
16		1030	946	1033	3415	1686	9124.	0.95
17		1030	945	1025	3347	1541	8902.	
18		1027	942	1011	3242	1372	8607.	0.90
19		1025	941	1002	3084	1184	8242.	0.86
20	991	-	940	982	2861	1020	7811.	0.82
21 .		1009	939	959	2718	958	7562.	0.79
22	926	964	933	917	2424	848	7012.	
23	838	900	900	809	2092	797	6336.	0.66
24	715	792	781	657	1791	763	5499.	0,58
25	622	654	612	524	1599	719	4730.	0.49
26	579	600	544	472	1532	704	4431.	0.46
27	530	537	474	393	1436	668	4038.	0.42
28	486	489	425	358	1349	637	3744.	0.39
29	460	461	391	333	1290	607	3542.	0.37
30	438	438	367	311	1232	575	3361.	0.35
31	424	424	357	300	1213	560	3278.	0.34
32	405	415	338	287	1161	530	3136.	0.33
33	390	397	328	268	1109	494	2986.	0.31
34	376	385	313	251	1063	459	2847.	0.30
35	362	375	301	234	1032	428	2732.	0.29
36	357	368	296	230	1013	418	2682.	0.28
37	344	355	287	221	975	391	2573.	0.27
38	331	342	276	208	937	359	2453.	0.26
39	320	327	266	197	891	327	2328.	0,24
40	314	321	255	184	852	302	2228,	0.23
41	308	318	250	179	837	289	2181.	Ø.23
42	295	306	246	169	782	263	2061.	0.22
43	284	302	237	159	741	234	1957.	0.20
44	269	291	230	144	688	211	1833.	0.19
45	260	280	221	135	652	184	1732.	0,18

TABLE P1 (cont.)

#### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS ASROC OUTER CASE (BOXED)

		RECO	RDER	30B.	OR CHANN	CHANNEL 16		
DEG,	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C,PROB
46	257	276	217	129	637	169	1685.	0.18
47	243	271	209	116	589	158	1586.	0.17
48	230	262	197	107	551	143	1490.	0.16
49	212	254	188	95	515	125	1389.	0.15
50	200	247	176	80	481	104	1288.	0.13

		07/				4.0		
46	257	276	217	129	637	169	1685.	0.18
47	243	271	209	116	589	158	1586.	0.17
48	230	262	197	107	551	143	1490.	0.16
49	212	254	188	95	515	125	1389.	0,15
50	200	247	176	80	481	104	1288.	0.13
51	194	243	170	78	461	97	1243.	0.13
52	181	233	157	72	426	84	1153.	0.12
53	172	225	149	64	392	71	1073.	0,11
54	160	210	142	57	351	55	975.	0.10
55	156	202	136	53	315	45	907.	0.09
56	144	197	126	50	300	40	857.	0.09
57	134	184	115	43	264	35	775.	0.08
58	123	167	108	38	234	27	697.	0.07
59	98	152	96	35	202	22	605.	0.06
60	84	139	81	29	170		519.	0,05
61	79	129	81	26	156	16 13	484.	0.05
62	65	124	72	19	138	10	428,	0.04
63	54	113	62	15	105	7	356.	0.04
64	47	100	56	12	80		299,	0.03
65	41	88	48	10	61	1	249.	0.03
66	35	84	45	10	54	ī	229.	0,02
67	. 25	76	39	6	41	ø	187.	0.02
68	19	66	32	4	26	Ø	147.	0.02
69	16	53	27		14	Ø	113.	0.01
7.0	8	43	18	3	6	ø	78.	0.00
71	8	35	15	3 3 2	5	Ø	65.	0.00
72	3	25	10	1	5 2	. 0	41.	0.00
73	3 3 2 1 1	21	9	i	i	Ø	35	0.00
74	9	14	5	î	ø		22,	0.00
75	1	8	5		ø	0	12.	0.00
76	1		5 2 1	1	ø		9	0.00
77	ē	6 5 2	ø	ø	Ø	Ø	5,	0.00
78	ø	2	Ø	ø	Ø	u	2,	0,00
79	Ø	ø	Ø	ø	Ø	Ø	ø.	0.00
,,	0			0	U	ž.		0,00

TABLE 01

### CUMULATIVE PROBABILITY DISTRIBUTION FOR HOCKET MOTOR TEMPS SPARROW FIBREGLASS SKIN (UNBOXED)

RECORDER 30B. ROCKET MOTOR CHANNEL 17

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1014	1030	947	1032	3508	2031	9562.	1.00
2		1030	947		3508	2031	9562.	1.00
3		1030		1032	3508	2031	9562.	1.00
4		1030	947	1032	3508	2026	9557.	1.00
5	1014	1030	947		3508	2024	9555.	1.00
6		1030		1032	3508	2019	9550.	1,00
7		1030		1032	3508	2010	9541.	1.00
8		1030		1032	3508	1993	9524.	1.00
9 10		1030		1032	35Ø8 35Ø8	1981 1960	9512. 9491.	Ø.99 Ø.99
11		1030	947		3508	1940	9471.	0.99
12	1014		947		3504	1903	9430.	0.99
13		1030		1032	3495	1845	9363.	0,98
14		1030	947		3467	1787	9277.	0,97
15	1014	1030		1032	3420	1676	9118.	0,95
16		1030		1031	3391	1613	9025.	0.94
17	1014	1027	944	1017	3303	1458	8763.	0.92
18	1012	1025	942	1004	3173	1239	8395.	0.88
19	993	1022	941	987	2988	1081	8012.	0.84
20	981 955	1002	940	961 940	2730	930	7544. 7270.	0.79
21	875	938	922	871	2562 2231	886 818	6655.	0.76 0.70
23	761	844	825	740	1896	777	5843.	0.61
24	637	708	629	596	1662	753	4985.	0.52
25	555	568	483	476	1514	720	4316.	0.45
26	525	517	437	433	1464	707	4083.	0.43
27	484	476	394	379	1382	680	3795.	0.40
28	458	450	367	347	1316	653	3591.	0.38
29	437	432	342	318	1259	629	3417.	0.36
30	416	408	323	302	1215	596	3260.	0.34
31 32	412 385	4Ø2 389	314 300	293 278	1188 1147	585 547	3194. 3046.	Ø.33 Ø.32
33	370	376	291	261	1106	527	2931.	0.31
34	357	362	278	249	1060	496	2802.	0.29
35	344	353	267	235	1019	470	2688.	0,28
36	338	347	257	230	1007	452	2631.	0.28
37	327	331	246	217	964	425	2510.	0.26
38	315	318	236	205	914	393	2381.	0.25
39	308	3Ø8	222	194	869	360	2261.	0,24
40	299	301	213	179	834	337	2163.	0.23
41	291 275	294	208	171	816	323 293	2103.	0.22
42	259	288	204	158	762 719	267	1980.	0.21
44	241	272	185	139	689	243	1769.	0.19
45	233	267	173	130	653	214	1670.	0.17
			-, 0	-00		-		

TABLE Q1 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW FIBREGLASS SKIN (UNBOXED)

		RECO	RDER	30B.	ROCKET MOT	OR CHANNE	L 17	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	230	263	168	126	625	199	1611.	0.17
47	219	254	155	112	581	177	1498.	0,16
48	211	242	142	101	537	157	1390	0.15
49	198	233	127	89	500	135	1282,	0,13
50	182	215	118	75	454	117	1161.	0,12
51	174	211	117	70	439	109	1120.	0.12
52	158	198	107	59	387	87	996.	0.10
53	143	181	95	53	347	67	886.	0.09
54	130	169	90	42	300	53	784.	0.08
55	102	158	84	39	250	41	674.	0.07
56	96	152	79	36	220	30	613.	0.06
57	82	135	70	28	175	15	508.	0.05
58	72	119	56	22	141	13	423.	0.04
59	55	100	48	15	104	7	329.	0.03
60	40	82	41	9	62	1	235.	0.02
61	32	73	39	7	45	1	197.	0.02
62	21	61	30	4	28	Ø	144.	0.02
63	10	45	24	3	19	Ø	101.	0.01
64	8	34	17	2 2	10	Ø	71.	0.00
65	7	24	12	2	5	Ø	50.	0.00
66	6	21	9	2	3	Ø	41.	0.00
67	1	13	5	1	3	Ø	23,	0.00
68	1	7	0	Ø	3	Ø	11.	0,00
69	Ø	1	Ø	Ø	3	Ø	4.	0,00
70	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
71	Ø	Ø	0	Ø	3 3 3 3	Ø Ø	3.	0.00
72	Ø	Ø	Ø	Ø	1		1.	0.00
73	Ø	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

TABLE R1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW AL SKIN (UNBOXED)

RECORDER 30B. ROCKET MOTOR CHANNEL 18

					HOOKE! HO!	<b> </b>		
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1015	1030	947	1032	3507	2031	9562.	1,00
2		1030		1032	3507	2031	9562.	1.00
3	1015	1030	947	1032	3507	2031	9562,	1,00
4	1015	1030	947	1032	3507	2031	9562.	1,00
		1030	947	1032	3507	2028	9559.	
5	1015	1030	947					1.00
6	1015				3507	2027	9558.	1.00
7	1014	1030		1032	3507	2022	9552.	1,00
8		1030		1032	3507	2014	9542.	1.00
9		1030	947		3507	1994	9522.	1.00
10		1030	947	1032	3507	1981	9509.	0.99
11	1012	1030	947	1032	3507	1970	9498.	0,99
12	1012		947	1032	3507	1937	9465.	0.99
13		1030	947		3502	1892	9415.	0.98
14	1012	1030	947	1032	3484	1838	9343.	0.98
15		1030	947	1032	3454	1757	9232.	0.97
16	1012	1030	946	1032	3431	1698	9149.	0.96
17	1012	1030	945	1026	3373	1550	8936.	0.93
18	1011	1029	943	1012	3269	1343	8607.	0.90
19	1007	1026	941	999	3109	1135	8217.	0,86
20	991	1018	941	980	2880	966	7776.	0.81
21	982	1015	939	952	2712	902	7502.	0,78
22	933	969	934	897	2377	808	6918.	0.72
23	830	895	878	777	1984	757	6121.	0.64
24	697	773	678	597	1682	710	5137.	0.54
25	585	603	500	463	1494	666	4311.	0.45
26	545	551	443	413	1424	641	4017.	0.42
27	493	490	377	343	1308	595	3606.	0.38
28	452	445	343	306	1227	568	3341.	Ø,35
29	422	422	319	279	1162	517	3121.	Ø.33
30	392	399	294	259		469	2901.	0.30
31	380	391	287	246	1088	456	2824.	0.30
32	360	368	268	230	1264	406	2629.	
33	334	346	249		997			0.27
				215	940	360	2444.	0.26
34	322	326	233	186	871	315	2253,	0.24
35	310	314	219	170	8Ø8	269	2090.	0.22
36	299	309	214	163	781	246	2012.	0.21
37	279	294	204	142	723	200	1842.	0.19
38	261	284	182	128	665	158	1678.	0.18
39	239	272	161	97	582	128	1479.	0.15
40	211	250	143	87	494	100	1285.	0.13
41	201	243	136	77	456	89	1202.	0.13
42	167	224	118	62	388	62	1021.	0.11
43	141	202	98	39	313	36	829.	0.09
44	123	178	86	25	234	21	667.	0.07
45	89	157	77	15	159	13	510.	0,05

TABLE R1 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW AL SKIN (UNBOXED)

RECORDER 30B. ROCKET MOTOR CHANNEL 18

46       74       134       68       12       130       7       425.         47       47       104       50       9       84       6       300.         48       30       71       35       3       48       1       188.         49       23       57       27       2       28       1       138.         50       10       39       16       2       15       0       82.         51       8       35       14       1       14       0       72.         52       4       24       7       0       8       0       43.         53       2       13       2       0       5       0       222.         54       1       7       1       0       4       0       43.       22.         55       1       3       0       0       4       0       4       0       4.       0       6.         57       0       0       0       0       4       0       4.       0       4.       0       4.       0       4.       0       4.       0       4.       0	
47       47       104       50       9       84       6       300       .       188       .       188       .       .       188       .       .       .       188       .	C.PROB
49       23       57       27       2       28       1       138         50       10       39       16       2       15       0       82         51       8       35       14       1       14       0       72         52       4       24       7       0       8       0       43         53       2       13       2       0       5       0       22         54       1       7       1       0       4       0       13         55       1       3       0       0       4       0       4         56       0       2       0       0       4       0       4         57       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         60       0       0       0       0       4       0       4         61       0       0       0       0       0       4       0 </td <td>0.04</td>	0.04
49       23       57       27       2       28       1       138         50       10       39       16       2       15       0       82         51       8       35       14       1       14       0       72         52       4       24       7       0       8       0       43         53       2       13       2       0       5       0       22         54       1       7       1       0       4       0       13         55       1       3       0       0       4       0       4         56       0       2       0       0       4       0       4         57       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         60       0       0       0       0       4       0       4         61       0       0       0       0       0       4       0 </td <td>0,03</td>	0,03
49       23       57       27       2       28       1       138.         50       10       39       16       2       15       0       82.         51       8       35       14       1       14       0       72.         52       4       24       7       0       8       0       43.         53       2       13       2       0       5       0       22.         54       1       7       1       0       4       0       13.         55       1       3       0       0       4       0       4         56       0       2       0       0       4       0       4         57       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         69       0       0       0       0       0       4       0       4         61       0       0       0       0       0       <	0.02
51       8       35       14       1       14       0       72         52       4       24       7       0       8       0       43         53       2       13       2       0       5       0       22         54       1       7       1       0       4       0       13         55       1       3       0       0       4       0       8         56       0       2       0       0       4       0       6         57       0       0       0       0       4       0       4       0         58       0       0       0       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       0       0       0       0       0       0       0       0       0       0       0       0	0.01
51       8       35       14       1       14       0       72         52       4       24       7       0       8       0       43         53       2       13       2       0       5       0       22         54       1       7       1       0       4       0       13         55       1       3       0       0       4       0       8         56       0       2       0       0       4       0       6         57       0       0       0       0       4       0       4       0         58       0       0       0       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       4       0       0       0       0       0       0       0       0       0       0       0       0       0	0.00
52       4       24       7       0       8       0       43.         53       2       13       2       0       5       0       22.         54       1       7       1       0       4       0       13.         55       1       3       0       0       4       0       8.         56       0       2       0       0       4       0       6.         57       0       0       0       0       4       0       4.         58       0       0       0       0       4       0       4.         59       0       0       0       0       4       0       4.         60       0       0       0       0       4       0       4.         60       0       0       0       0       4       0       4.         61       0       0       0       0       4       0       4.         62       0       0       0       0       4       0       4.         63       0       0       0       0       3       0       3	0.00
53       2       13       2       0       5       0       22         54       1       7       1       0       4       0       13         55       1       3       0       0       4       0       8         56       0       2       0       0       4       0       6         57       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         59       0       0       0       0       4       0       4         60       0       0       0       0       4       0       4         60       0       0       0       0       4       0       4         61       0       0       0       0       4       0       4         62       0       0       0       0       4       0       4         63       0       0       0       0       0       4       0       4         64       0       0       0       0       3       0       3 </td <td>0.00</td>	0.00
55       1       3       0       0       4       0       6.         56       0       2       0       0       4       0       6.         57       0       0       0       0       4       0       4.         58       0       0       0       0       4       0       4.         59       0       0       0       0       4       0       4.         60       0       0       0       0       4       0       4.         61       0       0       0       0       4       0       4.         62       0       0       0       0       4       0       4.         63       0       0       0       0       4       0       4.         64       0       0       0       0       4       0       4.         65       0       0       0       0       3       0       3.         66       0       0       0       0       3       0       3.         67       0       0       0       0       3       0       3.	0.00
55       1       3       0       0       4       0       6.         56       0       2       0       0       4       0       6.         57       0       0       0       0       4       0       4.         58       0       0       0       0       4       0       4.         59       0       0       0       0       4       0       4.         60       0       0       0       0       4       0       4.         61       0       0       0       0       4       0       4.         62       0       0       0       0       4       0       4.         63       0       0       0       0       4       0       4.         64       0       0       0       0       4       0       4.         65       0       0       0       0       3       0       3.         66       0       0       0       0       3       0       3.         67       0       0       0       0       3       0       3.	0,00
56       0       2       0       0       4       0       6.         57       0       0       0       0       4       0       4.         58       0       0       0       0       4       0       4.         59       0       0       0       0       4       0       4.         60       0       0       0       0       4       0       4.         61       0       0       0       0       4       0       4.         61       0       0       0       0       4       0       4.         62       0       0       0       0       4       0       4.         63       0       0       0       0       4       0       4.         64       0       0       0       0       4       0       4.         65       0       0       0       0       3       0       3.         66       0       0       0       0       3       0       3.         67       0       0       0       0       3       0       3.	0.00
57       0       0       0       0       4       0       4         58       0       0       0       0       4       0       4         59       0       0       0       0       4       0       4         60       0       0       0       0       4       0       4         61       0       0       0       0       4       0       4         62       0       0       0       0       4       0       4         63       0       0       0       0       4       0       4         64       0       0       0       0       4       0       4         65       0       0       0       0       3       0       3         66       0       0       0       0       3       0       3         67       0       0       0       0       3       0       3         68       0       0       0       0       3       0       3         70       0       0       0       0       3       0       3 <t< td=""><td>0.00</td></t<>	0.00
58       Ø       Ø       Ø       Ø       4       Ø       4         59       Ø       Ø       Ø       Ø       A       Ø       A         60       Ø       Ø       Ø       Ø       A       Ø       A         61       Ø       Ø       Ø       Ø       A       Ø       A         62       Ø       Ø       Ø       Ø       A       Ø       A         63       Ø       Ø       Ø       Ø       A       Ø       A         64       Ø       Ø       Ø       Ø       A       Ø       A         65       Ø       Ø       Ø       Ø       A       Ø       A         66       Ø       Ø       Ø       Ø       Ø       A       Ø       A         67       Ø       Ø       Ø       Ø       Ø       A       Ø       A       A       Ø       A <t< td=""><td>0.00</td></t<>	0.00
59       Ø       Ø       Ø       Ø       4       Ø       4         60       Ø       Ø       Ø       Ø       A       Ø       A         61       Ø       Ø       Ø       Ø       A       Ø       A         62       Ø       Ø       Ø       Ø       A       Ø       A         63       Ø       Ø       Ø       Ø       A       Ø       A         64       Ø       Ø       Ø       Ø       A       Ø       A         65       Ø       Ø       Ø       Ø       3       Ø       3         66       Ø       Ø       Ø       Ø       3       Ø       3         67       Ø       Ø       Ø       Ø       3       Ø       3       Ø         68       Ø       Ø       Ø       Ø       Ø       3       Ø       3       Ø         69       Ø       Ø       Ø       Ø       Ø       Ø       3       Ø       3       Ø       3       Ø       3       Ø       3       Ø       3       Ø       3       Ø       3       Ø       3	0.00
60 0 0 0 0 0 4 0 4 0 4 6 6 6 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00
61	0,00
64	0.00
64	0.00
65	0.00
66	0.00
67	0.00
	0.00
	0,00
	0.00
	0.00
	0.00
	0.00
	0.00
	0.00
75 0 0 0 0 2 0 2,	0.00
	0.00
	0.00
77 0 0 0 0 1 0 1.	0.00
78 0 0 0 0 1 0 1.	0.00
79 0 0 0 0 0 0 0.	0,00

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TABLE S1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW CENTRE (UNBOXED)

TABLE S1 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW CENTRE (UNBOXED)

		RECO	RDER	3ØB.	ROCKET MOT	OR CHANNE	L 19	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
47	Ø	Ø	Ø	0	4	Ø	4.	0.00
48	Ø	Ø	Ø	Ø	4	Ø	4,	0.00
49	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
50	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
51	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
52	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
53	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
54	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
55	Ø	Ø	0	Ø	4	Ø	4.	0.00
56	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
57	Ø	Ø	Ø	0	4	Ø	4.	0,00
58	Ø	Ø	Ø	Ø	4	Ø	4.	0,00
59	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
60	Ø	Ø	Ø	Ø	4	Ŵ	4.	0.00
61	Ø	Ø	Ø	Ø	4	Ø	4.	9.00
62	Ø	Ø	0	Ø	4	. 0	4.	0,00
63	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
64	Ø	Ø	Ø	Ø	4 .	Ø	4,	0.00
65	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
66	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
67	Ø	Ø	Ø	0	3	Ø	3.	0.00
68	Ø	Ø	Ø	Ø		Ø Ø	3,	0,00
69	Ø	Ø	Ø	Ø	3	0	3.	0.00
70	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
71	Ø	Ø	Ø	Ø	3	Ú	3.	0,00
72	Ø	Ø	0	Ø	3	Ø	3,	0.00
73	Ø	Ø	Ø	Ø	Ø	Ò	Ø.	0.00

TABLE T1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SPARROW WHITE SURFACE (UNBOXED)

		RECO	RDER	308.	ROCKET MOT	OR CHANNE	L 20	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1		1031	945		3503	2031	9559.	1.00
2		1031		1034	3503	2031	9559.	1.00
3		1031		1034	3503	2031	9559.	1.00
4		1031		1034	3503	2029	9557.	
5		1031		1034	3503	2025	9553.	1.00
6		1031		1034	3503	2023	9551.	1.00
7		1031		1034	3502	2017	9544.	
8		1031		1034	3502	2004	9531.	1.00
9		1031		1034	3501	1990	9516.	1,00
10		1031		1234	3501	1972	9498.	0.99
11		1031		1034	3501	1957	9483.	0,99
12		1031		1034	3499	1930	9454.	0.99
13		1031		1034	3488	1882	9395.	0.98
14		1031		1034	3467	1817	9309.	0.97
15		1031	944		3424	1736	9184.	0,96
16		1031		1033		1657	9079.	0,95
17		1030		1023	3332	1520	8862.	0,93
18		1028 1025	939	1911	3219	1303	8513.	0.89
19		1012	938	975	3059	1107 929	8127,	
20	971		937	951	2800 2635	859	7640. 7350.	Ø.80 Ø.77
22	914	952	926	882	2304	734	6712.	0.70
23	793	873	836	732	1923	642	5799	0,61
24	665	741	636	574	1593	564	4773.	0,50
25	578	590	480	435	1384	478	3945.	0,41
26	534	554	425	374	1285	444	3616.	0.38
27	481	484	359	303	1141	384	3152.	0,33
28	422	432	316	271	1008	311	2760.	0.29
29	382	383	289	229	899	251	2433.	0.25
30	341	355	255	193	793	203	2140.	0,22
31	325	342	243	180	753	185	2028.	0.21
32	289	318	207	143	649	. 135	1741.	0.18
33	263	291	186	115	536	100	1491.	0.16
34	232	265	158	79	447	76	1257.	0.13
35	211	246	138	55	381	53	1084.	0.11
36	193	232	122	48	350	41	986.	0.10
37	160	209			269	21	798.	0.08
38	128	178	87	17	197		619.	0.06
39	95	153	64	10	132	1273200000000000000000000000000000000000	461.	0.05
40	69	122	49	5	74	3	322.	0.03
41	59	106	39	3	52	2	261.	0.03
42	38	75	28	3 3 2	25	Ø	169.	0.02
43	23	60	22	2	16	Ø	123,	0.01
44	10	38	18	1	6 2	Ø	73.	0.00
45	2	25	10	1	2	Ø	40.	0.00

TABLE T1 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SPARROW WHITE SURFACE (UNBOXED)

		RECO	RDER	30B.	ROCKET MOT	OR CHANNE	L 20	
DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	2	21	7	1	2	И	33.	0.00
47	1	11	4	1	Ø	Ø	17.	0.00
48	Ø	8	Ø	1	Ø	Ø	9.	0.00
49	Ø	4	Ø	1	Ø	Ø	5.	0.00
50	Ø	2	Ø	1	Ø	Ø	3,	0.00
51	Ø	2	Ø	1	0	Ø	3.	0.00
52	Ø	1	Ø	1	Ø	Ø	2.	0.00
53	Ø	1	Ø	1	Ø	Ø	2.	0.00
54	Ø	1	Ø	1	Ø	Ø	2.	0.00
55	0	1	0	ī	Ø	Ø	2.	0.00
56	0	1	Ø	1	Ø	Ø	2.	0.00
57	Ø	1	Ø	1	Ø	Ø	2.	0.00
58	Ø	1	Ø	1	Ø	Ù	2,	0.00
59	Ø	1	Ø	1	Ø	Ø	2.	0.00
60	Ø	1	Ø	ī	Ø		2.	0,00
61	Ø	1	Ø	i	Ø	. Ø	2,	0.00
62	Ø	1	Ø	1	Ø	Ø	2,	0.00
63	Ø	1	Ø	1	Ø	Ø	2.	0.00
64	ø	1	Ø	. 1	ø	Ø	2.	0.00
65	Ø	1	Ø	1	ø	Ø	2.	0.00
66	Ø	1	Ø	1	Ø	Ø	2.	0.00
67	· Ø	1	Ø	ī	Ø	Ø	2,	0.00
68	Ø	1	0	1	Ø	Ø	2.	0.00
69	Ø	1	Ø	1	Ø	Ø	2.	0.00
70	Ø	1	Ø	1	Ø	Ø	2.	0.00
71	Ø	1	Ø	1	Ø		2.	0.00
72	Ø	Ø	Ø	ī	Ø	· Ø	1.	0,00
73	Ø	Ø	Ø	1	Ø	Ò	1.	0.00
74	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
75	Ø	Ø	Ø	1	ø	Ø	1.	0.00
76	Ø	Ø	Ø	1	ě	Ø	1,	0.00
77	ā	a	a	ā	ā	Ü	a	0.00

TABLE U1
CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS
CARTRIDGES 20mm INTERICR

ROCKET MOTOR CHANNEL 21

RECORDER 308.

TABLE U1 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS CARTRIDGES 20mm INTERIOR

		RECO	RDER	308.	ROCKET MOT	OR CHANNE	L 21	
DEG.	DEC.	JAN	FEB	MAR	AUT_SPRING	WINTER	TOTAL	C.PROB
46	122	182	87	19	223	7	640.	0.07
47	89	156	72	12	147	3	479.	0.05
48	67	127	56	5	87	i	343,	0.04
49	45	102	41	2	43	Ø	233.	0.02
50	32	77	26	Ø	21	Ø	156.	0.02
51	25	62	21	Ø	15	Ю	123.	0.01
52	15	41	9	Ø	6	Ø	71.	0.00
53	5	23	7	Ø	4	Ø	39.	0.00
54		15	Ø	Ø	4	Ø	19.	0.00
55	Ø	6	Ø	0	4	Ø	10.	0.00
56	Ø	5	Ø	Ø	4	Ö	9.	0.00
57	Ø	2	Ø	Ø	4	Ø	6.	0.00
58	Ø	1	Ø	Ø	4	Ø	5,	0.00
59	Ø	1	Ø	Ø	4	Ø	5,	0.00
60	Ø	Ø	Ø	0	4	Ø	4.	0.00
61	Ø	Ø	Ø	Ø	4	· Ø	4.	0.00
62	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
63	Ø	Ø	Ø	Ø	4	Ø	4.	0.00
64	Ø	Ø	Ø	Ø	4	Ò	4.	0.00
65	Ø	Ø	Ø	. Ø	3	Ø	3,	0.00
66	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
67	Ø	Ø	Ø	Ø	3	Ø	3.	0,00
68	Ø	Ø	Ø	Ø	3	Ø	3,	0.00
69	0	Ø	Ø	Ø	3	. Ø	3.	0.00
70	Ø	Ø	Ø	Ø	3	Ø	3.	0.00
71	Ø	Ø	Ø	Ø	3	Ø	3.	0,00
72	Ø.	Ø	Ø	Ø	3	. 0	3.	0,00
73	Ø	0	Ø	Ø	0	. 0	0.	0.00

TABLE V1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

CARTRIDGES 20mm EXTERIOR

0,

1079.

TABLE V1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

#### CARTRIDGES 20mm EXTERIOR

DEG. DEC JAN FEB MAR AUT-SPRING WINTER TOTAL C.PROB  46			RECO	RDER	30B.	ROCKET MO	TOR CHANNE	L 22	
47       166       216       100       38       319       27       866.       0.09         48       139       204       90       32       256       12       733.       0.08         49       106       179       85       19       192       7       588.       0.06         50       81       157       70       12       120       2       442.       0.05         51       72       140       62       6       88       2       370.       0.04         52       53       105       43       4       61       0       266.       0.03         53       38       82       30       4       21       0       175.       0.02         54       23       57       18       1       4       0       103.       0.01         56       9       32       8       1       0       0       52.       0.00         57       3       21       2       1       0       0       57.       0.00         58       1       10       1       0       0       7.       0.00         59	DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
48       139       204       90       32       256       12       733.       0.08         49       106       179       85       19       192       7       588.       0.06         50       81       157       70       12       120       2       442.       0.05         51       72       140       62       6       88       2       370.       0.04         52       53       105       43       4       61       0       266.       0.03         53       38       82       30       4       21       0       175.       0.02         54       23       57       18       1       4       0       103.       0.01         55       13       38       10       1       0       0       62.       0.00         56       9       32       8       1       0       0       62.       0.00         57       3       21       2       1       0       0       27.       0.00         58       1       10       1       0       0       7.       0.00         60       0 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
49       106       179       85       19       192       7       588.       0.06         50       81       157       70       12       120       2       442.       0.05         51       72       140       62       6       88       2       370.       0.04         52       53       105       43       4       61       0       266.       0.03         53       38       82       30       4       21       0       175.       0.02         54       23       57       18       1       4       0       103.       0.01         55       13       38       10       1       0       0       62.       0.00         56       9       32       8       1       0       0       27.       0.00         57       3       21       2       1       0       0       27.       0.00         58       1       10       1       0       0       27.       0.00         58       1       10       1       0       0       3.       0.00         59       0       6									
50       81       157       70       12       120       2       442       0.05         51       72       140       62       6       88       2       370       0.04         52       53       105       43       4       61       0       266       0.03         53       38       82       30       4       21       0       175       0.02         54       23       57       18       1       4       0       103       0.01         55       13       38       10       1       0       0       62       0.00         56       9       32       8       1       0       0       27       0.00         56       9       32       8       1       0       0       27       0.00         57       3       21       2       1       0       0       27       0.00         58       1       10       1       0       0       7       0.00         58       1       10       1       0       0       7       0.00         60       0       2       0 <t< td=""><td></td><td>139</td><td></td><td>90</td><td>32</td><td>256</td><td>12</td><td>733.</td><td>0.08</td></t<>		139		90	32	256	12	733.	0.08
52       53       105       43       4       61       0       266       0       03         53       38       82       30       4       21       0       175       0       02         54       23       57       18       1       4       0       103       0       00         56       9       32       8       1       0       0       50       0       00         57       3       21       2       1       0       0       27       0       00         57       3       21       2       1       0       0       27       0       00         58       1       10       1       0       0       7       0       00         59       0       6       0       1       0       0       7       0       00         60       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         62       0       2       0       1       0		106		85	19	192		588.	0.06
52       53       105       43       4       61       0       266       0       03         53       38       82       30       4       21       0       175       0       02         54       23       57       18       1       4       0       103       0       00         56       9       32       8       1       0       0       50       0       00         57       3       21       2       1       0       0       27       0       00         57       3       21       2       1       0       0       27       0       00         58       1       10       1       0       0       7       0       00         59       0       6       0       1       0       0       7       0       00         60       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         62       0       2       0       1       0							2		0.05
52       53       105       43       4       61       0       266       0       03         53       38       82       30       4       21       0       175       0       02         54       23       57       18       1       4       0       103       0       00         56       9       32       8       1       0       0       50       0       00         57       3       21       2       1       0       0       27       0       00         57       3       21       2       1       0       0       27       0       00         58       1       10       1       0       0       7       0       00         59       0       6       0       1       0       0       7       0       00         60       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         62       0       2       0       1       0					6	88	2	370.	0.04
54       23       57       18       1       4       0       103.       0.01         55       13       38       10       1       0       0       62.       0.00         56       9       32       8       1       0       0       50.       0.00         57       3       21       2       1       0       0       27.       0.00         58       1       10       1       0       0       7.       0.00         59       0       6       0       1       0       0       7.       0.00         60       0       2       0       1       0       0       7.       0.00         61       0       2       0       1       0       0       3.       0.00         62       0       2       0       1       0       0       3.       0.00         63       0       1       0       1       0       0       2.       0.00         64       0       1       0       1       0       0       2.       0.00         65       0       1       0       1<				43	4	61	Ø		0.03
55       13       38       10       1       0       0       62       0       00         56       9       32       8       1       0       0       50       0       00         57       3       21       2       1       0       0       27       0       00         58       1       10       1       1       0       0       13       0       00         59       0       6       0       1       0       0       7       0       00         60       0       2       0       1       0       0       7       0       00         61       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         62       0       2       0       1       0       0       3       0       00         63       0       1       0       1       0       0       2       0       00         64       0       1       0       1       0					4	21			
56       9       32       8       1       0       0       50       0       00         57       3       21       2       1       0       0       27       0       00         58       1       10       1       0       0       13       0       00         59       0       6       0       1       0       0       7       0       00         60       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         62       0       2       0       1       0       0       3       0       00         63       0       1       0       1       0       0       2       0       00         64       0       1       0       1       0       0       2       0       00         65       0       1       0       1       0       0					1	4			
57       3       21       2       1       0       0       27.       0.00         58       1       10       1       1       0       0       13.       0.00         59       0       6       0       1       0       0       7.       0.00         60       0       2       0       1       0       0       3.       0.00         61       0       2       0       1       0       0       3.       0.00         61       0       2       0       1       0       0       3.       0.00         62       0       2       0       1       0       0       3.       0.00         63       0       1       0       1       0       0       2.       0.00         64       0       1       0       1       0       0       2.       0.00         65       0       1       0       1       0       0       2.       0.00         67       0       1       0       1       0       0       2.       0.00         68       0       1       0					1		0	62.	0.00
58       1       10       1       1       0       0       13.       0.00         59       0       6       0       1       0       0       7.       0.00         60       0       2       0       1       0       0       3.       0.00         61       0       2       0       1       0       0       3.       0.00         62       0       2       0       1       0       0       3.       0.00         63       0       1       0       1       0       0       2.       0.00         64       0       1       0       1       0       0       2.       0.00         65       0       1       0       1       0       0       2.       0.00         66       0       1       0       1       0       0       2.       0.00         67       0       1       0       1       0       0       2.       0.00         68       0       1       0       1       0       0       2.       0.00         70       0       1       0       <				8	1		0	50.	0.00
59       0       6       0       1       0       0       7       0       00         60       0       2       0       1       0       0       3       0       00         61       0       2       0       1       0       0       3       0       00         62       0       2       0       1       0       0       2       0       00         63       0       1       0       1       0       0       2       0       00         64       0       1       0       1       0       0       2       0       00         65       0       1       0       1       0       0       2       0       00         66       0       1       0       1       0       0       2       0       00         67       0       1       0       1       0       0       2       0       00         68       0       1       0       1       0       0       2       0       00         70       0       1       0       1       0       0<					1				
60 0 2 0 1 0 0 3. 0.00 61 0 2 0 1 0 0 3. 0.00 62 0 2 0 1 0 0 0 3. 0.00 63 0 1 0 1 0 0 0 2. 0.00 64 0 1 0 1 0 0 2. 0.00 65 0 1 0 1 0 0 2. 0.00 66 0 1 0 1 0 0 0 2. 0.00 67 0 1 0 1 0 0 0 2. 0.00 68 0 1 0 1 0 0 0 2. 0.00 69 0 1 0 1 0 0 0 2. 0.00 70 0 1 0 1 0 0 0 2. 0.00 71 0 1 0 1 0 0 0 2. 0.00 72 0 0 0 1 0 1 0 0 0 1. 0.00 73 0 0 0 1 0 1 0 0 0 1. 0.00 74 0 0 0 1 0 1 0 0 0 1. 0.00 75 0 0 0 1 0 1 0 0 1 0 0 1. 0.00 76 0 0 0 1 0 1 0 0 1 0 0 1. 0.00					1				
61       Ø       2       Ø       1       Ø       Ø       3       Ø       Ø         62       Ø       2       Ø       1       Ø       Ø       3       Ø       Ø         63       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø       Ø         64       Ø       1       Ø       1       Ø       Ø       2       Ø <td< td=""><td></td><td>Ø</td><td></td><td>Ø</td><td>1</td><td></td><td></td><td></td><td></td></td<>		Ø		Ø	1				
63       Ø       1       Ø       Ø       2       Ø       Ø         64       Ø       1       Ø       Ø       2       Ø       Ø         65       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         66       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         67       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         68       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         69       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         70       Ø       1       Ø       1       Ø       2       Ø       Ø         71       Ø       1       Ø       1       Ø       2       Ø       Ø         72       Ø       Ø       0       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       I       Ø <t< td=""><td></td><td></td><td>2</td><td></td><td>1.</td><td>Ø</td><td></td><td></td><td></td></t<>			2		1.	Ø			
63       Ø       1       Ø       Ø       2       Ø       Ø         64       Ø       1       Ø       Ø       2       Ø       Ø         65       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         66       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         67       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         68       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         69       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         70       Ø       1       Ø       1       Ø       2       Ø       Ø         71       Ø       1       Ø       1       Ø       2       Ø       Ø         72       Ø       Ø       0       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       I       Ø <t< td=""><td></td><td></td><td>2</td><td></td><td>1</td><td></td><td>0</td><td></td><td></td></t<>			2		1		0		
64       Ø       1       Ø       Ø       2       Ø       Ø         65       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         66       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         67       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         68       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         69       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         70       Ø       1       Ø       1       Ø       2       Ø       Ø         71       Ø       1       Ø       1       Ø       2       Ø       Ø         72       Ø       Ø       0       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       I       Ø       Ø			2		1		Ø		
65					1			2.	
66					1			2.	
67       Ø       1       Ø       Ø       2       Ø       Ø         68       Ø       1       Ø       Ø       Ø       2       Ø       Ø         69       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         70       Ø       1       Ø       Ø       Ø       2       Ø       Ø         71       Ø       1       Ø       Ø       2       Ø       Ø         72       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø         73       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø         74       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø <td></td> <td></td> <td></td> <td>Ø</td> <td>1</td> <td></td> <td></td> <td>2.</td> <td></td>				Ø	1			2.	
68       Ø       1       Ø       Ø       2       Ø       Ø         69       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         70       Ø       1       Ø       1       Ø       Ø       2       Ø       Ø         71       Ø       1       Ø       Ø       2       Ø       Ø         72       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø         73       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø       I       Ø       Ø       I       Ø       Ø       I       Ø       Ø       I       Ø       Ø       I       Ø       Ø       I       Ø       Ø       I       Ø			7.00	Ø	1		The state of the s	2.	
69       Ø       1       Ø       Ø       2       Ø       Ø         70       Ø       1       Ø       Ø       Ø       2       Ø       Ø         71       Ø       1       Ø       Ø       Ø       2       Ø       Ø         72       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø         73       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø         74       Ø       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø       Ø       1       Ø			1	Ø	1			2,	
70       0       1       0       1       0       2       0       0         71       0       1       0       0       2       0       0         72       0       0       1       0       0       1       0       0         73       0       0       0       1       0       0       1       0       0         74       0       0       0       1       0       0       1       0       0         75       0       0       0       1       0       0       1       0       0         76       0       0       0       1       0       0       1       0       0			1	Ø	1			2.	
71 Ø 1 Ø 1 Ø Ø 2. Ø.00 72 Ø Ø Ø 1 Ø Ø 1. Ø.00 73 Ø Ø Ø 1 Ø Ø 1. Ø.00 74 Ø Ø Ø 1 Ø Ø Ø 1. Ø.00 75 Ø Ø Ø 1 Ø Ø Ø 1. Ø.00 76 Ø Ø Ø 1 Ø Ø Ø 1. Ø.00					1		0		
72					1				
74 Ø Ø Ø 1 Ø Ø 1. Ø.ØØ 75 Ø Ø Ø 1 Ø Ø 1. Ø.ØØ 76 Ø Ø Ø 1 Ø Ø 1. Ø.ØØ					1		0		
74 Ø Ø Ø 1 Ø Ø 1. Ø.ØØ 75 Ø Ø Ø 1 Ø Ø 1. Ø.ØØ 76 Ø Ø Ø 1 Ø Ø 1. Ø.ØØ					1		0		
75 0 0 0 1 0 0 1. 0.00 76 0 0 0 1 0 0 1. 0.00					1				
76 0 0 0 1 0 0 1. 0.00					1		Ø		
							Ø		
							. 0		
	77	Ø	Ю	0	9	0	ñ	0.	0.00

TABLE W1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

BULLPUP CENTRE

TABLE W1 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

#### BULLPUP CENTRE

		RECO	RDER	308.	ROCKET MOT	OR CHANNE	L 23	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	Ø	Ø	1	Ø	4	0	5,	0.00
47	Ø	Ø	1	Ø	4	Ø	5,	0,00
48	0	Ø	. 1	Ø	4	Ø	5.	0.00
49	0	Ø	1	Ø	4	Ø	5.	0.00
50	Ø	Ø	1	Ø	4	Ø	5.	0.00
51	0	Ø	1	Ø	4	Ø	5.	0.00
52	Ø	Ø	1	Ø	4	Ø	5.	0.00
53	Ø	0	1	Ø	4	Ø	5.	0.00
54	Ø	0	1	Ø	4	Ó	5.	0.00
55	Ø	Ø	1	Ø	4	Ø	5.	0.00
56	Ø	Ø	1	0	4	Ø	5,	0.00
57	Ø	Ø	1	0	4	Ø	5.	0.00
58	Ø	Ø	1	Ø	4	Ø	5 5 5	0.00
59	0	Ø	1	Ø	4	Ø	5.	0.00
60	Ø	Ø	1	Ø	4	Ø	5,	0.00
61	Ø	Ø	1	Ø	4	Ø	5,	0.00
62	Ø	Ø	1	Ø	4	Ø	5.	0.00
63	Ø	Ø	1	Ø	4	Ø		0.00
64	0	Ø	1	Ø	4	Ø	5.	0.00
65	Ø	Ø	1	0	3	Ø	4.	0.00
66	Ø	Ø	1	0	3	Ø	4.	0.00
67	Ø	Ø	1	Ø	3 3	0	4.	0.00
68	0	Ø	1	0	3	Ø .	4.	0.00
69	0	Ø	1	Ø	3		4.	0.00
70	Ø	0	1	Ø	3	Ø	4.	0.00
71	Ø	Ø	1	Ø	3	Ø	4.	0.00
72	0	Ø	1	Ø	3	Ø	4.	0.00
73	Ø	0	1	Ø	3	Ø	4.	0.00
74	Ø	Ø	Ø	Ø	2	Ø	2.	0.00
75	Ø	Ø	Ø	0	1	Ø	1.	0.00
76	0	Ø	Ø	Ø	0	Ø	Ø,	0.00

TABLE X1

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

BULLPUP MOTOR SKIN

RECORDER 30B. ROCKET MOTOR CHANNEL 24

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1015	1031	946	1033	3503	2031	9559.	1.00
2		1031		1033	3503	2031	9559.	1.00
3		1031		1033	3503	2031	9559	1.00
4		1031		1033	3503	2031	9559.	1.00
		1031		1033	3503	2031	9559.	1.00
5		1031		1033	3503	2031	9559.	
7		1031		1033	3503	2027	9555.	
8		1031		1033	3502	2023	9550.	
9		1031		1033	3501	2011	9537.	1,00
10	1015	1031	946	1033	3501	1999	9525.	
11	1015	1031	946	1033	3501	1992	9518.	
12	1015	1031		1033	3501	1970	9496.	0.99
13	1015	1031		1033	3500	1942	9467.	0.99
14		1031		1033	3495	1898	9418.	
15		1031		1033	3480	1841	9346.	0,98
16		1031		1033	3467	1802	9294.	0.97
17		1031		1033	3422	1687	9133.	0.96
18		1031		1024	3356	1505	8874.	0,93
19		1031		1.013	3252	1299	8551.	
20	1004		941	999	3068	1089	8129.	
21		1025	941	979	2922	997	7860.	
22			938	932	2598	845	7287.	0.76
23	898	952	886	813	2251	715	6515.	0.68
24	786	852	726	638	1872	601	5475.	0.57
25	663	702 640	565	476	1567	515	4488.	
26 27	624 546	561	499	409	1442	466 374	4080.	
28	482	491	341	318 265	1251	315	3453, 2984,	Ø.36 Ø.31
29	423	439	292	215	1090	245	2543.	
30	375	392	249	168	929 801	196	2181.	0,23
31	355	371	236	155	738	170	2025.	
32	309	331	203	119	620	122	1704.	
33	269	291	168	82	503	86	1399.	
34	234	252	133	50	390	63	1122.	0,12
35	186	224	108	18	316	34	886.	0.09
36	164	208	90	12	285	26	785.	0.08
37	126	171	73	2	213	9	594.	
38	102	129	49	2		3	435.	
39	65	100	33	1	15Ø 88	3	290.	0.03
40	33	63	21	1 1	50	3	168.	0.02
41	29	48	15	ī	35	10	128.	0.01
42	8	28	8		12	Ø	57.	0.00
43	5	15	1	1	5	Ü	27.	0.00
44	4	8	Ø	1 1 1 1	2	Ø	15.	0,00
45	1	4	Ø	1	12 5 2	Ø	8.	0.00

TABLE X1 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS BULLPUP MOTOR SKIN

		RECO	RDER	3øB.	ROCKET MOT	OR CHANNE	L 24	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	1	3	Ø	1	2	Ø	7.	0.00
47	1	2	Ø	1	2	Ø	6.	0.00
48	1	2	Ø	1	2	Ø	6.	0.03
49	Ø	2	Ø	1	2	Ø	5,	0.00
50	Ø	1	Ø	1	2	Ø	4.	0.00
51	Ø	. 1	0	1	2	Ø	4.	0.00
52	0	1	Ø	1	2	Ø	4.	0.00
53	Ø	1	Ø	1	2	Ø	4.	0.00
54	Ø	1	Ø	1	2 2 2 2 2	Ø	4.	0.00
55	Ø	1	Ø	1	2	Ø	4.	0.00
56	Ø	. 1	0	1	2	Ø	4.	0.00
57	. 0	1	Ø	1	1	Ø	3.	0.00
58	Ø	1	Ø	1	1	Ø	3,	0.20
59	Ø	1	Ø	1	1	Ø	3,	0.00
60	Ø	1	Ø	1	1:	Ø Ø Ø	3.	0.00
61	Ø	1	Ø	1	1	Ø	3,	0.00
62	0	1	Ø	1	1	Ø	3,	0.00
63	Ø	1	Ø	1	1	U	3.	0.00
64	Ø	1	Ø	1	1	Ø	3.	0.00
65	Ø	1	Ø	1	1	Ø	3.	0.00
66	. Ø	1	Ø	1	Ø	Ø	2.	0.00
67	Ø	1	Ø	1	Ø	Ø	2.	0.00
68	Ø	1	Ø	1	Ø	0	2.	0.00
69	0	1	Ø	1	Ø	Ø	2.	0.00
70	Ø	1	0	1	0	Ø	2.	0.00
71	Ø	1	0	1	0	. 0	2.	0.00
72	Ø	Ø	Ø	1	0	Ø	1,	0.00
73	Ø	0	Ø	1	Ø	0	1.	0,00
74	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
75	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
76	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
77	Ø	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

Q.

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TABLE A2

#### LINNET EXT. TOP (WHITE)

DEG.	DEC	MAL .	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1232	1030	948	1026	3681	2031	9746.	1.00
2	1033	1030		1326	3681	2031	9746.	1.00
3		1030	948		3681	2030	9745.	1.03
4	1033	1430	948	1026	3681.	2028	9743.	1.03
5	1030	1032	948	1026	3681	2021	9736.	1.00
6	1030	1030	948	1 126	3681	2017	9732.	1.00
7	1333	1030	947	1026	3581	2337	9721.	1.00
8.	1030	1330	947	1026	3681	1993	9707.	1.00
9	1035	1030	947	1926	3681	1965	9679.	0.99
		1030	947	1026	3681	1933	9647.	0.99
	1030	1030	947	1326	3681	1917	9631.	0.99
12	1330	1930	947	1026	3575	1875	9583.	3.98
13	1/30	1030	947	1/26	3667	1818	9518.	2.98
14	1030	1030	945	1/26	3652	1755	9439.	0.97
	1030	1030	946	1026	3626	1679	9337.	2.96
	1033	1030	946	1326	3605	1640	9277.	0.95
17	1030	1030	946	1026	3564	1547	9143.	0.94
18	1030	1030	945	1326		1465	8993.	3.92
19	1033	1228	945	1026	3497 3413	1348	8790.	0.90
- 50	1030	1024	945	1926	3298	1244	8567.	0.83
21	1030	1019	945	1319	3216	1185	3415.	0.86
22	1026	1011	945	988	2975	1069	3014.	2.82
	396	933	924	911	2644	942	7425.	2.76
24	911	933	382	321	2290	833	6675.	0.68
25	812	369	333	737	1985	727	5938.	0.61
26	765	326	741	592	1828	670	5522.	2,57
27	648	730	591	596	1524	573	4662.	0.48
28	557	605	497	484	1291	491	3925.	0.40
29	493	597	422	376	1132	421	3351.	0.34
39	451	449	363	331	1219	374	2957.	0.30
31	423	428	339	267	965	348	2770.	0.28
32	387	392	289	217	868	305	2456.	0.25
33	352	359	252	179	767	264	2173.	0.22
34	315	532	221	158	651	236	1916.	0.20
35	236	293	192	133	556	193	1658.	0.17
36	272	289	173	122	520	173	1549.	0.16
37	234	253	1.49	124	434	145	1325.	0.14
36	223	232	1.35	90	376	125	1165.	0.12
39	180	1.93	114	76	319	93	971.	0.10
40	145	173	93	55	244	69	779,	0.08
41	138	1.67	84	44	211	58	722.	0.07
42	106	128	60	28	154	33	579.	0.05
43	8.7	102	43	15	125	20	386.	2.04
44	52	31	27	+7	91	9	267.	0.03
45	35	56	1.4	3	50	6	164.	0.02

TABLE A2 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET EXT. TOP (WHITE)

		RECO	RDER	230.	ROCKET MOT	OR CHANNE	L 1	
DEG.	DEC.	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	28	45	14	1	31	2	124.	0.01
47	12	24	3	. 0	17	Ø	61.	0.00
48	8	15	5	Ø	6	Ø	34.	5.00
49	4	3	3	Ø	4	Ø	19.	0.00
50	1	6	2	Ø	1	Ø	10.	0.00
51	1	5	1.	Ø	Ø	W	7.	2.02
52	. 9	3	0	Ø	Ø	Ø	3.	0.00
53	9	. 0	a	0	Ø	V)	Ø	0.00

TABLE B2

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET PROP. SURFACE (WHITE)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1033	1030	948	1.026	3681	2032	9747.	1.00
2		1030		1226	3581	2032	97.47.	1.00
3		1032		1026	3681	2031	9746.	1.00
4		1030	943	1226	3581	2030	9745.	
			949				9743.	
5		1030		1025	3681	2/12/3		1.00
6		1030		1026	3681	2/124	9739.	1.00
7		1230	948	1026	3681	2016	9731.	1.90
8		1030	948	1026	3681	2,003	9718,	1.33
9		1030		1326	3681	1977	9691.	
10		1730		1026	3681	1944	9658.	0,99
11		1030		1326	3681	1939	9653.	∅.99
12	1333	1030	947	1026	3679	1901	9613.	0.99
13	1233	1030	947	1326	3671	1846	9552.	0.98
14	1032	1030	947	1326	3662	1774	9469.	9.97
15	1037	1030	946	1026	3639	1687	9358.	2.95
16		1032	946	1026	3628	1.639	9299.	0.95
17		1030			3583	1554	9169.	0.94
18		1030		1026	3520	1476	9028.	0.93
19		1029		1826	3461	1374	8865.	0.91
20		1026	945	1326	3343	1274	8644.	0.89
21		1025	945	1321	3266	1218	8585.	0.87
22		1019	945	1301	3258	1096	8149.	0.84
23	1022	1004	934	923		969	7616.	Ø.78
					2766			
24	951	969	898	836	2435	849	6938.	0.71
25	864	906	834		2103	750	6217.	0.64
-26	894	861	789.		1922	694	5782.	0.59
27	694	771	542	621	1596	579	4903.	0.50
28	592	631	521	511	1359	487	4181.	0.42
29	526	526	450	396	1172	415	3486.	0.36
30	456	468	383	297	1738	370	3322.	0.31
31	451	447	367	261	977	347	2850.	0.29
32	411	406	317	217	865	295	2512.	2.26
33	358	367	250	180	750	255	2170.	25.0
34	355	337	224	151	620	219	1873.	机 0.19
35	288	293	195	127	533	1:75	1611.	0.17
36	277	277	183	117	482	156	1465,	0.15
37	232	245	154	94	410	124	1264.	0.13
38	201	217	133	80	334	133	1065.	3.11
39	170	190	108		253	76	844.	0.09
40	131	153	81		203	50	651.	0.07
41	121	138	66	26	176	36	563.	0.06
42	85	137				16	489.	0.04
43	62	81	52	13	136			0.03
44	39	55	27	4	89 57	107	273. 173.	
			14	1				0.02
45	24	35	9	Ø	25	3	96.	0.33

TABLE B2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET PROP. SURFACE (WHITE)

		RECO	RDER	230.	ROCKET MOT	OR CHANNE	r 5 .	
DEG.	DEC	JAM	FEB	MAR	AUT-SPRING	WINTER	TOTAL	c.PR03
46	18	26	8	Ø	20	2	74.	3.23
47	8	17	6	0	5	1	37.	0.00
48	5	11	4	. 0	3	1	24.	0.00
49	2	S	3	0	3	Ø	13.	0.00
50	0	4	1	Ø	2	Ø	5.	0.03
51	Ø	. 2	3	2	2	V	2.	0.33
52	3	2	A	0	3	Ø	2.	0.33
53	7	1	3	Ø	Ø	0	1.	0.00
54	. 0	. 0	3	3	Ø	U	Ø.	0.00

TABLE C2

#### LINNET INT. PROP. CHARGE (WHITE)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
			0.10		750/	6070	2444	4 00
1		1.030	943	545	3526	2032	9111.	
2		1030	948	545	3526	2032	9111.	1.00
3		1030	943	545	3526	2032	9111.	1.00
4		1030	948	545	3526	2030	9129.	1.00
5		1030	948	545	3526	5055	9124.	1.00
0		1/30	943	545	3526	5050	9099.	1.00
7		1.030	948	545	3526	2015	9094.	
8		1030	947	545		2003	9081.	
9	1032	1030	947	545	3526	1984	9062.	0.99
10	1030	1030	947	545	3526	1952	9030.	0.99
11	1030	1230	947	545	3526	1934	9012.	0.99
12	1.030	1030	947	545	3524	1993	8979.	0.99
13	1039	1236	947	545	3518	1852.	8922.	0.98
1.4	1030	1030	947	545	3509	1787	8848.	0,97
15	1030	1.039	946	545	3489	1709	8749.	0.96
16	1.030	1030	946	545	3476	1668	8695.	0.95
17		1730	946	545	3431	1595	8577.	0.94
18	1030	1030	945	545	3374	1503	8427.	0.92
19	1030	1028	945	545	3305	1405	3258.	
20		1026	945	544	3207	1305	8057.	0.88
21	1237	1.220	945	542	3135	1257	7929.	0.87
22	1039	1013	945	525	2922	1112	7547.	0.83
23	1013	996	929	455	2606	971	6967.	0.76
24	946	953	884	374	2301	862	6320.	0.69
25	845	886	819	308	1946	754	5559.	0.61
26	794	849	766	280	1790	693	5172.	0.57
27	676	753	620	217	1491	590	4347.	0.48
28	587	627	514	169	1256	492	3636.	0.40
29	516	522	446	124	1797	433	3138.	0.34
30	459	465	377	101	981	385	2768.	0.30
31.	439	444	347	87	927	358	2602.	0.29
32	400	404	305	72		311	2324.	0.26
33	365	369	257		831	272	2048.	0.22
34	329			54	731	232	1785.	0.20
35	293	331	228	41	624	191	1535.	
36	278	305	.192	27	527	176	1439.	0.17
			182	22	489			0.16
37	238	254	156	1.1	410	142	1211.	0.13
38	211	229	143	9	350	115	1054.	0.12
39	181	203	115	6	268	94	867.	0.10
40	151	173	92	2	223	67	708.	0.08
41.	139	156	80	2	188	55	620.	0.07
42	101	126	54	2	154	30	465.	0.05
43	75	100	43	77	1.21.	18	357.	0.04
44	53	76	26	Ø	89	10	254.	0.23
45	31	51	14	Ø	46	6	148.	0.02

TABLE C2 (cont.)

#### LINNET INT. PROP. CHARGE (WHITE)

		RECO	RDER	23c.	ROCKET MOT	OR CHANNE	L 3	
DEG.	DEC.	JAN	FEB	NAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	25	41	11	. 2	31	5	113.	0.21
47	13	24	7	0	17	1	62.	0.00
48	7	11	4	Ø	8	1	31.	0.00
49	5	9	2	9	3	Ø	19.	. 0.00
50	1	6	2	0	Ø	Ŋ	9.	0.02
51	1	6	1	0	И	Ø	8.	0.00
52	. 0	2	1	7	Ø	Ø	-3.	0.00
53	g .	· 0	0	Ø	O	10	Ø.	0.00

TABLE D2 CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

LINNET EXT. BOTTOM (WHITE)
RECORDER 23C. ROCKET MOTOR CHANNEL 4

			1121-11	200.		HOOK. I NO	OH CHARIN	-L "	
DEG.	DEC	MAL	FEB	MAR	A	UT-SPRING	WINTER	TOTAL	C.PROB
1	1030	1031	948	1028		3681	2032	9750.	1.00
2		1031		1028		3681	2032	9759.	1.00
3	1030	1031		1928		3681	2035	9750.	1.00
4	1032	1031		1028		3681	2032	9750.	1.00
5	1030	1031		1028		3681	2030	9748.	1.00
6		1031		1028		3681	2029	9747.	1.00
7	1030	1031		1028		3681	2019	9737.	1.00
8		1031		1028		3681	2013	9730.	1.00
9				1/28		3681	1997	9714.	1.00
10		1031		1328		3581	1978	9695.	0.99
11	1030			1023		3681	1953	9669.	0.99
12		1031		1027		3681	1912	9627.	0.99
13	1030	1031		1027		3678	1869	9581.	0.98
14	1939	1031		1/27		3674	1316	9524.	0.98
15	1330	1031		1027		3657	1735	2424	0.97
16	1030	1031		1027		3647	1685	9365.	0.96
17	1030	1031	945	1327		3613	1576	9222.	0.95
16	1030	1031		1327		3569	1479	9981.	0.93
19	1030	1231		1027		3505	1387	8925.	0.92
20	1030	1030	945	1327		3439	1283	8745.	0.90
21	1030	1029	945	1026		3378	1233	3641.	0.89
55	1030	1026	945	1017		3181	1103	8302,	0.85
23	1027	1012	943	969		2883	947	7781.	0.83
24	991	.985	904	876		2541	829	7125.	0.73
25	913	940	857	778		5505	720	6410.	0.66
.26	559	897	805.			1980	660	5935.	0.61
27	739	815	675	628		1625	559	5041.	3.52
28	522	680	519	523		1326	451	4126.	0.42
29	535	550	446	401		1130	377	3439.	0.35
30	474	482	370	291		958	303	2878.	Ø.30
31	450	457	342	236		380	289	2654.	0.27
32	398	398	290	192		748	247	2273.	0.23
33	347	364	240	150		625	205	1931.	0.20
34	302	307	194	120		517	154	1594.	0.16
35	245	264	160	101		399	116	1285.	0.13
36	231	247	143	85		357	97	1160.	0.12
37	194	211	111	56		285	6.5	923.	0.09
38	159	1.76	89	32		550	31	707.	0.07
39	123	137	64			166	16	516.	0.05
40	102	1.01	35	4		107	1.1	360.	0.04
41	81	86	56	3		35	5.3	289.	9.03
42	59	55	13	1.		43	3	174.	0.03
43	34	38	8.			23	3	107.	0.01
44	25	23	5	1		11	5	68.	0.00
45	12	13	5	1 1		4	2	37,	0.00
									15 4 25 45

TABLE D2 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LINNET EXT. BOTTOM (WHITE)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	1.0	1.1	5	1	3	2	29.	0.00
47	7	6	1	1	9	5	17.	0.93
48	4	5	0	1.	Ø	.Ø	10.	0.00
49	1	4	0	1	0	Ø	6.	0.00
50	1	3 3	3	1	7	٥	5.	0.00
51	Ø	3	0	1	Ø	Ø	4.	0.00
52	Į.	2	03	1	ð	0	3.	0.00
53	3	2	2	1	ð	D D	3.	0.00
54	J	1.	Ø	1	Ø	Ú	2.	0.00
55	3	1	Ø	1.	Ø	Ø	2.	0.00
56	Ø	1	Ø	1	Я	Ø	2.	0.00
57	2	1	0	1	0	Ø	2.	0.00
58	Ø	1	Ø	1	Ø	Ø	2.	0.00
59	. 5	1	Ø	1.	g	Ø	2.	0.00
60	0	1	J	1.	D	b	2.	0.00
61	Ø	1	O	1	Ð	- 10	2.	0.00
62	Ø		U	1.	Ű	U	2.	0.00
63	Ø	1	Ø	1	Ø	Ø	2,	. 0.00
64	5	1	Ø	1	Ø	Ø	2.	0.00
65	2	1	Ø	1	Ø	Ø	2.	0.00
66	0	1	Ø	1	Ø	Ø	2.	0.00
67	Ø.	1	Ø	1	0	W	2.	0.00
68	0	1	J	1	Ø	Ø.	2.	0.00
69	Ø	1	Ø	1	Ø .	0	2,	0.60
70	Ø	1	ð	1	Ø	Ŋ	2.	0.00
.71	Ø.	1	0.	1	Ø	Ŋ	2.	0.00
72	Ø	Ø	9	1	Ø	Ŋ	1.	0.03
73	Ø	Ø	Ø	1	Ø	· · · ·	1.	0.00
74	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
75	Ø	0	9	1	J	10	1.	0.00
76	D D	Ø	0	1	Ø	Ø	1.	0.00
77	0	Ø	9	Ø	g ·	0	Ø.	0.30

TABLE E2

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

CUCKOO EXT. TOP (TAIL)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1030	1.030	948	1027	3681	2032	9743.	1.00
2		1030		1027	3681	2032	9748.	
3		1030		1027	3681	2031	9747.	1.00
4	1030			1027	3681	2330	9746.	1.00
5		1330		1027	3681	2025	9741.	1.20
ó		1037		1727	3681	2323	9739.	1.00
7		1930		1327		2016	9732.	
8		1030		1927	3681	2019	9723.	
9		1030		1027	3581	1992	9707.	1.00
	1030			1827		1960	3674.	0.99
16	1630				3681	1943	9657.	0.99
11				1227	3681	1924		
	1930			1327	3679		9616.	
	1039			1/27	3674	1855	9562.	
14				1027	3661	1798	9492.	
15	1030			1827	3649	1723	9424.	0.96
	.1030			1027	3634	1674	9340.	
	1030			1927	3604	1594	9230,	0,95
18		1030		1927	3546	1507	9085.	0.93
19		1029		1027	3486	1418	8935.	0.92
20		1028	945	1725	3396 .	1384	8728.	
. 21		1027		1824	3332	1261	8619.	
55		1020	945	1012	3157	1123	6287.	0.85
23		1012	931	952	2382	1003	7797.	0.80
24	957	982	901	869	2582	891	7192.	2.74
25	886	935	847	775	2255	779	5477.	0.66
26	831	899	805	734	2774	727	6070.	0.62
27	734	821	664	653	1696	616	5184.	0.53
28	640	676	540	548	1411	5.07	4322.	
29	553	562	459	427	1196	419	3616.	0.37
30	476	485	377	345	1935	362	3088.	0.32
31	453	463	356	289	972	333	2866.	0.29
32	424	414	301	223	851	279	2477.	0.25
33	352	367	253	188	719	245	2134.	0.22
34	312	319	219	1.48	584	203	1785.	0.18
35	258	292	178	120	481	160	1499.	0.15
36	249	266	1.65	109	443	141	1373.	0.14
37	212	233	136	99	369	116	1165.	0.12
38	181	202	1.1.1			97	956.	0.19
39	148	171	93	51	217.	68	748.	9.08
40	108		70	37	155	42	543.	Ø.06
41	97		58	26	135	31	469.	0.05
42	57	91	44	1.3	91	14	310.	0.03
43		66	- 26	5	55	6	195.	0.02
44	18	41	15	- 0	26	. 4	174.	0.01
45	10	27	.7	.0	13	3	69.	0.00
	1. 27	6	. /		10			0.00

TABLE 52 (cont.)

# CUMULATIVE PROSABILITY DISTRIBUTION FOR MOCKET MOTOR TEMPS CUCKOO EXT. TOP (TAIL)

		RECO	RDER	230.	ROCKET NOT	OR CHANNE	El. 5	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	6	18	6	Ø	10	2	42.	0.00
47	5	8	6	0	3	2	24.	0.09
48	2	4	5	Ø	1	1	1.3.	0.00
49	1	4	2	Ø	Э	Ø	7.	. 0.00
50	U	4	Ø	Ø	0	<sub>Ø</sub>	4.	0.00
51	Ø	3	Ø	Ø	Ø .	Ø	3.	Ø.20
52	C	3	9	Ø	a	. 0	3.	9.00
53	2	1.	Ø	7	3 .	Ø	1.	0.20
54	Ø	0	Ø	Ø	3	Ø	.0.	0.00

TABLE F2

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS CUCKOO PROP. SURFACE (TAIL)

					Q., ta	3		
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1.		1030		1027	3681	2032	9748.	1.00
5	1233	1030	948	1827	3681	2035	9748.	1.00
3	1030	1030	948	1727	3681	2032	9748.	1.00
4	1032	1030	948	1027	3681	2032	9748.	1.00
5	1030	1030	948	1327	3581.	2931	9747.	1.00
6	1030	1030	948	1027	3681	2029	9745.	1.00
7		1239		1027	3681	2026	9742.	1.00
8	1030	1030		1027	3681	2018	9734.	1.09
9	1332	1030		1727	3681	2007	9723.	1.00
17		1.030		1727	3681	1994	9710.	1.03
11		1030		1227	3681	1984	9705.	1.00
12	1830	1030		1227	3681	1952	9668.	0.99
13	1030	1030		1027	3680	1898	9613.	0.99
14	1832	1230		1027	3678	1837	9549.	0.96
15	1032	1030		1027	3664	1754	9451.	0.97
16	1033	1930		1827	3657	1699	9388.	0.96
17	1032	1030		1827	3636	1608	9276.	0.95
18	1032	1030	945	1227	3602	1500	9134.	0.94
19	1030	1030	945	1027	3558	1391	8981.	0.92
20		1030	945	1227	3494	1291	8817.	0.99
21		1030	945	1325	3462	1244	8736.	0.90
22	1030	1028	945	1020	3333	1153	8579.	0.87
23	1039	1024	944	987	3141	1039	8165.	9.84
24		1712	916	989	2861	930	7649.	0.78
25	968	993	893	828	2565	816	7063.	0.72
.26	937	977	860		2406	758	6714.	0.69
27	353	916	776	704	2011	657	5917.	0.61
28	753	821	625	609	1642	525	4978.	0.51
29	654	679	522	489	1324	433	4101.	0.42
30	569	589	435	364	1113	355	3425.	0.35
31	531	552	401	311	1311	329	3135.	0.32
32	461	481	349	238	842	270	2632.	0.27
33	400	410	283	176	673	214	2156.	0.22
34	334	348	223	135	555	159	1759.	0.18
35	287	285	180	96	425	123	1389.	0.14
36	251	250	169	79	367	1.03	1210.	0.12
37	193	210	118	57	287	75	943.	0.10
38	157	163	82	31	217	45	698.	0.07
39	118	128	59	19	144	21	489.	0.05
40	73	89	36	6	91.	1.5	308.	0.03
41	62	70	23	2	57	11	230.	0.02
42	5.9	41	14	. Ø	26	6	116.	0.01
43	16	19	10	0	9	4	58.	0.00
44	9	14	6	0	5	4	38.	0.00
45	. 4	10	4	Ø	7	3	21.	9.00

TABLE F2 (cont.)

#### CUCKOO PROP. SURFACE (TAIL)

47 3 7 1 2 8 3 11.	.PROB
47 3 7 1 9 9 3 11.	0.00
48 7 6 1 7 7 1 8	0.00
70 0 1 0 1	0.00
49 - 3 4 0 0 0 1 5.	0.00
50 0 4 0 0 0 0 4.	0.00
51 0 3 0 0 0 0 3.	0.00
52 0 3 0 0 0 0 3.	0.00
53 0 0 0 0 0 3.	0.00
54 7 3 0 0 0 0 3.	0.00
55 7 2 0 0 0 0 2	0.00
56 7 2 0 0 0 0 v 2.	0.00
57 0 1 0 0 0 0 1.	0.00
58 0 0 0 0 0 0 0.	0.00

JABLE GS

#### CUCKOO INT. PROP. SURFACE (TAIL)

0

C	DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
	1	1929	1031	948	1227	3689	2032	9747.	1.22
	2	1029	1031		1827	3582	2032	9747.	1.00
0	3	1029	1031		1027	3680	2032	9747.	1.02
<b>*</b>	4	1029	1331		1827	3682	2032	9747.	
	5		1031	948	1827				1.02
C	6	1029	1031		1727	3680	5059	9743.	1.02
	7	1029	1031			3682	2025	9740.	1.00
	8	1029	1031		1227	3680	2016	9733.	1.00
C					1327	3580	2005	9722.	1.00
	9	1.029			1227	3680	1995	9729.	1.33
	10	1029	1031		1027	3680	1969	9683,	0.99
-	11	1029			1027	3679	1957	9670.	0.99
0	12	1029			1027	3678	1921	9632.	0.99
	13	1029	1031		1027	3675	1879	9587.	0.98
_	14	1029	1031		1927	36.67	1821	9521.	0.98
C	15	1029			1027	3656	1750	9439.	3.97
	16	1029	1031	945	1027	3646	1700	9384.	0.96
	17			945	1927	3619	1623	9265.	0.95
C.	18	1029			1027	3563	1526	9121.	3.94
	19	1029		945	1227	3496	1442	8970.	0.92
	20	1029	1929	945	1326	3415	1347	8791.	0.90
C	21	1029	1023	945	1025	3351	1295 .	8673.	0.89
	22	1029	1021	945	1711	3159	11.72	3337,	1.86
-	23	1919	1012	942	956	2912	1044	7885.	9.81
C	24	976	991	902	874	2595	917	7255.	0.74
	25	907	939	856	795	2275	795	6567.	1.67
	26	847	917	814	752	2/187	734	6144.	0.63
0	27	752	820	672	668	1718	618	5240.	0.54
	28	650	698	547	572	1425	513	4425.	0.45
	29	557	581	462	444	1177	416	3637.	3.37
0	30	490	499	390	333	1014	353	3079.	0,32
	31	461	468	359	289	954	321	2852.	0.29
	32	414	425	297	233	900	279	2445.	1.25
0	33	352	368	256	181	663	. 227	2047.	7.21
	34	310	326	207	145	542	189	1720.	Ø.18 ·
	35	270	278	.171	111	442	151	1423.	0.15
0	36	247	260	152	1.07	409	128	1296.	0.13
	37	207	221	126	83	322	104	1063.	0.11
	38	172			60		80	859.	0.09
0	39	132	154	76	39	192	56	649.	0.07
	40	95	117	56	19	137	36	460.	0.05
	41	78	1.03	44	15	106	23	369.	0.04
0	42	48	72	26	5	71	8	230.	0.02
-	43	23	45	12	1	35	5	121.	0.01
	44	1.5	27	8	ø	17	4	71.	0.00
0	45	6	15	6	. 0	8	S	37.	0.03
	7.5	0	-	0	12	O		37.	0,00

TABLE G2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS CUCKOO INT. PROP. SURFACE (TAIL)

		RECO	RDER	23C.	ROCKET MOT	OR CHANNE	L 7 .	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	4	13	6	Ø	4	2	29.	0.00
47	2	7	2	Ø	1	2	14.	0.00
48	Ø	6	1	0	Ø	1	8.	0.00
49	Ø	4	1	Ø	Ø	Ø	5.	0.00
50	0	3	1	Ø	Ø	Ø	4.	0.00
51	Ø	3	1	2	Ø	Ø	4.	0.00
52	Ø	2	Ø	2	Ø	. 0	2.	0.00
53	Ø	1	Ø	Ø	Ø	Ø	1.	0.00
54	3	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

TABLE H2

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS CUCKOO EXT. BOTTOM (TAIL)

					Notice .	J		
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1029	1031	948	1827	3681	2032	9748.	1.00
2	1029	1031		1027	3681	2032	9748.	1.00
3	1029	1031		1027	3681	2032	9748.	1.00
4	1029	1031	948	1027	3681	2032	9748.	1.00
5	1029	1031	948	1027	3681	2032	9748.	1.00
6	1029	1,231	948	1327	3681	2032	0748	1.00
7		1031		1827	3681	2031	9747.	1.00
8		1031		1027	3681	2026	9741.	1.00
9		1.031	947		3681	2023	9738.	1.20
10	1029	1031		1827	3681	2017	9731.	
11		1031		1027	3681	2011	9725.	1.00
12		1.031		1027	3681	1993	9727.	1,00
13	1029	1331		1027	3681	1954	9668.	0.99
14	1029	1.031		1027	3681	1911	9625.	0.99
15	1029	1231		1027	3677	1845	9555.	0.93
16	1029	1231	946		3671	1795	9499.	0.97
17	1029	1231	945	1027	3659	1704	9395.	0,96
18	1029	1031	945	1027	3628	1606	9266.	0.95
19	1029	1031	945	1027	3581	1.485	9098.	0.93
20	1029	1031	945	1027	3524	1382	8938.	0.92
21	1029	1.031	945	1027	3489	1326	3847.	0.91
22	1029	1,030	945	1024	3373	1217	8618.	0.88
23	1029	1028	944	999	3152	1091	8243.	
24	1022	1018	919	921	2854	964	7698.	0.79
25	975	994	891	812	2518	828	7018.	0.72
26	943	972	850		2329	782	6652.	Ø.68
27	854	918	744	592	1909	651	5768.	0.59
28	740	798	597	588	1497	509	4729.	0.49
29	637	662	476	456	1156	379	3766.	0.39
30	529	550	384	319	923	298	3003.	0.31
31	492	515	346	257	832	264	2776.	0.28
32	414	433	284	197	651.	1.84	2163.	0.22
33	344	342	225	142	505	130	1688.	0.17
34	268	568	158	93	369	83	1239.	0.13
35	201	205	97	40	260	4.5	855.	0.09
36	176	178	86	40	221	28	729.	0.07
37	133	128	53	21	156.	17	511.	0.05
38	101	90	38	7	85	13	334.	0.03
39	67	59	22	1	46	10	275.	0.08
40	35	35	15	C	21	8	114.	0.01
41	23	25	11	0	11	3	78.	0.00
42	13	15	6	Ø	1 3	7	42.	0.02
43	6	9	3	Ø		5	23,	0.00
44	4	9	3 3 2	9.	7	4 3	50.	0.00
45	1	6	2	0	0	5	12.	0.00

TABLE H2 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR MOCKET MOTOR TEMPS

#### CUCKOO EXT. BOTTOM (TAIL)

		RECO	RDER	23C.	ROCKET HOT	OR CHANNI	EL 8	
DEG.	DEC.	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	1	5	1	9	Ø	2	9.	0.00
47	7	4	1	2	Ø	1	5.	0.03
48	Ø	3	0	9	3	1	4.	9.00
49	Ø	3	3	3	ð	Ø	3.	0.90
50	Ø	3	0	0	û	O	3.	9.03
51	Ø	3	Ø	2	Ø	W	3.	0.00
52	0	3	Ø	,3	C1	(J	3.	0.93
53	0	. 2	0	Ø	3)	Ø	2.	0.00
54	. 0	2	J	Ø	Ø	Ø	2.	0.00
55		. 07	01	7	(1	01	- 14	1 00

TABLE J2

CUMULATIVE PROBABILITY DISTRIBUTION FOR HOCKET MOTOR TEMPS

#### CUCKOO EXT. TOP (NOSE)

							•	
DEG.	DEC	NAU.	FEB	MAR	AUT-SPRING	WINTER	TOTAL	c.PROB
1		1732	948	1026	3681	2032	9747.	1.00
2	1028	1.732	948	1956	3681	2032	9747.	1.02
3	1028	1032	948	1326	3681	2032	9747.	1.03
4	1028	1032	948	1026	3681	2031	9746.	1.03
5	1028	1//32	948	1826	3681	2027	9742.	1.00
5	1028	1032	948	1826	3681	2023	9738.	1.00
7	1028		948	1026	3681	2016	9731.	1.00
8	1028		747	1326	3681	2013	9727.	1.00
9	1028		946	1026	3681	1996	9789.	1.00
10	1028	1832	946	1826	3581	1968	9681.	0.99
	1028			1726	3681	1958	9670.	
	1 28		945		3580	1926	9637.	
	1/28	1032	945	1026	3675	1889	9595.	0.98
14	1328	1032	945	1726	3668	1835	9534.	3.93
	1028		945	1026		1750	9438.	
	1028	1935	945	1326	3657	1789	9384.	0.97 0.96
16 17	1228	1032	945		3644		9258.	0.95
			944	1826	3613	1614		
18		1032		1026	3567	1537	9134.	0.94
19	1028	1231	944	1226	3506	1454	3989.	3,92
20	1/28	1030	944	1826	3419	1363	3810.	0.93
21	1028	1030	944	1824	3357	1310	8693.	0.39
22	1/428	1024	944	1014	3154	1229	8423.	0.85
23	1014	1012	938	963	2951	1095	7978.	0.32
24	978	934	906	889	2652	970	7379.	
25	910	935	860	799	2334	868	6726.	0.69
26	847	897	312	760	2170	805	6294.	Ø.65
27	744	850	673	674	1821	7.82	5434.	0.56
58	646	699	556	584	1524	586	4595.	0.47
59	571	585	477	463	1285	497	3883.	0.40
32	502	502	407	368	1139	425	3343.	0.34
31	472	483	377	321	1060	395	3128.	0.32
32	425	429	321	274	946	353	2748.	0.28
33	373	359	585	551	937	309	2411.	0.25
34	335	352	234	187	736	261	2135.	9.55
35	308	321	505	148	634	216	1829.	0.19
36	286	361	191	142	594	500	1714.	0,18
37	251	270	1.62	122	502	165	1473.	0.15
38	218	249	143	103	423	145	1281.	0.13
39	194	217	124	90	351	11/	1093.	0.11
40	158	1.87	101	65	282	94	887.	0.09
41	141	177	95	61	253	88	815.	0.08
42	126	142	67	44	183	61	623.	0.96
43	89	115	43	29	127	35	443.	0.05
44	57	92	36	19	93	19	316.	0.03
45	34	60	25	1.0	57	6	194.	- 0.22
			7,500					

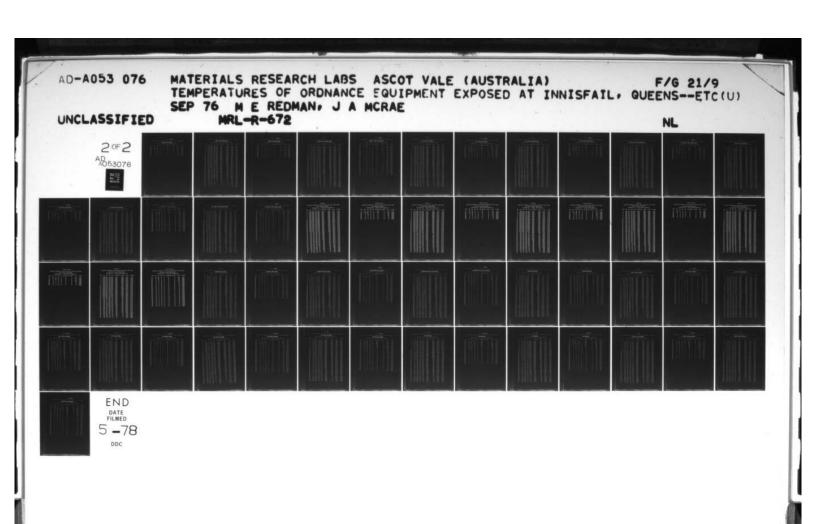


TABLE J2 (cont.)

#### CUCKOO EXT. TOP (NOSE)

		RECO	ROER	23C.	ROCKET MOT	OR CHANNE	L 9	
DEG.	DEC	JAN	FEB	FAM	AUT-SPRING	WINTER	TOTAL	C.PROB
46	24	46	15	7	42	5	139.	0.01
47	11	31	9	5	18	3	74.	0.20
48	5	16	5	0	3	2	37.	0.00
49	2	10	3	27	5	1	21.	. 0.22
5%	1	6	1	Ø	1	Ø	9.	0.20
51	7	3	1.	0	0	Ü	4.	0.28
52	Ø	2	0	9	Ø	Q	2.	0.00
53	3	1	0	3	Ø	6	1.	0.00
54	0	1	0		9	Ø	1.	0.22
55	9	Ø	3	Ø	5	Ø	0.	0.00

TABLE K2.

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

CUCKOO PROP. SURFACE (NOSE)

TABLE K2 (cont.)

### CUMULATIVE FROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS CUCKOO PROP. SURFACE (NOSE)

		RECO	RDER	230.	ROCKET MOT	OR CHANNE	L 10	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	Ø	5	. 1	2	3	5	9.	9.98
47	2	5	1	(3	a	3	9.	0.00
48	9	4	1	7	0	5	1.	0.00
49	27	4	Ø	Ø	Ø	5	6.	0.00
50	2	4	0	J	ij	1	5.	0.00
51	2	3	0	Ø	0)	1	4.	0.23
52	3	3	2	0	g	9	3.	0.00
53	Ø	3	Ü	2	. 0	Ø	3.	0.00
54	2	3	Ø	Ø	Ø	Ø	3.	0.20
55	Ø	2	Ø	0	Ø-	W	2.	0.03
56	3	2	0	0	1	Ø	2.	0.23.
57	2	1.	Ø	P	1	Ð.	1.	0.00
58	0	O	Ø	2	9	N	<i>v</i> .	0.00

TABLE L2

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

CUCKOO INT. PROP. CHARGE (NOSE)

RECORDER 23C. ROCKET MOTOR CHANNEL 11

DEG.	OEC	MAL.	FEB	MAR	AUT-SPRING	WINTER	TOTAL	O.PROB
1	1029	1032 .	949	1028	3679	2031	9747.	1.30
2	1629	1932	948	1728	3679	2031	9747.	1.00
3	1729	1732	948	1328	3679	2031	9747.	1.00
4	1329	1032	948	1828	3679	2028	9744.	1.00
5	1829	1032	948		3679	2026	9742.	1.30
6	1829	1.732	948	1028	3679	5055	9741.	1.00
7	1329	1032	948		3679	2021	9737.	1.00
8.	1029	1932	947		3679	2012	9727.	1,00
9	1055	1232		1028	3679	2000	9715.	1.03
	1029	1032	947	200	3679	1977	9692.	3.99
	1029	1032	947		3679	1971	9686.	0.99
	1729	1032		1928	3678	1939	9652.	0.99
13	1029	1032	946	1228	3677	1904	9616.	0.99
14	1929	1332		1828	3670	1849	9554.	0.98
15	1029			1028	3654	1770	9459.	0.97
16		1032		1028	3652	1726	9411.	
17	1029	1032	945		3621	1647	9302.	0.95
18	1029	1/32	945	1028	3580	1567	9181.	0.94
19	1029	1032	945	1028	3517	1492	9943.	0.93
. 20	1029	1036	945	1523	3442	1389	8863.	0.91
21	1029	1.030	945	1028	3391	1341	8764.	0.90
	1029	1024	945	1024	3237	1216	8475.	Ø.87
22	122	1916	943	987	2985	1099	8045.	0.83
24	997	298	912	896	2694	978	7468.	0.77
	921	954	871		2395	875	6835.	3.70
25	876	923	821	819 783		816	6432.	
26 27	767		711	688	2216 1853	695	5562.	0,66
23	668	135		589	1515	578	4661.	0.48
29			576			477	3891.	
	582	607	488	458	1279			0.43
39	505	517 494	411	359	1118	404	3314.	0.34
31 32	481	444	372	311	1253	365 316	3076. 2676.	0.32
33			330	254	967	275	23/4.	0.27
34	375 329	398 342	273	204	779		1937.	0.20
35	505	300	227	165	648	226 186	1654.	
36			191	135	550			0.17
37	269	292	187	117	497	162	1517.	0.16
	227	248	149	97	404	131	1256.	
38	195	210	1.23		325	110	1037.	
39	162	184	94	53	249	8/	829.	0.09
49	128	145	70	37	163	64	627.	0.06
41	129	128	60	31	158	50	536.	0.05
42	70	100	44	14	110	29	367.	0.04
43	47	70	24	. 8	63	11	228.	0.02
44	24	48	1.4	3	42	7	138.	0.01
45	12	29	7	2	20	4	74.	0.00

0

0

TABLE L2 (cont.)

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS CUCKOO INT. PROP. CHARGE (NOSE)

RECORDER 23C. ROCKET MOTOR CHANNEL 11 DEG. DEC JAN FEB MAR AUT-SPRING WINTER TOTAL C.PROB 55. 0.00 26. 0.00 0.00 12. 0.00 8. 6. Ø 0.00 6. 0.00 4. 0.00 3. 0.03 2. 3.00 2. 0.00 O 2. 3.00 Ø 2. 0.30 3.03 2. 2. 0.00 2. (1) 0.00 ø 2. 0.00 2. Ø 0.00 5. 3.33 1) 0,09 5. 2. 0.00 O 2. 0.00 2. 0.36 a 2. Ø V. 0.00 5. 0.00 2. () 3.00 1. 2. 0.00 .72 ø 1. 0.00 1. 3.00 1. 0.00 1. 0.00 Ø 1. 0.00

0.00

TABLE M2

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5603 EXT. TOP (TAIL)

DEG.	DEC	. JAII	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1.26	1031	947	1027	3676	2030	9737.	1.00
2		1031		1227	3676	2/13/2	9737.	1.00
3		1031		1027	3576	2030	9737.	1.00
4		1231		1027	3676	2029	9736.	1.00
5		1031		1827	3676	2028	9735.	1.00
6		1931		1027	3576	2023	9730.	1.00
7		1031		1027	3576	2014	9721.	
8		1030		1327	3676	2003	9708.	1.00
9		1937		1/27	3676	1987	9692.	1.00
10 .	1026	1930	946	1327	3676.	1956	9661.	0.99
11	1/26	1030		1827	3576	1935	9640.	0.99
12.	1/26	1035	946	1.027	3574	1908	9611.	0.99
13	1.126	1230	946	1827	3672	1864	9565.	0,98
14	1/26	1030		1827	3664	1818	9511.	0.98
15	.1026		945	1027	3635	1739	9402.	0.97
16	1026		945		3621	1693	9342.	
17		1030	945	750	3586	1610	9224.	0.95
18	1026	1030	945		3533	1540	9101.	0.93
19	1026				3466	1454	8947.	0.92
20		1328	944	1025	3370	1362	8755.	
21	1826	1/25	944	1023	3287	1308	8613.	0.88
22		1017	944	-	3375	1166	8238.	0.85
23	1005	994	933	945	2774	1036	7684.	0.79
24	940	955	894	846	2411	893	6939.	0.71
25	834	875	818	769	2379	791	6166.	
26	776	831	767	728	1903	735	5732.	0.59
27	663		638	640	1583	620	4889.	0.50
28	555	627	513	537	1348	519	4099.	0.42
29	493	515	438	414	1187	454	3501.	0.36
30	451	459	382	319	1265	406	3082.	
31 32	433	439	353	279	1006	389	2899.	0.30
33	394	398	305	234	907	295	2578. 2293.	Ø.26
34	363	376 351	256 227	199	804 698	250	2025.	Ø.24 Ø.21
35	334	322	196	144	594	505	1762.	0.18
36	291	306	187	130	553	184	1651.	0.17
37	260	273	166	108	471	150	1428.	0.15
38	234	253	1.45	89	395.	119	1236,	
39	201	219	124	71	307	96	1018.	0.10
40	1.74	198	104	40	236	62.	814.	0.08
41	162	181	92	34	204	47	720.	0.07
42	138	1.49	71	- 20	157	19	554.	0.96
43	110	124	48	9	119	11	421.	0.04
44	93	106	25	.5	82	6	318.	0.03
45	78	79	1.8	2	59	5	239.	0.02
			-	-				

TABLE M2 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5603 EXT. TOP (TAIL)

DEG.	DEC	JAH	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	75	67	16	1	41	v	200.	9.02
47	55	50	3	7	23	Ø	136.	2.31
48	41	31	5	a	10	Ø.	87.	0.00
49 .	5.2	22	3	3	3	JØ	50.	. 9.90
50	1.1	17	2	Ø	1.	Ø	31.	0.10
51	8.	11	2	0	Ø	Ø	21.	0.00
52	3	6	1	Ø	b	Ø	10.	0.00
53	2	3	1	9	Ø	69	6.	6.59
54	Ø	2	1	0	Ø	Ø	3.	0.00
55	0	1	1	9	Ø	.0	2.	0.00
56	9	1.	1	Ø	2)	Ü	2.	0.00
57	Ø	1	1	9	0	IJ	2.	0.00
58	7	Ø	Ø	9	Ø	Ю	ø.	0.00

TABLE N2

### CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5603 PROP. SURFACE (TAIL)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1027	1931	946	1327	3678	2030	9739.	1.00
2		1031		1027	3678	2030	9739.	
3		1/31		1727	3578	2036	9739.	1.00
4		1031		1/27	3678	2030	9739.	1.00
5		1031		1027	3678	2026	9735.	1.00
6		1031		1027	3678	2023	9732.	1.00
7		1031		1027	3678	2012	9721.	
8		1831		1327	3577	2003	9711.	
o		1931		1827	3677	1989	9696.	
10		1031		1/27	3677	1965	9672.	0.99
11		1.031		1727	3676	1946	9652.	0.99
12				1327	3576	1913		Ø.99
							9619.	
13	1027	1031		1327	3672	1859	9561.	Ø.98
14		1231		1.327	3560	1801	9491.	8.97
15		1//31		1327	3637	1718	9385.	
16		1031		1027	3623	1671	9324.	
17		1031		1/27	3574	1585	9188.	Ø.94
13		1931		1/27	3523	1511	9263.	0.93
10		1030		1027	3460	1426	8915.	8.92
20		1029		1027	3355	1333	3714.	
21.		1028			3285	1282	8589.	
55		1.718		1013	3075	1151	8227.	
23	1015	998	931		2761	1021	7669.	0.79
24	956	965	897	847	2422	890	6977.	0.72
25	854	896	832	759	2111	789	6232.	0.64
20	787	856	785	717	1935	716	5796.	
27	679	768	640	643	1608	615	4954.	
28	575	651	512	531	1359	516	4144.	
53	512	525	445	416	11,95	455	3548.	0.36
30	461	457	383	320	1067	411	3099.	0.32
31	444	445	364	280	1320	335	2933.	0.30
32	426	411	319	244	922	334	2635,	0.27
33	372	382	272	505	819	. 285	2332.	0.24
34	339	357	235	162	716	242		0.21
35	316	322	.2012	140	614	224	1798.	0.18
36	293	31.0	196	133	557	189	1673.	0.17
37	277	278	170	111	484	149	1462.	0.15
33	244	253	149	95	399	120	1266.	0.13
39	216	230	129	8.7	315	99	1069.	9.11
40	181	194	104	55	253	63	850.	0.09
41	171	184	97	44	217	51	764.	0.08
42	144	148	74	25	170	25	586.	3.05
43	118	129	50	15	129	1.1	452.	0.05
44	98	108	33	6	87	8	349.	0.03
45	84	84	21	3	62	5	259.	9.03

TABLE N2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET HOTOR TEMPS LAP. 5603 PROP. SURFACE (TAIL)

		RECO	RDER	23C.	ROCKET MOT	OR CHANNE	IL 14	
DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	77	72	16	2	51	2	223.	V.02
47	59	55	11	1	23	Ø	149.	0.02
48	46	31.	7	2	15	Ð	99.	0.01
49	29	23	.6	3	4	W	62.	0.00
50	13	15	3	(A	1	U	32.	. 0.22
51	12	11	3	63	Ø	90	26.	0.03
52	3	6	2	21	Ø.	Ø	11.	0.00
53	1	3	2	.7	Ø	. 0	6.	3.03
54	Ø	1	1	7	Ø	Ø	2.	0.00
55	7	1	1	0	Ø	Ø	2.	0.00
56	-9	0	1	3	Ø	IJ	1.	Ø.90
57	Ø	Ø	Ø	7	Ø	Ø	u.	0.20

TABLE 02

#### LAP. 5603 INT. PROP. CHARGE (TAIL)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1027	1831	946	1028	3675	2031	9738.	1.00
2		1031		1023	3675	2031	9738.	
3	1027	1831		1028	3675	2331	9738.	
4		1231		1328	3675	2028	9735.	
5		1031		1228	3675	5052	9732.	
6		1031		1828	3675	5057	9728.	1.00
7		1231		1028		2016	9722.	1.28
8		1031		1328		2007	9713.	
9		1031		1028	3675	1986	9691.	
10		1231		1028	3675	1955		
		1231		1028	3574	1942	9660. 9646.	
11								0.99
12		1231		1328		1893	9597.	
13		1931		1928	3668	1859	9548.	
14		1031		1028	3658	1784	9472.	
15		1831		1026	3639	1712	9381.	
16		1231		1728	3530	1661	9321.	0.95
17		1231		1228	3573	1575	9132.	0.94
18		1031		1028		1516	9072.	0.93
19		1030		1028		1444	8931.	
2/		1029		1327		1358	8720.	
21		1028		1926		1282	8605.	
55		1217	943		3105	1171	8277.	0.85
23		1201		965	2816	1955	7779.	8.83
24	974	976	904		2479	919	7124.	
25	873	912	854	783	2146	875	6378.	
.26	815	870	795	753	1996	746	5975.	0.61
27	689	774	659	563	1651	651	5087.	
28	583	663	527	558	1393	533	4254.	
29	520	537	448	432	1235	466	3638.	0.37
30	465	467	393	338	1105	412	3150.	Ø.33
31	447	451	365	300	1057	393	3213.	0.31
32	488	410	322	251	943	346	2688.	0.28
33	376	384	278	508	825	292	2361.	0.24
34	343	356	243	180	728	254	2184.	0.22
35	318	328	206	148	631	216	1847.	0.19
36	374	317	199	134	585	193	1732.	0.13
37	277	283	1.78	116	499	161	1514.	8.16
38	249	261	157	99	416	132	1314.	
39	559		134	84	334	1006	1113.	0.11
40	186		110	63	258	75	897.	0.09
41	177		100	49	559	64	811.	3.08
42	149		79	37	171	35	623.	0.06
43	126		54	14	139	14	481.	0.05
44	124		31.	7	103	10	366.	0.04
45	84	89	23	5	63	4	268,	0.03

TABLE 02 (cont.)

### LAP. 5603 INT. PROP. CHARGE (TAIL)

		RECO	RDER	230.	ROCKET MOT	OR CHANNE	L 15	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	79	78	18	3	55	1.	234.	0.02
47	60	56	12	1	26	W	155.	0.02
48	47	36	7	Ø	15	0 -	125.	0.21
49	32	24	5	Ç.	7	ω.	66.	0.00
59	16	16	3	0	1	. 2)	36.	0.00
51	9	13	2	0	Ø	Ø	24.	0.00
52	3	5	1	7	ð	. 0	9.	0.30
53	1.	3	1	Ø	Ø	Ø	5.	0.20
54	Ø	3	1.	P	Ø	Ø	4.	0.30
55	. &	1.	1	0.	Ø	Ø	2.	0.33
56	Ø	6	1.	Ø	N	Ø .	1.	0.00
57	0	0	1.	2	প্র	Ø	1.	0.00
58	Ø	0	Ø	Ø	Ø	Ø	Ø.	6.03

TABLE P2

CUMULATIVE PROBABILITY DISTRIBUTION FOR MOCKET MOTOR TEMPS

LAP. 5603 EXT. BOTTOM (TAIL)

DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1027	1030	947	1829	3676	2031	9739.	1.00
2		1030		1028	3676	2931	9739.	
3				1028	3676	2031	9739.	
4				1028	3676	2030	9738.	1.00
5				1028	3676	2026	9734.	1.00
6				1228	3676	2024	9732.	
7		1030		1028	3676			1.30
						2019	9727.	1.00
8		1838		1/28	3676	2008	9715.	1.00
9		1030		1228	3676	1994	9781.	1.30
	1027			1828	3675	1964	9678.	
11		1030		1728	3675	1949	9655.	
	1.027			1028	3675	1913	9619.	0.99
13		1,030		1028	3675	1872	9578.	0.98
14		1036		1928	3668	1823	9522.	0.98
15				1028	3644	1749	9423,	Ø.97
16		1030		1028	3628	1701	9359.	0.96
17		1030		1958	3588	1619	9237.	W.95
1.8		1939		1328	3534	1538	9101.	0.93
19		1030		1028	3476	1445	8953,	7.92
54	1887	1027		1027	3368	1348	8741.	0.90
21	1927	1926	944	1025	3295	1292	8619.	0.88
55	1027	1019	944	1008	3082	1160	8240.	0.85
23	1018	1802	939	948	2781.	1032	7720.	0.79
24	969	969	907	857	2434	891	7027.	0.72
25	872	908	843	781	2106	781	6289.	0.65
26	817	869	787	745	1941	724	5876.	0.60
27	689	774	652	645	1592	625	4977.	0.51
28	578	659	518	539	1344	512	4150.	2.43
29	505	529	444	409	1192	438	3517.	0.36
30	459	468	382	310	1371	394	3084.	6.32
31	445	442	351	274	1925	369	2906.	0.30
32	399	398	314	228	900	316	2555.	0.26
33	367	372	272	197	799	276	2283.	0.23
34	339	349	236	163	678	230	1995.	0.20
35	396	314	203	142	588	184	1737.	0.18
36	204	300	191	132	543	165	1623.	0.17
37	250	267	169	120	452	133	1400.	0.14
38	226		147		362	125	1187.	0.12
39	198	808	125	84	277	75	967.	0.10
40	170	182	99	71	213	39	774.	0.08
41	155	162	67	67	189	28	681	0.07
42	137	136	66	33	144	12	528.	0.05
43	106	112	41	23	100	8	390.	0.04
44	88	93	20	13	64	4	282.	0.03
45	76	69	14	6	43	1	209.	0.02
	, 0	0.	7.4	0	70.	J.		17 . KI C

TABLE P2 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5603 EXT. BOTTOM (TAIL)

		RECO	RDER	23C.	ROCKET MOT	OR CHANNE	L 16	
DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	72	57	13	4	29	1	176.	6.02
47	54	39	8	3	14	Ø	118.	0.01
48	34	26	7	Ø	6	Ø	7.3.	0.00
49	18	18	4	a	1 .	. 0	41.	20.80
50	7	9	3	Ø	. 3	- 69	19.	0.00
51	5	8	3	a	Ø	()	16.	0.00
52	3	4	2	2	0	. Ø	9.	0.00
53	2	1	g	9	2	Ø	1.	0.00
54	Ø	0	2	Ø	Ø	И	0.	0.00

TABLE 02

### LAP. 5603 PROP. SURFACE (NOSE)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1027	1030	947	1028	3676	2031	9739.	1.00
2		1030		1228	3676	2031		
3		1030		1028	3676	2031	9739. 9738.	
4		1030		1023				1.00
5.		1230		1023	3676	2030	9738.	
		1237			3676	2020	9734.	1.00
6				1.028	3676	2326	9734.	1.20
7		1230		1028	3676	2017	9724.	1.00
3		1037		1828	3676	2008	9714.	1.33
9		1037		1028	3676	1995	9699.	1.00
10		1030		1228	3676	1964	9670.	8.99
11		1036		1028	3676	1946	9652.	0.99
12		1030		1228	3675	1999	9614.	0.99
13		1930		1823	3672	1870	9572.	0.98
14		1030		1728	3661	1805	9496.	2.93
15		1030		1.023	3641	1739	9429.	
16		1030		1228	3627	1695	9351.	0.95
17		1030	945	1028	3587	1602	9218.	0,95
18		1230		1228	3523	1528	9094.	0.93
19		1728	944	1/28	3465	1442	8933.	0.92
20		1027	944	1225	3347	1352	5721.	2.92
21	1/126	1.023	944	1022	3273	1308	8596.	3.88
22	1026	1.014	944	998	.3356	1174	3212.	3.84
23	1614	997	921	928	2754	1032	7626.	0.78
24	955	958	886	816	2415	909	6939.	7.71
25	853	891	818	742	2098	799	6231.	3.64
.26	785	851	768.	703	1937	751	5800.	0.63
27	670	152	619	626	1589	635	4889.	2.50
28	564	521	503	524	1365	53%	4187.	0.42
29	496	513	433	417	1208	472	3539.	0.36
30	453	458	373	313	1086	425	3135.	0.32
31	441	443	344	279	1930	406	2943.	3.33
32	395	397	307	231	921	348	2599.	0.27
33	350	373	255	195	807	315	2385.	0.24
34	331	351	230	163	712	271	2058.	2.21
35	394	314	200	144	618	221	1871.	0.18
36	239	299	186	131	5 <b>7</b> 5	207	1687.	0.17
37	251	271	164	116	478	1.65	1455.	0.15
38	231	241	147	99	419	135	1272.	0.13
39	290	211	122	82	315	197	1037.	0.11
40	158	182	93	65	227	71	812.	0.08
41	160	167	85	52	203	59	726.	0.07
42	137	137	66	33	160	33	559.	0.06
43	107		40	22	131	15	428.	0.04
44	92	94	25	9	85	8	311.	0.03
45	77	71	17	5	51	4	225.	0.02
							-6	

TABLE .U2 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET NOTOR TEMPS

LAP. 5603 PROP. SURFACE (NOSE)

•		RECO	RBER	23C.	ROCKET MOT	OR CHANNE	L 17	
DEG.	DEC.	JAN .	FEB	MAR	AUT-SPRING	WINTER	TOTAL	c.PRog
46	71	60	15	. 3	41	2	192.	0.92
47	54	38	11	1	. 18	N	122.	0.01
48	35	25	8	n	17	;)	78.	0.00
49	21	19	6	ũ	1	14	47.	6.33
50	9	9	2	0	0	Ø	20.	9.33
51	7	7	1	Ø	01	Ø	15.	2.23
52	. 1	. 4	1.	Ø	3	Ø	-6.	3.03
53	3	. 1	. 1	Ø	Ø.	Ø	2.	0.00
54		. 0	1	Ø	Ø	Ü	1.	0.00
55	2	0	1	Ø	3	Ø.	1.	0.90
56	3	, a	1	a	Ø	W	. 1.	3.50
57 .	. 2.	. 0	1	. 0	Ø	Ø	1.	0.00
58	· 3 ·	0	1	6	Ø	6.	1.	3.83
59	3	0	1	G	Ø	, W	1.	3.43
63	. 3	0	1	Ø	Ø	.0	1.	3,00
61	3	0	1	9	3	, k	1.	0.23
62	Ø	0	1	Q	7,	Ø	1,	0.00
63	2	Ø	1	Ø	8	. &	1.	0,00
64	2	7	1	. 0	0	· v	1.	0.00
65	3	2	1	a	c	Ŋ	1,	2.23
66	75	0	1	. Ø	Ø	U .	1.	0.00
67	. 7	Ø.	a	7	<b>a</b> .	И	31	50 . 51.01

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TABLE R2

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5603 INT. PROP. SURFACE (NOSE)

DEG.	OEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1027	1031	947	1029	3675	2731	9742.	1.20
2		1031		1329	3575	2031	9740.	1.00
3	1827	1731		1029	3675	2031	9740.	1.00
4	1027	1231	947	1329	3675	2030	9739.	1.03
5	1827	1031	947	1729	3675	2227	9736.	1.00
6	1827			1029	3675	5055	9731.	1.00
7	1827	1/31	947	1329	3675	. 2016	9725.	1.02
8	1027	1231	946	1329	3675	2026	9714.	1.00
9	1027	1 31	946	1329	3675	1983	9691.	9.99
10	1927	1031	946	1329	3675	1961	9569.	3.99
11	1/27	1031		1029	3675	1941	9649.	0.99
12	1027	1031	946	1029	3674	1895	9600.	0.99
13	1027	1031	946	1029	3666	1845	9542.	0.98
14	1027	1031		1029	3654	1781	9468.	0.97
15		1/31		1956	3633	1701	9366.	0.96
16		1231		1/29	3616	1658	9386.	0.95
17	1227	1031	945	1929	3581	1583	9196.	0.94
18	1327	1731	945	1320	3522	1508	9362.	0.93
19	1327	1032	944	1029	3459	1424	8913.	0.92
20	1327	1027	944	1029	3355	1319	8721.	0.89
21	1027	1027	944	1327	3292	1271	8588.	0.88
22	1027	1217	944	1314	3382	1154	3236.	0.85
23	1916 962	998	927	963	2800	1017	7721. 7038.	0.79
25	354	597	841	867 785	2455 2122	792	6291.	0.72
26	822	847	791	744	1943	742	5869.	0.60
27	676	764	656	652	1618	633	4999.	0.50
28	573	637	513	540	1369	5210	4157.	0.43
29	493	519	446	417	1220	462	3562.	7.37
30	455	463	375	324	1795	416	3128.	0.32
31	441	443	350	287	1244	394	2964.	0.30
32	483	434	31.4	246	934	. 343	2644.	0.27
33	366	375	270	201	326	31.0	2348.	0.24
34 .	336	352	239	1.73	718	266	2084.	0.21
35	305	321	.213	149	629	210	1836.	0.19
36	294	301	200	138	590	231	1724.	0.18
37	263	274	176	117	493	164	1.457.	0.15
38	236	247	152	98	409	139	1281.	
39	203	214	127	81	317	108	1959.	0.11
43	176	186	104	66	239	86	857.	0.09
41	162	174	98	52	217	61	770.	0.08
42	142	143	73	31	171	33	593.	0.06
43	114	118	50	19	138	1/	456.	0.05
44	94	102	31	7	93	,	334.	0.03
45	79	77	5.5	5	57	5	243.	0.02

TABLE R2 (cont.)

### LAP. 5603 INT. PROP. SURFACE (NOSE)

		RECO	RUER	23C.	ROCKET MOT	OR CHANNE	L 18	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	76	64	1.7	4	45	5	229.	2.32
47	55	5.3	11	1.	25	0	142.	0.01
43	42	26	9	1 .	14	U	. 35.	0.00
49	23	20	7	1	4	0	55,	3.33
50	11	12	4	1	1	υ	29.	0.00
51	7	11	5	1	1	Ø	55.	3.02
52	1	4	1	1	1	Ø.	8.	2.00
53		5	1	1	1	0	5.	0.00
54	2	2	1	1	1	9	٥.	0.03
55	2	1	1	1	1	M	4.	2.90
56	J	1	1	1	1	.3	4.	0.22
57	Ø	1	1	1	1	ý.	4.	0.00
58	3	1	1	1.	1	W.	4.	0.02
59	7	1	1	1	1	Ø	4.	0.00
60	77	1	1	1	1.	Ð	4.	0.00
61	7	1	1	1	1	J	4.	0.20
62	3	1	1	1	1	0	4.	ଉ.ହର
63	3	1	1	1	Ø	Ü	3.	0.00
64	Ø	1	1	1	Ŋ	¥ð	3,	0.00
65	3	1	1	1	0	U	3.	0.00
66	Ø	1	1	1	3	Ø	3.	3.00
67	Ø	1	Ø	1.	Ø	S)	2.	0.00
68	J	1	Ø	1.	И	v3	2.	2.32
69	Ø	1	Ø	1.	Ø	M	2.	0.00
70	Ø	1	Ø	1	2	0	2.	0.00
71	Ø	1.	· Ø.	1	0		2.	0.00
72	Ø	Ø	0	1	Ø,	D	1.	2.93
73	Ø	Ø	Ø	1	Ø	()	1.	0.00
74	Ø	0	9	1	Ø	U	1.	0.00
75	Ø	0	Ø	1	Ø	٥	1.	0.00
76	O	Ø	Ø	1	3	Ø	1.	2.00
77	07	(7	07	1	CA	M.	VI.	0.00

TABLE S2

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 EXT. TOP (TAIL)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1027	1030	947	1028	3674	2031	9737.	1.00
2	1027	1030	947		3674	2031	9737.	1.00
3	1027	1030	947		3674	2031	9737.	1.00
4	1027	1030	947		3674	2030	9736.	1.00
5	1027	1030	947	1028	3674	2026	9732.	1.00
6	1027	1030	947	1028	3674	2025	9731.	1.00
7	1027	1030		1028	3674	2020	9725.	1,00
8	1027	1030		1028	3674	2012	9717.	1.00
9	1027	1030		1028	3674	1979	9684,	0,99
10	1027	1030		1028	3674	1954	9659.	0.99
11	1027	1030		1028	3673	1935	9639,	0,99
12	1027	1030		1028	3672	1894	9597.	0,99
13	1027			1028	3666	1846	9543,	0,98
14	1027	1030		1028	3659	1787	9477.	0.97
15 16	1027	1030		1028	3628 3622	1784 1659	9363, 9312,	0,96
17	1027	1030	945	1028	3573	1572	9175.	Ø.94
18	1027	1030	945	1028	3514	1486	9030.	0.93
19	1027	1030	944		3444	1413	8886.	0,91
20	1027	1026	944	1027	3316	1316	8656.	0.89
21	1027	1025	944	1025	3238	1265	8524.	0.88
22	1027	1017	944	1011	3228	1126	8153.	0.84
23	1014	995	932	930	2719	1002	7592.	0,78
24	943	952	896	839	2380	887	6897,	0.71
25	834	885	828	759	2061	774	6141.	0.63
26	779	841	783	725	1915	718	5761.	0,59
27	647	739	629	637	1589	621	4862.	0,50
28	569	611	515	542	1347	521	4105.	0.42
29	494	513	440	418	1193	453	3511.	0,36
30	448	457	374	325	1076	409	3089.	0.32
31	423	432 400	344	287	1022	390 347	2898, 2613,	Ø,30 Ø,27
33	397 367	361	269	200	923 823	299	2319,	0.24
34	328	334	246	172	708	254	2042.	0.21
35	297	312	212	153	607	211	1792.	0.18
36	284	291	199	142	560	191	1667.	0,17
37	250	270	173	121	476	152	1442.	0.15
38	218	244	154	103	405	122	1246.	0.13
39	196	217	135	89	324	96	1057,	0.11
40	166	195	118	70	252	68	869.	0.09
41	154	178	102	65	220	51	770.	0.08
42	117	143	81	45	165	22	573,	0.06
43	89	104	64	28	116	12	413,	0.04
44	68	88	48	19	74	ý	306.	0.03
45	39	68	29	8	46	5	195.	0.05

TABLE S2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 EXT. TOP (TAIL)

		RECO	RDER	23Ç.	ROCKET MOT	OR CHANNI	EL 19	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	30	54	22	4	28	3	141.	0.01
47	19	32	7	Ø	10	2	70.	0.00
48	10	20	7	0	3	Ø	40.	0.00
49	6	12	4	Ø	0	Ø	22.	0.00
50	4	9	2	Ø	Ø	Ø	15.	0.00
51	3	7	1	Ø	Ø	Ø	11.	0.00
52	1	. 7	1	Ø	Ø	Ø	9.	0.00
53	Ø	. 2	Ø	Ø	0	Ü	2.	0.00
54		a	a	a	a	ä	a	0 00

TABLE T2

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

LAP. 5604 PROP. SURFACE (TAIL)

TABLE T2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 PROP. SURFACE (TAIL)

		RECO	RDER	23C.	ROCKET MOT	OR CHANNE	L 20	
DEG.	DEC.	JAN	FEB	MAR	AUT_SPRING	WINTER	TOTAL	C.PROB
46	28	51	19	3	28	2	131.	0.01
47	17	29	9	Ø	12	1	68.	0.00
48	8	18	6	Ø	3	Ø	35.	0.00
49	7	10	4	Ø	Ø	Ø	21.	0.00
50	4	8	1	Ø	0	Ø	13.	0.00
51	3	7	1	Ø	Ø	Ø	11.	0.00
52	Ø	. 3	Ø	Ø	Ø	Ũ	3.	0.00
53	Ø	. 2	Ø	Ø	Ø	Ø	2.	0.00
54	0	Ø	Ø	Ø	0	Ø	Ø.	0.00

TABLE U2

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 INT. PROP. CHARGE (TAIL)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1028	1030	947	1028	3674	2030	9737.	1.00
2	1028	1030		1028	3674	2030	9737.	1.00
3	1028	1030	947	1028	3674	2030	9737.	1.00
4	1028	1030	947	1028	3674	2029	9736.	1.00
5	1028	1030	947	1028	3674	2028	9735.	1,00
6	1028	1030		1028	3674	2024	9731.	1.00
7	1028	1030		1028	3674	2016	9722.	1.00
8	1028	1030		1028	3674	2007	9713.	1.00
9	1028	1030		1028	3674	1979	9685.	0.99
10	1028	1030		1028	3674	1935	9641.	0.99
11	1028	1030		1028	3674	1914	9620.	0,99
12	1028	1030		1028	3671	1880	9583.	0,98
13	1028	1030		1028	3665	1839	9536.	0.98
14	1028	1030		1028	3659	1765	9456.	0,97
15	1028	1030	945 945		3629	1677 1635	9337. 9280.	Ø.96 Ø.95
16 17	1028	1030	945	1028	3614 3573	1557	9161.	0.94
18	1028	1030	945	1028	3518	1483	9032.	0.93
19	1028			1028	3462	1391	8882.	0.91
20	1028	1026	944	1026	3372	1297	8693.	Ø.89
21	1028	1025	944	1024	3301	1249	8571.	0.88
22	1028	1018	944	1011	3114	1143	8258.	0.85
23	1019	1000	929	949	2808	1006	7711.	0.79
24	964	969	897	859	2497	882	7068.	0.73
25	875	912	851	779	2172	781	6370.	Ø.65
26	815	867	811	741	2027	727	5988.	0.61
27	690	764	654	663	1703	619	5093.	0.52
28	590	651	530	552	1417	520	4260.	0,44
29	511	525	445	440	1236	454	3611.	0.37
30	461	466	386	351	1117	404	3185.	0.33
31	442	446	357	309	1063	381	2998,	Ø.31
32	404	407	315	253	955	330	2664.	0.27
33	372	376	281	206	862	292	2389.	0,25
34	341	339 314	250	172 153	745 643	25Ø 216	2097. 1851.	0.19
36	290	302	205	144	595	192	1728.	Ø.18
37	258	275	179	120	514	160	1506.	0.15
38	227	248	154	106	423	127	1285.	0,13
39	201	218	138	89	336	102	1084.	0.11
40	170	198	116	65	265	76	890.	0.09
41	154	183	102	60	226	60	785.	0.08
42	123	146	73	41	167	30	580.	0.06
43	93	113	60	29	131	13	439.	0.05
44	66	93	38	18	86	9	310.	0.03
45	40	66	22		49	4	190.	0.02

TABLE U2 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 INT. PROP. CHARGE (TAIL)

		RECO	RDER	23C.				
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	34	52	18	4	34	2	144.	0.01
47	17	29	8	Ø	13	2	69.	0.00
48	9	18	5	0	5	1	38.	0.00
49	7	11	2	Ø	1	Ø	21.	0.00
50	4	7	2	0	Ø	Ø	13.	0.00
51	3	6	ī	ø	Ø	Ø	10.	0.00
52	Ø	3	1	Ø	Ø	Ó	4.	0.00
53	Ø	. 1	Ø	Ø	Ø	Ø	1.	0.00
54	Ø	0	a	a	Ø	Ó	Ø.	9.99

TABLE V2

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 EXT. BOTTOM (TAIL)

RECORDER 23C. ROCKET MOTOR CHANNEL 22

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	884	514	464	1027	3390	2030	8309.	1.00
2	884	514		1027	3390	2030	8309.	1.00
3	884	514		1027	3390	2030	8309.	1.00
4	884	514	464	1027	3390	2029	8308.	1.00
5	884	514	464		3390	2028	8307.	1.00
	884	514	464		3390	2025	8304.	1.00
7	884	514		1027	3390	2017	8295.	1.00
8	884	514		1027	3390	2005	8283.	1.00
9	884	514		1027	3390	1986	8264.	0,99
10	884	514 514		1027	3390	1951 1933	8229.	0,99
11	884 884	514		1027	339Ø 3389	1896	8211. 8173.	Ø.99 Ø.98
13	884	514		1027	3382	1846	8116.	0.98
14	884	514		1027	3375	1788	8051.	0,97
15	884	514		1027	3347	1706	7940.	0,96
16	884	514		1027	3330	1655	7872.	9.95
17	884	514		1027	3292	1579	7758.	0,93
18	884	514	461		3227	1498	7611.	
19	884	514	461	1027	3151	1415	7452.	0.90
20	884	512	461	1026	3054	1333	7270.	0,87
21	884	511	461		2995	1283	7159.	0,86
22	884	502	461		2801	1153	6812.	0.82
23	874	489	451	951	2521	1027	6313.	0.76
24	829	460	416	860	2245	920	5730.	0.69
25	731	405	352	766	1962	819	5035.	
26	691 600	376	322	727	1796	755 638	4667.	0.56
28	511	316 270	251	64Ø 547	1483 1234	548	3951. 3361.	Ø.48 Ø.40
29	450	243	217	420	1081	466	2877.	0.35
30	397	222	178	335	966	396	2494	0.30
31	380	209	164	291	914	379	2337.	0.28
32	345	189	137	239	829	337	2076.	0.25
33	319	180	119	196	720	292	1826.	Ø.22
34	289	165	108	161	614	240	1577.	0.19
35	257	152	91	141	525	201	1367.	Ø.16
36	246	142	86	135	477	183	1269.	0.15
37	213	120	78	112	409	146	1078.	
38	183	101	71	99	326	120	900.	
39	160	88	60	77	244	93	722.	0.09
40	130	66	41	59	179	63	538.	0.06
41	113	60	37	46	155	45	456.	0.05
42	87	42	26	32	112	21	320.	0.04
43	65 45	33	16	19	70	13 10	216.	0.03
45	28	21 13	6 3	7	38 15	4	64.	0.00
75	20	10	9	1	10		07.	0,00

(

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TABLE V2 (cont.)

### LAP. 5604 EXT. BOTTOM (TAIL)

		RECO	RDER	23C.	ROCKET MOT	OR CHANNE	L 22	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	20	11	2	Ø	9	2	44.	0.00
47	12	7	1	Ø	3	1	24.	0.00
48	8	4	Ø	Ø	Ø	1	13.	0.00
49	5	3	Ø	0	Ø	Ø	8.	0.00
50	3	2	Ø	Ø	Ø	Ø	5.	0.00
51	2	1	Ø	0	0	Ø	3.	0.00
52	2	1	Ø	Ø	Ø	Ø	3.	0.00
53	Ø	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

TABLE W2

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 PROP. SURFACE (NOSE)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C,PROB
1	1028			1027	3675	2030	9737.	1.00
2		1030		1027	3675	2030	9737.	1,00
3	1028	1030	947	1027	3675 3675	2029	9736.	1,00
5	1028	The same of the same of		1027	3675	2027	9734. 9728.	1.00
6	1028	1030	946		3675	2019	9725.	1,00
7	1028	1030	946		3675	2011	9717.	1,00
8		1030		1027	3675	1998	9704.	1.00
9		1030		1027	3675	1970	9676.	0.99
10		1030	946		3675	1934	9640.	0,99
11	1028			1027	3675	1915	9621.	0.99
12	1028			1027	3672	1870	9573.	0,98
13 14	1028	1030	946	1027	3663	1817 1757	9511. 9438.	0,98
15	1028			1027	3651 3631	1677	9338.	Ø.97 Ø.96
16	1028		945		3610	1641	9281.	0.95
17	1028		945		3561	1540	9131.	0.94
18	1028	The state of the s	944		3506	1457	8992.	0.92
19	1028	1029	944	1027	3432	1375	8835.	0.91
20	1028	1026	944	1026	3328	1275	8627.	Ø,89
21		1024	944	1020	3248	1235	8499.	Ø.87
22	1028	1017	944	998	3037	1114	8138.	0.84
23 24	1016	997 951	923 883	923 830	2714	984 879	7557.	Ø.78 Ø.71
25	850	893	831	748	2384 2083	769	6881, 6174,	Ø.63
26	804	855	783	709	1908	718	5777.	0.59
27	667	754	652	636	1570	618	4897.	0,50
28	574	624	519	536	1369	527	4149.	0.43
29	505	508	440	404	1204	458	3519.	0.36
30	447	450	371	317	1078	409	3072.	0.32
31	425	428	348	284	1028	384	2897.	0.30
32	396	394	303	238	931	331	2593.	0,27
33 34	361 323	358 329	267	199	818	293 256	2296.	0.24
35	289	303	235	168	718 615	212	2029.	Ø.21 Ø.18
36	283	287	190	132	567	190	1649.	0,17
37	242	262	171	108	477	159	1419.	0.15
38	214	237	152	94	392	125	1214.	0.12
39	187	204	128	75	299	103	996.	0.10
40	154	183	97	59	229	74	796.	0.08
41	138	161	90	48	197	61	695,	0.07
42	103	122	68	33	149	27	502.	0.05
43	8Ø 59	96	47	23	108	15	369. 242.	0.04
45	35	74 47	26 18	10	66 31	7	140.	Ø,02 Ø,01
-	05	7,	10	,	91	3	140.	0,01

TABLE W2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 PROP. SURFACE (NOSE)

		RECO	RDER	23C.	ROCKET MOT	OR CHANNE	L 23	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46 47	26 16	37 22	15	2	19	2	101.	0,01
48	8	12	7	Ø	3	i	31.	0,00
49	5	7	2	Ø	Ø	0	14.	0.00
5Ø 51	2 2	5	2	Ø	Ø Ø	Ø	10.	0.00 0.00
52	Ø	3	1	ø	Ø	Ø	4.	0.00
53	Ø	0	1	Ø	Ø	0	1.	0.00
54	Ø	Ø	Ø	Ø	Ø	Ø	Ø.	0.00

TABLE X2

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

LAP. 5604 INT. PROP. CHARGE (NOSE)

RECORDER 23C. ROCKET MOTOR CHANNEL 24

		-	-					
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1028	1031	947	1027	3676	2030	9739.	1.00
2	1028	1031	947	1027	3676	2030	9739.	1.00
3	1028	1031	947		3676	2030	9739.	1.00
4	1028	1031	947		3676	2028	9737.	1.00
5	1028	1031	947		3676	2024	9733.	1.00
6	1028		946		3676	2021	9729.	1.00
7	1028			1027	3676	2010	9718.	1.00
8	1028	1031	946	1027	3676	1995	9703.	
9	1028	1031	946		3676	1977	9685.	
10	1028	1031	946		3676	1941	9649.	0.99
11	1028	1031	946		3676	1925	9633.	0.99
12		1031	946		3673	1890	9595.	0.99
13	1028	1031	946	1027	3668	1843	9543.	0.98
14	1028	1031	945	1027	3659	1788	9478.	0.97
15	1028	1031	945	1027	3642	1706	9379.	0,96
16	1028	1031	945	1027	3627	1655	9313.	
17	1028	1031	945	1027	3580	1566	9177.	0.94
18	1028	1031	944	1027	3520	1482	9032.	0.93
19	1028	1030	944		3453	1408	8890,	0.91
20	1028	1028	944	1025	3350	1308	8683.	0.89
21	1028	1026	944	1022	3276	1246	8542.	
22	1028	1017	944	1008	3089	1119	8205.	0.84
23	1019	1001	933	944	2776	999	7672.	
24	964	965	900	850	2453	887	7019.	0.72
2.5	863	905	840	760	2119	777	6264.	
26	815	861	803	729	1959	720	5887.	0,60
27	680	764	647	639	1633	614	4977.	0.51
28	586	639	520	543	1387	523	4198.	0.43
29	507	521	442	421	1214	468	3573.	
30	456	459	378	333	1089	418	3133.	0.32
31	438	437	359	295	1034	393	2956.	0.30
32	396	398	319	252	943	347	2655.	0.27
33	364	367	280	200	845	308	2364.	0.24
34	333	335	241	167	737	261	2074.	
35	297	310	215	145	638	211	1816.	
36	285	298	196	138	587	196	1700.	0.17
37	254	272	168	109	498	154	1455.	0.15
38	221	244	150	96	418	126	1255.	0.13
39	192	213	135	78	315	106	1039.	0.11
40	160	186	103	64	240	76	829.	0.09
41	147	166	95	51	214	61	734.	0.08
42	105	130	64	36	160	33	528,	0.05
43	86	108	49	23	119	16	401.	0.04
44	63	80	29	13	72	11	268.	0.03
45	38	50	18	6	34	6	152,	0.02

TABLE X2 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS LAP. 5604 INT. PROP. CHARGE (NOSE)

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	30	40	15	3	24	4	116.	0.01
47	17	25	7	1	10	2	62.	0.00
48	9	16	7	1	4	Ø	37.	0.00
49	7	9		1	2	Ø	22.	0.00
50	3	8	3	ī	2 Ø	Ü	13.	0.00
51	2	7	Ø	1	0	Ø	10.	0.00
52	1	4	Ø	1	Ø	Ø	6.	0,00
53	ĩ	1	Ø	1	Ø	Ø	3,	0.00
54	Ø	1	Ø	1	Ø	Ø	2.	0.00
55	Ø	1	Ø	1	0	Ü	2.	0.00
56	Ø	1	Ø	ī	Ø	0	2.	0.00
57	Ø	1	Ø	1	0	Ø	2,	0.00
58	Ø	1	Ø	1	0	Ø	2.	0.00
59	Ø	1	0	1	0	0	2.	0.00
60	ø	1	Ø	ī	Ø	Ø	2,	0,00
61	Ø	. 1	0	1	Ø	Ľ	2.	0,00
62	Ø	1	Ø	1	Ø	6	2.	0.00
63	Ø	ī	Ø	ī	Ø	v	2.	0.00
64	ø	1	0	1	Ø	Ø	2.	0.00
65	Ø	1	Ø	1	0	Ü	2.	0.00
66	Ø	1	Ø	ī	Ø	Ø	2.	0.00
67	Ø	1	Ø	1	0	Ø	2.	0.00
68	Ø	1	Ø	1	Ø	0	2.	0.00
69	Ø	1	Ø	1	0	Ø	2.	0.00
70	Ø	1	Ø	1	Ø	Ø	2.	0.00
71	Ø	1	Ø	1	Ø	Ø	2.	0.00
72	Ø	0	Ø	1	Ø	Ø	1.	0.00
73	Ø	Ø	Ø	1	Ø	Ü	1.	0.00
74	Ø	0	Ø	ī	Ø	Ø	1.	0.00
75	Ø	0	Ø	1	Ø	Ø	1,	0.00
76	0	Ø	Ø	1	Ø	Ø	1.	0.00
77	Ø	0	Ø	ø	Ø	Ø	Ø.	0.00

TABLE A3

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SIDEWINDER CENTRE (BOXED)

		RECO	RDER	31A.	ROCKET NOT	TOR CHANN	IEL 1	
5-0	5.00		F. C.	V/ 4 D	AUT CODING	UNTER		a 6506
DEG.	DEC	JAI	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1019	1030	949	1.031	3697	2032	9758.	1.00
2	1019	1030		1931	3697	2932	9758.	1.00
3	1019	1030	949	1031	3697	2032	9758.	1.00
4	1019	1030	949	1031	3697	2032	9758.	1.00
5	1019	1030	949	1031	3597	2032	9758.	1.00
6		1030	949	1031	3697	2032	9758.	1.88
7	1019	1030	949	1031	3697	. 2029	9755.	1.02
8		1030	949	1831	3697	2025	9751.	1.00
9	1819		949	1031	3697	2619	9745.	
10	1019	1930	949	1031	3696	2007	9732.	1.00
11	1019	1030	949	1831	3696	2000	9725.	1.00
12	1019	1030	949	1031	3695	1984	9708.	0.99
13	1019	1030	949	1031	3692	1964	9685.	0.99
14	1219	1030	949	1931	3684	1923	9636.	0.99
15	1019	1039	949	1.031	3679	1869	9568.	9.98
16	1019	1.030	949	1931	3655	1826	9512.	0.97
1.7	1018	1030	949	1031	3618	1717	9353.	0.96
18	1018	1030	949	1829	3550	1557	9133.	0.94
19	1018	1029	949	1021	3442	1366	3825.	0.90
20	1013	1028	949	1012	3213	1158	8373.	0.96
21.	1026	1025	949	1302	3277	1084	8143.	0.83
22	975	1008	946	950	2669	946	7523.	0.77
23	900	965	376	825	2248	806	6620.	0.68
24	793	881	692	630	1933	704	5633.	9.58
25	700	741	566	494	1.702	603	4876.	0.49
26	658	689	517	448	1592	559	4463.	0.46
27	590	618	452	366	1428	487	3941.	0.43
28	535	555	401	322	1268	401	3482.	0.36
29	483	513	351	282	1124	324	3977.	0.32
30	439	471	300	248	1012	250	2720,	6.58
31	426	452	291	225	937	221	2558.	0.26
32	382	418	267	190		. 180	2260.	0.23
33	350	384	231	164	594	135	1958.	0.20
34	312	353	2012	131	604	113	1715.	0.18
35	280	323	177	96	511	72	1459.	0.15
36	266	308	165	85	467	58	1349.	0.14
37	227	278	137	63	380	4.5	1137.	0.12
38	196	253	122	36	327	23	957.	0.10
39	163	216	101	27	253	12	772.	Ø.08
40	140	183	84	16	191	7	621.	9.06
41	1.20	1.66	77	9	163	4	539.	8.06
42	. 88	138	. 58	3	111	1	399.	0.04
43	58	99	46	2	63	10	268.	0.03
44	43	72	31	5	4.0	Ø	198.	0.02
45	28	54	55	Ø	26	U	130.	0.01

TABLE A3 (cont.)

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SIDEWINDER CENTRE (BOXED)

		RECO	RDER	31A.	ROCKET NOT	TOR CHANNE	L 1	
DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	20	47	16	Ø	12	Ø	95.	0.00
47	10	38	1.0	0	4	Ø	62.	0.00
48	4	24	5	Ø	2	Ø	35.	0.00
49	1	13	1	Ø	2	Ø	17.	. 0.00
50	1	8	1	-6	2	W	12.	0.90
51	1	5	1	9	2	Ø	9.	0.00
52	1	2	1.	Ø	2	. ()	6.	6.00
53	1	1.	1	C	2	0	5.	0.00
54	1	1.	1.	. 0	2	IJ.	5.	0.20
55	· Ø	Ø:	Ø	Ø	2	Ø	2.	0.00
56	0	Ω	Ø	0	2	Ø	2.	0.30
57	Ø	.0	0	Ø	2	0	2.	0.00
58	9	(1	9	Çī.	2	Ø	2.	0,00
59	E	C	Ø	Ø	5	N	2,	9.00
60	S S	17	Ø	63	2	Ø	2.	0.00
61	2	Ω	Ø	Ø	2	Ø	2.	0.00
62	0	0	Ø	0	5	. 0	2.	0.20
63	Ø	0	Ø	g.	2	Ø	2.	0.00
64	0	Ø	N	(i	. 2	Ø	2.	0.20
65	Ø	0.	0	0		W	2.	0.00
66	Ø	Ø	Ø	Ø	5	Ø -	2.	0.00
67	C	C	N	0	. 2	Ø	2.	0.00
68	Ø	0	Ø		1.	0	1.	0.00
69	Ø	C	0	0	Ø	Ø	Ø.	0.00

TABLE 83

CUMULATIVE PROBABILITY DISTRIBUTION FOR HOCKET MOTOR TEMPS

SIDEWINDER MOTOR SKIN (BOXED)

		RECO	RDER	31A.	ROCKET HOT	OR CHANNI	EL 2	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
	1010	1070	0.40	1070	7/07	0070	0757	
1		1030		1032	3697	2032	9757.	1.00
2		1030		1030	3697	2032	9757.	
3		1030		1030	3697	2032	9757.	1.20
4		1030	949		3697	2032	9757.	1.00
5		1030		1232	3697	2032	9757.	1.00
6		1030		1330	3697	5835	9757.	
7		1/30		1032	3697	. 2029	9754.	
8		1 830		1339	3697	5052	9750.	
9		1030		1 432	3697	2019		1.03
10		1230		1933	3696	2906	9730.	1.00
11		1039	949	1333	3696	1995	9722.	1.00
12		1030		1337	3696	1981	9725.	0.99
13		1.330		1037	3693	1963	9684.	0.99
14		1030		1333	3682	1916	9626.	8.99
15		1030		1030	3667	1861	9556.	Ø.98
16		1030	949	1030	3654	1822	9524.	0.97
1.7		1037	949	1030	3615	1709	9351.	0.96
18	1018	1030	949	1228	3548	1546	9121.	0.93
19	1018	1/129	949	1821	3434	1350	8831.	0.93
5K	1112	1023	949	1211	3208	1161	8369.	0.86
21	1885	1025	949	1200	3059	1073	8111.	0.83
22	972	1009	947	957	2649	936	7472.	0.77
23	893	955	868	822	2235	802	6575.	0.67
24	775	862	692	634	1910	698	5571.	0.57
25	691	732	558	500	1685	599	4765.	0.49
26	656	676	518	440	1589	561	4440.	0.46
27	588	627	450	373	1410	485	3913.	0.40
28	531	553	397	314	1259	408	3462.	0.35
29	482	511	348	278	1140	322	3081.	0.32
30 .	437	464	305	248	1700	256	2710.	0.28
31.	420	444	294	227	942	228	2555.	0.26
32	384	413	263	192	821	. 183	2256.	0.23
33	354	382	232	163	702	139	1972.	7 0 7
34	316	347	213	141	606	111	1734.	0.18
35	285		179	103	524	82	1492.	0.15
36	261	306	167	86	476	69	1365.	9.14
37	233	277			396	42	1157.	0.12
38	197	251.		39	333	25	964.	0.10
39	169	221	104	33	267	14	828.	2.23
40	140	186	88	19	199	6	638.	0.07
41	123	173	80	11	1.76	5	568.	8.06
42	96	137	63	5	115	2	418.	0.34
43	60	104	49	2	69	้อ	284.	0.23
44	47	80	36	5	47	Ø	212.	80.02
45	29	60	27	1	30	W.	147.	0.02
				-				

TABLE 83 (cont.)

# CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SIDEWINDER MOTOR SKIN (BOXED)

		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	L 2	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	27	51	22	1	22	10	123,	0.01
47	13	41	11	. 8	6	3	71.	0.00
48	8	26	5	(3	1	Ø	40.	3.22
49	1	15	3	9	1	15	. 20.	0.23
50	1	9	1	0	1	. 0	12.	0.00
51	Ø	7	1	0	1	IJ	9.	0.00
52	Ø	3	1	9	1	10	5.	0.00
53	0	2	1	2	1	٥	4.	0.00
54	2	0	1	g	1	Ø	2.	0.20
55	Ø	C	1.	. Ø	1.	J	2.	0.00
56	Ø	Ø	1	21	1.	Ø	2.	0.00
57	Ø	0	1.	Ø	1	Ø	2.	0.00
58	C	0	1	Ø	1	0	2.	0.00
59	Ø	Ø	1	3	1	13	2.	0.00
60	Ø	Ø	1.	2	1	Ø	2.	0.00
61	8	0	1.	0	1	IJ	2.	0.00
62	Ø	0	1	0	1	U	2.	0.00
63	0	U	1	3	1	3	2.	0.00
64	Ø	6	1	0	1	υ	2.	0.00
65	Ø	61	1	9	1	. 0	2.	0.02
66	Ø	Fi	1	0	1	U	2.	0.00
67	Ø	- 13	1	2	1	Ø .	2.	0.00
68	Ø	D	1	0	1	٥	2.	0.00
69	2	Ø	1	3	1	_ Ø .	2.	0.00
70	Ø	C	1.	Ø	1	5	2.	0.00
71	Ø	C	1	0	1	10	2.	0.00
.72	Ø	Ø	1	Ø	-1	Ŋ	2.	0.00
73	Ø	CI	Ø	Ø	1	60	1.	0.00
74	O	0	0	7/.	a	Ø	Ø.	0.00

TABLE C3
CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

#### SIDEWINDER HALFWAY BET. SKIN AND BOX

		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	£L 3	
DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	MINIER	TOTAL	C.PROB
1	1019	1030	948	1030	3597	2032	9756.	1.00
2	1019		948		3697	2032	9756.	1.00
3		1030		1030	3697	2032	9756.	1.50
4		1030		1030	3697	2232	9756.	1.02
5		1230	948	1030	3697	2032	9756.	1.00
6		1030	948		3697	2030	9754.	1.00
7		1030		1030	3597	2025	9749.	1.20
8		1/30		1039	3697	5050	9744.	1.00
9		1030		1030	3697	2012	9736.	1.00
10		1030	948	1330	3697	1993	9717.	1.00
11		1030	948	1030	3697	1981	9785.	0.99
12		1039	948	1030	3695	1958	9680.	0.99
13		1030		1230	3688	1922	9637.	0.99
14		1030		1230	3576	1871	9574.	0.98
15	1019		948	1037	3638	1805	9470.	0,97
16	1018	1030	948	1030	3623	1742	9391.	9.96
17	1018	1030	948	1229	3563	1621	9289.	2.94
18		1729	948	1321	3464	1446	5926,	0.91
19	1017	1025	948	1312	3302	1246	8551.	0.88
20	1000	1021.	948	996	3846	1050	8061.	2.83
21	988	1012	947	982	2866	989	7784.	0.80
22	927	980	935	914	2421	853	7010.	0.72
23	830	913	319	768	2007	747	6084.	0.62
24	793	794	616	562	1735	672	5067.	0.52
25	628	656	504	446	1547	604	4385.	0.45
26	588	608	465	407	1461	575	4184,	0.42
27	537	549	410	351	1322	529	3698.	0.38
28	495	494	361	303	1206	455	3314.	0.34
29	453	465	316	269	1110	398	3011.	0.31
30	413	432	294	236	1027	349	2751.	0.28
31	396	415	282	222	982	325	2620.	0.27
32	371	391	260	209	391	292	2414.	0.25
33	344	368	224	185	806	245	2170.	0.22
34	314	344	213	166	731	199	1967.	0.20
35	295	326	197	141	647	165	1771.	0.18
36	283	310	186	130	608	150	1667.	0.17
37	262	293	168	117	543	1.24	1500.	0.15
38	244	273	154	84	486	94	1335.	0.14
39	212	249	143	67	414	74	1159.	0.12
46	193	229	124	58	357	49	1010.	0.10
41	180	223	114	57	335	43	952.	0.10
42	149	204	101	45	285	33	817.	0.08
43	122	187	94	31	227	23	684.	0.07
44	101	155	83	26	181	1.7	563.	0.06
45	86	132	74	19	150	9	470.	0.25

TABLE C3 (cont.)

#### SIDEWINDER HALFWAY BET. SKIN AND BOX

		RECO	RDER	314.	ROCKET MOT	OR CHANNE	EL 3	
DEG.	DEC	MAL	FEB	MAR	AUT-SPRING	WINTER	TOTAL	c.PRoa
46	76	124	72	16	134	7	429.	0.94
47	62	107	58	1.3	97	3	340.	0.03
48	51	87	48	1.5	76 .	5	274.	0.33
49	35	71	38	7	50	1	202.	0.02
50	29	57	27	4	33	1	151.	0.02
51	26	52	24	2	23	U	127.	0.01
52	22	42	1.8	2	14	Ø	96.	0.00
53	1.3	34	14	1	9	Ø	71.	0.20
54	5	25	10	1	6	10	47.	0.09
55	4	16	5	0	3	2	28.	0.00
56	3	13	3	Ø	5	i)	21.	0.08
57	2	7	2	73	2	Ø	13.	2.00
58	1	4	1	0	2	Ø.	8.	0.03
59	1	1	Ø	O	2 .	63	4.	0.00
60	Ø	1	0	0	2	W .	3.	0.00
61	Ø	1	Ø	0	2	0	3.	7.20
62	Z	1	9	Ø	2	Ø	3.	0.23
63	2	0	Ø	0	2	Ø	2.	Ø.00
64	Ø	0	7	9	2	Ø	2.	0.00
65	2	0	Ø	9	2	Ø	2.	0.00
66	Ø Ø	Ø	0	2	2	Ø	2.	2.02
67	2	Ø	Ø	3	2	Ø	2.	0.00
68	2	Ø	Ø	03	2	Ю	2.	0.30
69	Z	0	Ø	3	1	Ø .	1.	0.00
78	0	0	Ø	Ø	1	Δ	1.	0.20
71	Ø	O	Ø	2	1	W	1,	0.00
72	Ø	Ø	a	2	1	VI	1.	2.02
73	0	Ø	9.	2	1	Ø	1.	0.00
74	Ø	Ø	Ø	2	1	9	1.	0.00
75	2	Ø	Ø	Ø	1	Ø	1.	2.22
76	Ø	0	0	7	1	10	1.	0.00
77	2	Ø	Ø	2	1	Ø	1.	0.00
78	2	0	Ø	0	3	1)	0.	0.20

TABLE D3

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

SIDEWINDER OUTER CASE

				DIDL	MINDER OUTER OF			
		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	EL 4	
DEG.	DEC.	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1018	1931	949	1032	3596	2032	9756.	1.02
2	1018	1031	949	1939	3596	2032	9755.	1.00
3		1031		1037	3496	2032	9756.	1.00
4		1.031		1032	3596	2030	9754.	1.00
5		1031		1033	3696	2025	9749.	1.00
6	1018			1333	3696	2024	9748.	1.00
7		1031		1032	3596	2329	9744.	1.00
8		1.031		1030	3696	2009	9733.	1.60
9		1331		1030	3696	1985	9727.	0.99
10	1.718			1332	3594	1962	9684.	0.99
		1331		1037	3693	1949	9678.	2.99
	1018			1030	3585	1916	9630.	0.99
13	1.018			1333	3669	1865	9565.	0,98
14		1.331		1030	3436	1790	9454.	0.97
15		1031		1030	3596	1693	9321.	0.96
16	1017	1031	949	1029	3562	1635	9223.	0.95
17	1017	1229	949	1024	3458	1495	8970.	9.92
18	1015	1023	949	1313	3322	1303	5632.	0.88
19	1003	1020	949	999	3109	1104	8184.	0.84
29	978	1203	947	971	2796	945	7642.	0.78
21	945	988	944	939	2593	893	7310.	0.75
22	367	927	903	865	2138	739	6489,	0.67
23	729	820	732	772	1785	724	5492.	0.56
24	635	711	539	516	1580	674	4655.	0.48
25	562	574	457	414	1448	643	4091.	0.42
26	534	546	406	380	1391	621	3878.	0.40
27	494		375	334	1296	5.78	3564	0.37
28	455	452	345	298	1215	539	3304.	0,34
29	424	424	318	271	1136	498	3071.	0.31
30	431	402	291	248	1/81	458	2881.	0.30
31	392	394	285	242	1052	445	2810.	9.29
32	374	376	259	227	989	41.2	2637.	9.27
33	353	363	238	216	928	374	2472.	0.25
34	338	350	223	207	875	348	2341.	0.24
35	324	338	217	194	<sup>9</sup> 27	317	2217.	0.23
36	317	334	21,5	187	802	307	2162.	9.22
37	300	321	204	173	755	281	2034.	8.21
38	291	310	196	163	707	247	1911.	0.23
39	271	300	185	140	665	225	1786.	₹,18
40	256	286	169	126	621.	197	1655.	0.17
	251	280	164	120	599	183	1597.	0.16
42	238	267	151	108	558	155	1477.	0.15
44	225	256	145	93	514	129	1362.	0.14
45	212 198	235	125	85 72	463	93	1251. 1139.	0.13
10	170	600	162	11	410	70	1.107	1.076

TABLE D3 CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS SIDEWINDER OUTER CASE

				SIDE	VINDER OUTER CA	DE .		
		RECO	RDER	31A.	ROCKET MOT	L 4		
DEG.	DEC.	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	193	226	121	63	394	88	1099.	0.11
47	175	213	113	55	352	70	979.	0.10
48	158	5 9 0	107	45	317	55	882.	0.09
49	139	184	94	41	275	41.	774.	3.23
50	120	167	87	33	243	30	683.	0.07
51	114	159	83	29	218	33	636.	0.27
52	95	144	8.1	26	176	22	543.	0.06
53	82	135	70	5.5	158	Sn	487.	0.05
54	65	:116	63	18	122	14	398.	0.04
55	. 59	101	53	15	102	7	337.	0.03
56	54	95	49	15	93	5	311.	0.03
57	44	86	45	13	74	2	258.	0.03
58 -	. 34	69	36	13	55	5	229.	0.02
59	26	55	29	10	37	2	159.	0.02
60	17	45	22	9	24	1	118.	0.01
61	15	41	21	7	23 ·	1	106,	0.01
62	10	32	16	6	15	Ø	79.	0.00
63	5	27	14	4	8	V.	58.	0.00
64	2	21	11	3	5	Ŋ	42.	3.02
65	1	12	11	. 2	2	(2)	28.	0.00
66	1	10	3	2	1	U	22.	0.00
67	1	8	2	1	Ø	2	12.	0.00
68	1	6	2	1	Ø	. 0	10.	0.00
69	2	4	1.	1	Ø	. <i>v</i>	6.	0.00
70	2	3	9	1	Ø	W	4.	0.00
71	Ø	3	Ø	1	Ø	J	4.	0.00
72	2.	2	Ø	1	. 0	19	3,	0.00
73	0	Ø	Ø	1.	Ø	. 0	1.	0.00
74	Ø	C	Ø	1	Ø	6	1.	0.00
75	Ø	Ø	Ø	1	Ø	Ø	1.	2.00
76	0	a	Ø	1	Ø	Ŋ	1.	0.00
77	Ø	0	9	Ø	Ø	Ø	ø.	0.00

TABLE E3

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

ASROC INTERIOR (UNBOXED)

TABLE E3 (cont.).

## CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS ASROC INTERIOR (UNBOXED)

		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	L 5	
DEG.	DEC	JAII	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	1	17	1	1	3	W	23.	Ø.00
47	Ø	10	0	1	3 3	Ø	14.	2.00
48	0	6	Ø	1	3	i)	1.0.	0.00
49	Ø	Ø	0	1	2	Ø	3.	0.00
50	Ø	0	Ø	1	2	Ø	3.	0.00
51	Ø	0	Ø	. 1	2	Ø	3.	0.00
52	Ø	O	Ø	1	2	. 60	3.	0.00
53	2	Ø	Ø	1	2	Ø	3.	0.00
54	Ø	Ø.	Ø	1	2	W	3.	2.33
55	.0	Ø	Ø	1	2	Ø	3.	0.00
56	3	Ø	0	1	2	Ø	3.	0.00
57	2	Ø	0	1.	2	O	3.	6.32
58	Ø	Ø	9	1.	5	Ø	3.	0.00
59	Ø		2	1	2	v	3.	0.20
69	2	0	7	1	2	Ø	3.	0.00
61	Ø	Ø	Ø	1	2	Ø	3.	0.00
62	3	Ø	Ø	Ø	2	Ø	2.	0.00
63	3	Ø	Ø	Ø	2	Ю	2.	0.00
64	3	Ø.	Ø	3	2	N	2.	0.00
65	2	0	Ø	Ø	1	. W	1.	0.00
66	2	0	0	2	1	Ø.	1.	0.00
67	2	Ø	Ø	Ø	1	. 0	1.	0.09
68	Ø	0	0	Ø	1	И	1.	0.00
69	9	J	0	0	1	Ø	1.	0.00
70	Ø	Ø	Ø	Ø	1	Ø	1.	0.00
71	Ø	. 0	Ø	Ø	1	U.	1.	0.00
72	Ø	Ø	Ø	Ø	1	Ø	1.	0.20
73	0	U	Ø	Ø	1	Ø	1.	0.00
74	· Ø	Ø	Ø	0	1	Ø	1.	0.00
75	Ø	Ø	Ø	Ø	0	Ø	. Ø.	0.00

TABLE F3 .

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

ASROC MOTOR SKIN (UNBOXED)

		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	EL 6	
DEG.	OEC	MAL	FEB	MAR	AUT-SPRING	UINTER	TOTAL	c.PRoB
1	1018	1031	948	1031	3696	2031	9755.	1.99
2		1031	948	1031	3696	2031	9755.	1.00
3	1013	1.031	948	1231	3696	2031	9755.	1.05
4	1018	1231	943	1031	3696	2029	9753.	1.30
5	1018	1231	948	1231	3696	2025	9749.	1.00
6	1018	1031	948	1031	3696	2025	9746.	1.00
7	1018	1231	948	1031	3696	-2018	9742.	1.00
3	1013	1231	948	1231	3696	2029	9733.	1,00
9	1018	1031	948	1231	3696	1992	9716.	1.00
10	1013	1031	948	1731	3696	1972	9696.	0.99
11	1018	1//31	948	1031	3694	1961	9683.	0.99
12	the transfer of the	1031	948	1231	3688	1931	9647.	0.99
13		1031	948	1031	3675	1892	9595.	9.98
14		1031	948	1031	3654	1830	9512.	Ø.98 Ø.96
15 16	1015	1231	948	1031	3612 3590	1742 1691	9382. 9388.	0.95
17	1017		948	1037	3519	1566	9110.	0.93
18		1030	948	1218	3394	1394	8831.	0.90
19	1009		948	1209	3225	1212	8430.	2.86
20	993	1314	948	992	2951 -	1035	7933.	0.81
21	976	1006	945	964	2773	979	7643.	0.78
22	915	965	917	901	2343	868	5989.	0.71
23	798	883	730	746	1984	791	5982.	0.61
24	691	731	605	553	1751	738	5119.	0.52
25	61.6	669	506	461	1603	703	4558.	0.47
26	536	617	470	427	1541	683	4324.	0.44
27	533	556	416	379	1450	659	3998.	0.41
28	525	509	388	339	1368	631	3740.	0.38
29	471	470	364	311	1308	598	3522.	0.36
30	448	445	335	297	1240	559	3324.	0.34
31	435	433	324	289	1215	547	3242.	0.33
32	416	410	305	268	1159	. 508	3066.	0.31
33	309	399	294	251	1119	476	2940.	0.30
34	386	383	277	237	1268	441	2792.	0.29
35	371	373	266	556	1716	412	2664. 2588.	0.27
36	364	363	258	219	981	493		0.27
37 38	348 328	353	244	210	926	375 337	2456.	0.25 0.24
39	316	329	223	185	867 8 <b>3</b> 5	312	2200.	0.23
40	308	321	209	174	809	279	2126.	0.22
41	324	319	203	168	781	270	2045.	0.21
42	296	313	194	158	731	236	1928.	0.23
43	282	599	182	144	677	21.0	1794.	Ø.18
44	267	294	169	133	638	179	1677.	0.17
45	254	287	163	116	597	15/	1574.	0.16

TABLE F3 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

ASROC MOTOR SKIN (UNBOXED)

DEG.	DEC	NAU	FEB	MAR	AUT-SPRING	WINTER	TOTAL	, C.PROB
46	245	281	169	113	568	142	1509.	0.15
47	231	273	1.47	101	518	12/	1397.	0.14
48	221	261	136	89	473	110	1290.	0.13
49	204	243	132	82	441	96	1198.	0.12
50	193	229	1.26	74	413	83	1118.	0.11
51	186	224	124	71	395	74	1074.	0.11
52	166	209	113	55	358	59	960.	0.10
53	151	200	103	48	322	52	876.	0.09
54	137	191	92	42	283	37	779.	2.28
55	126	181	80	32	245	31	695.	0.97
56	123	175	77	27	229	28	656.	2.37
57	135	159	70	24	203	21	582.	3,26
58	95	145	6.3	23	163	14	497.	0.05
59	74	132	54	16	129	1	412.	0.04
60	62	117	50	14	105	3	351.	0.04
61	59	109	46	11	97 .	2	324.	0.03
62	45	92	42	9	64	2 1 1	253.	0.03
63	35	78	38	6	44	1	202.	0.02
64	25	62	29	5	26	1	148.	0.02
65	17	54	22	4	12	Ø	107.	0.01
66	14	51	17	3	8	Ø	93.	9.00
67	8	38	1.4	3	3	10	66.	0.00
68	5 2	23	8	3	Ø	Ŋ	44.	3.00
69	2	25	5	2	Ø	Ŋ	34.	0.00
70	1	13	4	1	Ø	Ø	19.	0.00
71	1	11	3	1.	0	И	16.	0.00
.72	1	4	3 -	1	Ø	U	9.	0.00
73	1	2	2	1	Ø	0	6.	0.00
74	Ø	Ø	2	1	Ø	W	3.	0.00
75	Ø	Ø	Ø	1	Ø	Ø	1.	0.00
76	Ø	0	Ø	1	Ø	. 0	. 1.	0.00
77	D	Ø	Ø	Ø	9	Ø	0.	0.00

TABLE G3

### FFAR INTERIOR (BOXED)

				LIMI	THIDRIDGE (DOM	10,		
		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	IL. 7	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1018	1030	949	1030	3695	2031	9753.	1.00
2	1018	1030	949	1330	3695	2031	9753.	1.00
3		1030		1333	3695	2031	9753.	1.00
4		1030		1930	3695	2231	9753.	1.00
5		1030		1030	3695	2031	9753.	1.00
6		1030		1030	3695	2031	9753.	1.00
7		1030		1330	3695	2025	9747.	1.00
8		1430		1030	3695	-2021	9743.	1.00
9		1030		1030	3695	2014	9735.	1.00
10		1030		1030	3695	1996	9718.	1.00
11		1.030		1337	3695	1986	9788.	1.00
12		1030		1030	3695	1969	9691.	0.99
13		1030		1030	3686	1938	9651.	0.99
14		1030		1030	3672	1891	9598.	0.98
15		1030		1030	3652	1822	9591.	0.97
10		1030		1030	3635	1775	9438.	0.97
17		1030	949		3581	1648	9255.	0.95
18		1030		1024	3496	1449	3965.	0.92
19		1029		1015	3345	1256	3610.	0.88
20		1024	949	1003	3274	1071	3126.	0.83
21	997	1019	949	983	2901	1997	7856.	0.81
55	938	992	941	912	2434	874	7391.	0.73
23	843	922	812	748	2365	778	6165.	9.63
24	726	802	614	558	1787	686	5173.	0.53
25	652	673	515	441	1604	612	4497.	0.46
26	61.9	629	476	407	1520	563	4214.	0.43
27	550	575	423	341	1372	501	3772.	0.39
28	513	528	361	319	1248	427	3412.	0.35
29	471	489	335	272	1132	363	3062.	0.31
30	426	459	306	243	1719	301	2754.	0.28
31	415	439	289	227	952	266	2588.	0.27
32	387	407	257	191	851	215	2329.	0.24
33	353	375	235	163	748	. 163	2037.	0.21
34	323	344	209	137	659	133	1805.	0.19
35	297	322	187	118		104	1579.	0.16
36	287	312	176	100	551	90	1483.	0.15
					518			
37	254	289	148	69	452	64	1276.	0.13
38	213	265	125	53	378	40	1074.	0.11
39	185		108	38	309	25 11	970. 733.	0.09
40	150	210	91	21	250	1.9		
41	136	189	81	17	226	4	558.	0.07
42	116	157	73	8	156		511.	0.05
43	93	133	52	5	105	1	363.	
44	57	97	36	1.	57	Ø	248.	0.03
45.	34	68	28	1	35	Ø	166.	0.05

TABLE G3 (cont.)

### FFAR INTERIOR (BOXED)

		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	L 7	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	27	59	19	Ø	24	U	129.	0.01
47	11	41	11	Ø:	11	IJ	74.	0.00
48	6	32	5	Ø	4	Ð	.47.	9.03
49	Ø	19	1	Ø	1	i)	21.	0.00
50	Ø	8	3	Ø	1	W	9.	0.00
51	3	6	B	Ø	1	v	7.	0.00
52	Ø	3	Ø	24	1	Ø	4.	0.00
53	3	1	Ø	n	1	W	2.	0.00
54	7	C	Ø	Ø	1	Ø	1.	0.00
55	9	U	Ø	Ø	1	Ø	1.	0.30
56	Ø	0	3	2	1	Ю	1.	0.00
57	2	0	Ö	0	1.	12	1.	0.00
58	3	C	Ø	Ç)	1	И	1.	0.00
59	. 3	Ø	Ø	Ø	1	b)	1.	0.00
62	Ø	C	3	3	1.	Ø	i.	0.00
61	3	Ø	Ø	0	1.	i i	1.	0.00
62	Ø	O	Ø	Ø	1	10	1.	0.00
63	Ø	0	2	Ø	1	(i)	1.	0.00
64	3	Ø	Ø	Ø	1	()	1.	0.00
65	Ø	D	Ø	a	1	W	1.	0.00
66	Ø	0	Ø	Ø	1	Ø	1.	0.00
67	Ø	Ø	Ø	Ø	1	Ø	1.	0.00
86	3	0	Ø	Ø	1	_ U .	1.	0.00
69	3	0	Ø	a	1	10	1.	0.00
70	Ø	D	Ð	Ø	1	1)	1.	0.00
71	3	0.	Ø	Ø	1	0	1.	0.00
72	Ø	C	D.	D	Ø	i)	J.	0.00

TABLE H3
CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET NOTOR TEMPS
FFAR MOTOR SKIN (BOXED)

TABLE H3 (cont.)

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

### FFAR MOTOR SKIN (BOXED)

		RECO	RDER	31A.	ROCKET NOT	OR CHANNE	L 8	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	c.PROB
46	33	70	26	1	32	Ø	162.	0.02
47	23	49	13	N	18	Ø	103.	0.01
48	8	34	9	0	6	Ŋ	57.	0.03
49	3	30	3	Ø	3	IJ	39,	0.00
50	3	15	1	0	3	U	19.	0.00
51	Ø	9	1	Ø	3	Ø	13.	0.00
52	0	4	1.	Ø	3	. 0	8.	2.00
53	0	3	Ø	Ø	3	W	6,	0.00
54	Ø	2	D	Ø	3	(i)	5.	0.00
55	.0	0	Ø	Ø	3	И	3.	0.00
56	0	0	2	Ø	3	Ø	3.	0.00
57	Ø	0	Ø	Ø	3	Ø	3.	3.00
58	Ø	O	Ø	Ø	3	ω	3,	0.99
59	Ø	Ø	Ø	Ø	3	o o	3.	0.00
60	Ø	0	۵	Ø	3	U	3.	0.00
61	Ø	Ø	O	9	3	Ø	3.	0.00
62	Ø	0	3	Ø	3	i i	3.	3.00
63	Ø	Ø	Ø	Ø	3	ø	3.	0.00
64	7	Ø	0	3	3	U	3.	0.00
65	Ø	6.	0	U	3	N	3.	9.93
66	Ø	N	Ø	Ø	3	Ø	3.	0.00
67	Ø	C	Ø	Ø	3	Ø	3.	0.03
68	0	Ø	Ø	O	2	v	2.	0.00
69	Ø	0	0	3	2	0	2.	0.02
70	Ø	Ø	Ø.	Ø	2	Ø	2.	0,90
71	Ø	C	Ø	Ø	2	Ŋ	2.	Ø.00
72	0	0	Ø	2	2	W	2.	0.00
73	Ø	0	Ø	Ø	2	10	2.	0.00
74	Ø	0	Ø	Ø	2	Ø	2.	0.33
75	Ø	0	0	0	2	V	2.	0.00
76	Ø	0	Ø	g	2	9	2.	0.00
77	Ø	Ø	0	0	2	. 0	2.	0.00
78	Ø	Ø	Ø	2	1	8	1.	0.00.
79	Ø	Ø	Ø	Ø	0	Ø	ø.	0.00

TABLE J3

CUMULATIVE PROBABILITY DISTRIBUTION FOR ROCKET MOTOR TEMPS

FFAR OUTER CASE (BOXED)

		RECO	RDER	31A. ROCKET MOTOR CHANNEL 9				
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1019	1731	947	1231	3692	2031	9751.	1.00
2		1031		1031	3692	2031	9751.	1.00
3		1031		1231	3692	2031	9751.	1.00
4		1231	947		3692	2031	9751.	1.00
5		1231		1231	3692	2021	9747.	1.00
6		1031		1231	3692	2024	9744.	1.00
7		1031		1331	3692	2021	9741.	1.00
8		1231		1231	3592	2014	9734.	
9		1031		1031	3692	2000	9720.	1.00
10	1019			1231	3692	1981	9700.	0.99
11		1831		1231	3691	1972	9691.	0.99
12	1019	1031		1031	3685	1944	9657.	0.99
13	1019	1031		1031	3675	1905	9638.	0.99
	1019			1231	3655	1834	9517.	0.98
15		1031		1031	3616	1755	9399.	0.96
16	1018			1031	3597	1695	9319.	0.96
17		1030		1037	3522	1545	9092.	0.93
18		1032		1717	3391	1332	8735.	0.90
19	1012			1206	3189	1135	0316.	
20	991			983	2962	978	7777.	
21	969			955	2566	923	7454.	2.77
22	894	944	912	866	2177	817	6619.	0.68
23	766	851	731	671	1837	745	5671.	0.57
24	651	727	532	497	1626	688	4721.	0.48
25	587	599	444	402	1487	629	4141.	0.42
26	551	565	415	374	1428	604	3937.	9.40
27	504	514	373	326	1326	559	3602.	0.37
28	471	473	343	297	1239	502	3325.	0.34
29	439	448	315	270	1155	462	3089.	0.32
30	411	420	290	254	1383	41.5	2861.	0.39
31	391	407	283	245	1049	398	2773.	0.28
32	368	387	272	223	980	348	2578.	0.26
33	354	374	257	208	907	315	2415.	0.25
34	341	348	240	190	823	278	2220.	0.23
35	316	334	215	166	758	23>	2027.	0.21
36	327	323	206	150	722	215	1923.	0.20
37		312		132	661	178	1772.	0.18
38	273	293	185	117	610	153	1631.	0.17
39	254	277	172	96	541	122	1462.	0.15
40	237	266	151	86	488	93	1321.	0.14
41	224	260	141	75	452	82	1234.	0.13
42	198	241	126	62	396	61	1084.	0.11
43	179	226	108	55	333	49	953.	0.10
44	164	201	97	41	276	31	810.	0.08
45	138	1.82	86	33	229	20	688.	0.07

TABLE J3 (cont.)

#### FFAR OUTER CASE (BOXED)

		RECO	RDER	31A.	ROCKET MOT	TOR CHANNE	EL 9 .	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	126	175	82	27	206	15	631.	0.06
47	117	160	68	55	156	9	525.	0.05
48	86	129	54	16	1.17	4	406.	0.04
49	63	108	46	14	78	3	317.	0.03
50	46	85	38	5	48	Ø	255.	3.02
51	39	75	34	4	37	U	189.	0.92
52	27	59	19	5	22	. 0	129.	0.01
53	16	45	10	2	8	Ø	81.	0.00
54	9	33	7	1	2	0	52.	0.00
55	. 5	5.5	4	1	1	Ø	33.	0.30
56	3	18	3	1	9	N	25.	0.00
57	2	7	1	1.	ð	Ø	11.	0.30
58	1	3	1	1	0	Ø	6.	0.00
59	1	2 2 2	1	1	Ø	Ю	5,	0.00
62	2	5	1	1	Ø	10	4.	0.00
61	0	2	1.	1	ก	0	4.	0.00
62	Ø	1	1	1	0	Ø	3.	9.00
63	Ø	1.	1	1	Ø	N.	3.	0.33
64	2	1	1	1	. Ø	Ŋ	3.	0.00
65	0	1	1	1	Ö	W .	3.	0.00
66	2 2 2 2	1.	1	1	Ø	Ø	3.	0.00
67	Ø	1	1	1	0	Ŋ	3.	0.00
68	Ø	1	1	1	9	10	3.	0.30
69	2	1	1	1	ð	Ø	3.	0.00
70	3	1	Ø	1	Ø	Ø	2.	0.00
71	2 2 2	1	2	1	Ø	VI.	2.	0.00
72	0	27	Ø	1	Ø	· 10	1.	0.00
73	2	Ø	)	1	Ø	Ø	1.	0.00
74	2	0	Ø	1	Ø	Ø	1.	0.00
75	Ø	Ø	Ø	1	Ø	U	1.	0.00
76	0	C	0	1	Ø	Ø	1.	0.00
77	Ø	Ø	0	7	Ø	. 0	Ø.	0.00

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TABLE K3

CUMULATIVE PROBABILITY DISTRIBUTION FOR KOCKET MOTOR TEMPS

ZUNI MOTOR SKIN

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
,1	1019	1029	949	1031	3596	2731	9755.	1.23
2		1829		1831	3696	2031	9755.	1.00
3	1019	1029	949		3696	2031	9755.	1.00
4	1019	1929	949	1031	3696	2031	9755.	1.00
5		1229	949		3696	2031	9755.	1.00
	1019		949	1331		2031	9755.	
6		1029		1031	3696	2024		1,00
		1029	949	1231	3696		9748.	1.00
8		1729		1231	3696	-2015	9742.	1.00
9		1029	949	1231	3696	2010	9734.	1.00
12		1729	949	1231	3696	1989	9713.	1.00
11		1/29	949	1.031	3696	1977	9721.	0.99
12		1029	949	1031	3695	1959	9682.	0.99
13		1729	949	1231	3585	1924	9637.	0.99
14		1829	949	1231	3667	1870	9565.	3.98
15	1019	1029	949	1231	3644	1801	9473.	2.97
16	1019	1/29	949	1031	3622	1743	9391.	0.96
17	1218	1029	949	1030	3557	1615	9198.	0.94
18	1018	1028	949	1022	3445	1397	3859.	0.91
19		1027	949	1.013	3284	1200	8495.	0.87
20	1001	1019	949	997	3000	1040	8006.	0.82
21		1009	948	973	2305	987	7728.	0.79
22	921	976	935	894	2322	870	6918.	0.71
23	835	887	773	731	1975	787	5953.	0.61
24	686	770	568	528	1748	720	5020.	0.51
25	617	638	477	443	1608	663	4451.	0.46
26	586	597	448	399	1542	635	4210.	0.43
27	539	542	409	362	1418	580	3850.	8.39
58	531	505	373	318	1314	534	3545.	0.36
59	457	471	339	291	1212	476	3256.	Ø.33
30	444	441	313	264	1131	426	3019.	0.31
31	437	433	305	256	1386	400	2910.	0.30
32	395	417	533	227	1018	352	2689.	0.28
33	371	338	258	505	936	. 288	2443.	0.25
34	355	369	231	187	863	238	2243.	0.23 .
35	333	348	223	162	786	223	2052.	0.21
36	328	340	213	154	746	182	1963.	0.20
37	325	324	193	132	562	146	1764.	0.18
38	285	337	174	110	596	122	1594.	3,16
39	263	292	157	85	526	96	1419.	0.15
40	241	275	143	63	449	70	1238.	0.13
41	223	260	131	56	417	56	1148.	0.12
42	197	243	115	41	353	41	990.	0.10
43	168	226	99	33	312	25	863.	0.09
44	145	201	87	18	255	17	723.	0.07
45.	1.25	1.75	72	11	205	6	594.	0.06

TABLE K3 (cont.)

### ZUNI MOTOR SKIN

RECORDER 31A. R	OCKET M	OTOR I	CHANN	EL :	10
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DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	109	161	66	8	176	4	524.	0.05
47	33	137	59	3	122	1	425.	0.04
48	69	109	47	1	81	Ø	327.	0.03
49	43	84	33	1	51	ø	214.	0.02
50	28	60	19	1	33	Ø	141.	0.01
51	25	53	15	1	27	Ø	121.	0.21
52	7	36	8	Ø	8	W	59.	0.00
53	3	24	4	9	2	Ø	33.	0.00
54	2	17	1	Ø	2	Ø	22,	0.00
55	5	5 3	Ø	2	2	Ø	7.	0.20
56	2		Ø	0	2	Ø	5.	0.00
57	7	2	Ø	Ø	2	ð	4.	0.00
58	9	Ø	3	Ø	2	٥	2.	0.00
59	. 0	Ø	Ø	Ø	5 .	Ø	2.	0.90
60	Ø	Ø	Ø	Ø	2	Ø	2.	0.00
61	0	Ø	Ø	3	2	Ŋ	2.	0.00
62	3	Ø	3	Ø	2	i)	2.	0.00
63	2	Ø	Ø	0	2	N N	2.	0.00
64	3	Ø	Ø	Ø	2	Ø	2.	0.00
65	Ø	()	Ø	93	2	Ø	2.	0.00
66 .	Ø	Ø	2	0	2.	Ю	2.	0.00
67	Ø	Ø	Ø	Ø	2	v	2.	0.00
68	0	Ø	2	Ø	2	W .	2.	0.00
69	Ø	Ø	7	Ø	2	9	2.	0.00
70	3	Ø	Ø	Ø	9	i)	Ø.	0.00

TABLE L3
CUMULATIVE PROBABILITY DISTRIBUTION FOR HOCKET MOTOR TEMPS
ZUNI INTERIOR

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1	1319	1030	949	1032	3693	2031	9754.	1.00
2	1019			1232	3693	2231	9754.	1.22
3	1819			1032	3693	2031	9754.	1.00
4	1019			1232	3693	2031	9754.	1.07
5	1019			1232	3693	2031	9754.	
6	1019			1032	3593	2030	9753.	1.00
7	1019	1030	949	1032	3693	2025	9748.	1.00
8	1019	1338	949	1232	3693	2010	9741.	1.00
9	1017	1030	949	1032	3693	2039	9732.	1.00
10	1019		949	1032	3693	1992	9715.	1.00
	1219		949	1032	3693	1978	9781.	0.99
12	1019		949		3692	1961	9683.	0.99
13	1019		949	1.032	3683	1927	9640.	0.99
14	1019		949	1032	3664	1876	9570.	2.98
	1019		949	1032	3641	1801	9472.	0.97
	1015		949	1332	3619	1742	9392.	3.96
17		1230	949	1031	3557	1606	9191.	0.94
18		1029	949	1022	3438	1401	8857,	0.91
19		1028	949	1012	3281	1205	8491.	0.87
. 23	999 986	1021	949	997	2099	1036 937	8021.	2.82
21 22	921	975	929	895	2793	875	7701. 6912.	Ø.79 Ø,71
23	798	391	762	728	2317 1979	785	5943.	9.61
24	685	771	564	547	1750	722	5032.	0.52
25	614	642	476	439	1505	666	4442.	2.46
26	584	595	450	404	1544	637	4214.	0.43
27	537		408	361	1423	578	3852.	0.39
28	499	504	374	316	1310	531	3540.	0.36
29	470	475	337	288	1204	481	3255.	0.33
30	443	443	312	264	1115	423	3000.	0.31
31	424	433	300	258	1380	461	2896.	0.30
32	394	418	278	227	1309	345	2674.	0.27
33	369	396	257	207	933	291	2453.	0.25
34	353	374	230	185	853	231	2226.	0.23
35	337	355	221	161	783	197	2054.	0.21
36	328	344	515	150	734	17/	1945.	0.20
37	325	325	186	134	658	145	1753.	0,19
38	284	398	163	109	586.	121	1576.	
39	261	293	155	84	510	97	1400.	0.14
40	237	27.6	134	61	436	63	1227.	0.12
41	555	267	129	59	403	53	1133.	0.12
42	192	242	113	39	349	38	973.	0.10
43	165	224	97	32	300	25	843.	2.09
44	141	197	81	19	248	14	720.	0.07
45	121	177	63	11	189	,	571.	0.06

TABLE L3 (cont.)

### ZUNI INTERIOR

DEG.	DEC	JAI	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	176	161	63	9	1,66	4	509.	0.05
47	82	134	54	4	1.16	1	391.	0.24
48	65	104	42	2	73	U	286.	0.03
49	47	81	27	2	43	v	200.	9.02
50	29	57	17	2	28	V	133.	2.01
51	23	52	14	1	23	- W	113.	0.01
52	6	34	8	1	5	Ø	54.	2.20
53	3	23	4	1	Ø	Ø	31.	9,30
54	2	15	1	1	Ø	Ø	19.	0.00
55	3	5	Ø	1	9	И	6.	2.00
56	Ø	4	Ø	1	Ø	И	5.	0.00
57	Ø	3	0	1	Ø	W	4.	0.00
58	7	1	Ø	1	Ø	Ø	2.	0.00
59	3	1	3	1	Ø	Ø .	2.	0.00
60	3	1	ð	1	Ø	₩	2.	0.00
61	Ø	1.	0	1	Ð	W	2.	0.00
62	Ø	1	3	1	Ø	Ø	2.	0.00
63	Ø	1	Ø	1	Ø	Ø	2.	0.00
64	Ø	1	Ø	1	Ø	И	2.	0.00
65	Ø	1	0	.1	Ŋ	Ø	2.	0.00
66	Ø	1	Ø	1	0	0	2.	0.00
67	Ø	1	Ø	1	Ø	W	2.	0.00
68	Ø	1	2	1	Ø	Ø	2.	0.00
69	J	1	Ø	1	0	v	2.	0.00
70	Ø	1	3	1	Ø	U	2.	0.00
71	Ø	1.	Ø	1	Ø .	Ø	2.	0.00
72	3	Ø	Ø·	1	Ø	Ю	1.	0.03
73	Ø	9	Ø	1	Ø	i)	1.	0.00
74	3	0	Ø	1	Ø	Ø	1.	0.00
75	Ø	Ø	Ø	1	Ø	0	1.	0.00
76	0	0	Ø	1	ð	U	1.	0.00
77	9	Ø	Ø	Ø	n .	N	Ø.	0.00

TABLE M3

#### CARTRIDGES 7.62mm INTERIOR

DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	c.PROB
1	1017	1030	948	1.231	3693	2031	9750.	1.00
2		1030		1031	3693	2031	9750.	1.00
3		1030		1031	3693	2031	9750.	1.00
4		1230		1231	3593	2031	9750.	
5		1030		1031	3693	2030	9749.	1.00
6		1030		1031	3693	2329	9748.	1.00
7		1030		1331	3693	2025	9744.	1.00
8		1030		1031	3693	2319	9738.	1.33
9		1030		1031	3693	2005	9724.	1.00
10		1030	948	1331	3693	1984	9703.	1.00
11		1030	948	1031	3693	1975	9694.	3.99
12	1017	1030	948	1031	3691	1951	9668.	0.99
13	1017	1230	948	1231	3684	1917	9627.	3.99
14	1017	1030	948	1031	3662	1849	9537.	0.98
15		1230	948	1731	3635	1771	9432.	2.97
16		1030	948	1031	3611	1708	9345.	0.96
17		1030	948	1.030	3541	1555	9121.	0.94
18		1953	948	1018	3422	1332	8766.	0.90
19	1014	1026	948	1006	3233	1141	8365,	0.86
20	997	1019	948	986	2915	980	7845.	0.80
21	985	1013	948	961	2714	935	7556.	2.77
22	914	971	931	879	2202	837	6734,	0.69
23	773	373	758	682	1878	776	5740.	3.59
24	669	720	537	510	1665	728	4838.	9.50
25	588 562	560	449	417 385	1549	695	4299. 4087.	0.44
26	514	512	416. 381	349	1495 1402	626	3784.	Ø.42 Ø.39
28	490	483	347	314	1319	585	3538.	9.36
29	461	457	323	295	1252	535	3323.	0.34
30	432	432	307	266	1182	486	3105.	0.32
31	419	421	299	257	1140	450	2986.	0.31
32	399	405	283	242	1864	405	2798.	0.29
33	375	386	267	222	1300	355	2685.	0.27
34	356	371	241	201	933	305	2407.	0.25
35	337	359	221	180	853	252	2212.	0.23
36	326	352	214	171	814	244	2121.	0.22
37	304	335	200	151	717	2/18	1915.	0.20
38	276	315	187	124	653	166	1721.	0.18
39	253	296	166	96	571	114	1495.	0.15
40	558	280	143	82	482	90	1305.	0.13
41	217	270	135	73	4.40	75	1210.	0.12
42	184	233	119	59	368	45	1008.	0.10
43	157	212	101	41	293	29	833.	0.29
44	133	130	81	33	238	26	688,	0.07
45	113	159	63	29	191	14	566.	0.06

TABLE M3 (cont.)

#### CARTRIDGES 7.62mm INTERIOR

DEG.	DEC	JAH	FE3	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	94	1.48	61	23	1.73	12	511.	3.35
47	84	134	43	20	130	9	420.	0.04
48	65	118	35	11	102	5	336.	0.03
49	57	98	29	4	76	2	266.	0.23
50	42	81	24	0	46	1	194.	0.02
51	36	77	22	20	37	Ø	172.	0.32
52	27	58	13	0	14	Ø	112.	0.01
53	17	43	9	2	9	Ø	78.	0.00
54	6	27	7	Ø	5	0	45.	0.00
55	. 5	15	2	7	2	W	24.	0.00
56	5	12	1	2	1	И	19.	0.00
57	1.	.4	1	Ø	1	И	7.	0.00
58	. 7	. 0	Ø	9	1	Ø	1.	0.00
59	Ø :	Ø	a	ø	ī	Ø	1.	0.00
60	9	i j	Ø	0	1	0	î.	0.00
61	2	Ø	Ø	Ø	1	.0	1.	0.30
62	3	0	Ø	2	1	Ø	1.	0.00
63	ä	Ø	ð	2	1	Ø	1.	0.00
64	2	Ø	9	8	1	6	1.	0.00
65	Ø	O	Ø	. 0	ā	W	Ø.	Ø.0H

TABLE N3'

### CARTRIDGES 7.52mm EXTERIOR

DEG.	DEC.	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
1.	1018	1031	947	1832	3692	2931	9751.	1.00
2	1018			1232	3692	2031	9751.	1.00
3	1018			1/32	3692	2031	9751.	1.00
4	1018			1032	3692	2031	9751.	1.00
5	1018			1232	3692	2030	9750.	1.00
6	1018			1232	3692	2027	9747.	
7	1018			1032	3692	2024	9744.	1.00
8.	1018			1032	3692	2017	9737.	1.00
9	1018			1232	3692	2001	9721.	1.00
10		1031	947	1032	3592	1980	9700.	0.99
		1/31	947	1032	3592	1.971	9697.	0.99
		1031	947	1332	3689	1944	9661.	0.99
	1018		947	1032	3578	1907	9613.	0.99
14		1031	947	1332	3659	1840	9527.	0.98
15	.1013			1037	3528	1754	9418.	0.97
16	1713	1031	947	1032	3601	1691	9320.	0.96
17	1018	1031	947	1031	3529	1547	9123.	0.93
18	1018	1029	947	1018	3396	1316	8724.	0.89
19	1013	1025	947	1.005	3204	1125	8319.	0.85
. 20	993	1017	947	986	2383	975	7799.	0.80
21		1003	947	959	2663	931	7485.	0,77
22	.895	960	927	881	2181	835	6679.	0.68
23	763	865	753	688	1859	775	5700.	0.58
24	655	720	524	507	1652	734	4793.	
25	579	594	443	423	1541	696	4276.	
26	550	550	414	386	1485	574	4064.	0.42
27	515	508	377	349	1410	6.34	3793.	0.39
28	488	432	347	324	1334	594	3569.	0.37
29	459	451	326	304	1256	555	3351.	0.34
30	433	428	312	281	1198	506	3163.	0,32
31	428	423	302	272	1162	492	3079.	0.32
32	471	408	290	253	1288	448	2888.	0.30
33	377	392	277	228	1725	392	2691.	0.28
34	365	377	258	211	971	353	2535.	0.26
35	349	360	233	194	1914	307	2357.	0.24
36	342	357	226	184	384	285	2278.	2.23
37		339	212	171	820	252	2114.	0.22
38	295 276	324	201	158	754	211 171	1943.	0.20 0.18
39 40	259	295	175	140	678	139	1581.	0.16
41 .	257	287	167		601		1501.	0.15
42	234	275	150	99 79	57Ø 514	121	1348.	0.14
43	206	255	129	68	445	68	1171.	0.12
44	191	535	114	56	379	44	1015.	0.10
45	166	550	104	42	314	31	877.	0.09
43	700	220	104	46	314	27	0//.	0.09

TABLE N3 (cont.)

#### CARTRIDGES 7.62mm EXTERIOR

		RECO	RDER	31A.	ROCKET MOT	OR CHANNE	EL 19	
DEG.	DEC	JAN	FEB	MAR	AUT-SPRING	WINTER	TOTAL	C.PROB
46	157	206	98	39	280	21	807.	0.08
47	134	188	87	34	225	17	685.	0.07
46	111	167	73	25	186	11	.573.	0.06
49	87	155	54	19	153	10	478.	0.05
50	71	135	43	11	113	4	377.	0.94
51	63	128	35	7	96	. 5	332.	0.93
52	56	102	30	5	69	1	263.	0.03
53	42	89	24	2	39	1	197.	6.02
54	32	72	20	1	26	Ø	151.	0.02
55	23	54	15	1	12	Ø	102.	0.01
56	1.3	47	10	1	9	6	82.	0.00
57	7	30	7	1	4	U	49.	0.00
58	4	20	2	1	2	IJ	29.	0.00
59	2	11	1	1	1	И	16.	0.00
63	Ø	3	1	1	1	.)	6.	0.00
61	Ø	2	1	1.	1.	U	5.	0.00
62	Ø	1	Ø	1	1	U	3.	0.00
63	Ø	1	0	1.	ī	Ŋ.	3.	0.00
64	Ø	1	Ø	1	1	Ø	3.	0.00
65	Ø	1	2	1	1	()	3.	0.00
66	O	1	Ø	1	1	Ø	3.	0.00
67	Ø	1	Ø	1	1.	12	3.	0.00
68	Ø	1	0	1	0	ω.	2.	0.99
69	Ø	1.	Ø	1	Ø	Ø	2.	0.00
70	Ø	1.	Ø	1	Ø	Ø	2.	0.00
71	Ø	1	Ø	1	Ø	9	2,	0.00
72	Ø	- (3	Q.	1	0	0	1.	0.00
73	0	Ø	0	1	Ø	v	1.	0.00
74	g	Ø	Ø	1	ð	Ø	1.	0.00
75	Ø	0	Ø	1	Ø	8	1.	0.00
76	9	q	9	1	Ø	Ø	1.	0.00
77	g	(4	a	ā	Ø ·	Ø	ā.	0.03

0

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